FULL-SCALE CRASH EVALUATION OF THE NETC 4-BAR SIDEWALK-MOUNTED STEEL BRIDGE RAILING

C. E. Kimball and J. B. Mayer

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Prepared by:
Southwest Research Institute
6220 Culebra Road
San Antonio, Texas 78238-5166

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16. Abstract

This report presents the results of three (3) NCHRP Report 350, Test Level 4 (TL-4) crash tests conducted on a sidewalk-mounted steel bridge railing designed by the New England Transportation Consortium (NETC). The test vehicles included an 820-kg small car, a 2000-kg pickup truck, and an 8000-kg single-unit van truck. Barrier performance was determined to be acceptable for the Test Level 4 (TL-4) Longitudinal Barrier category outlined in NCHRP Report 350.

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INTRODUCTION

Three vehicle crash tests were performed by Southwest Research Institute, San Antonio, TX, to evaluate the performance of a 4-bar, sidewalk-mounted steel bridge railing which had been designed by the New England Transportation Consortium (NETC). Specifically, tests designated as types 4-10, 4-11, and 4-12 in NCHRP Report 350⁽¹⁾ were performed. This report summarizes those tests, but does not contain all the details found in the individual test reports. Instead, the reader is referred to Publication Nos. FHWA-RD-98-028⁽²⁾, -029⁽³⁾, and -030⁽⁴⁾ for more detailed descriptions and applicable data.

Since the same barrier configuration was utilized in all three tests, the only variables between tests were the vehicle types and weights as well as the impact velocities and angles. These are shown in table 1 along with the warrant for each type of test.

The text in the following sections briefly describes the test installation, vehicles, test sequences, and resulting damage to both the installation and vehicle. In addition, conclusions regarding barrier performance during each of the individual tests as well as an overall evaluation will be offered.

TEST INSTALLATION

Facility

These tests were performed along and adjacent to the inactive East Runway at Brooks Air Force Base, San Antonio, Texas. As shown in figure 1, a concrete approach and 34.1-m-long sidewalk were constructed at an angle to the runway and a 32.9-m-long bridge rail test article erected on the sidewalk.

Test Article

Drawings describing an elevation and cross section of the test installation are shown in figures 2 and 3, respectively. Briefly, the steel-reinforced, concrete sidewalk was 2.0 m wide by 203 mm high on the traffic side which sloped upward to a level 229 mm high where the bridge rail was mounted. The bridge rail utilized W6 x 25 steel posts which were welded to 25-mm x 254-mm x 356-mm base plates, and these were attached to the concrete with 25-mm anchor bolts. Post spacing was 2.44 m. Four longitudinal rails fabricated from steel structural tubing were attached to the posts with 19.1-mm diameter studs; rail heights, measured from the concrete sidewalk to the top of the rails, were 229 mm, 475 mm, 813 mm, and 1168 mm. Further details of the installation and its components are shown in the drawing of Appendix A.

Photographs of details of the barrier installation are shown in figure 4. Table 2 summarizes the beam and post materials used in the installation and also lists dimensions of the key components of the system.

¹Ross, H.E., Jr., Sicking, D.L., Zimmer, R.A., and Michie, J.D., "Recommended Procedures for the Safety Performance Evaluation of Highway Appurtenances," *NCHRP Report 350*, Washington, D.C., 1993.

²Kimball, C.E., and Mayer, J.B., "Full-Scale Crash Evaluation of Sidewalk-Mounted Steel Bridge Railing, NCHRP Test 4-10, SwRI Test No. NETC-1," Publication No. FHWA-RD-98-028, Federal Highway Administration, 1998.

³Kimball, C.E., and Mayer, J.B., "Full-Scale Crash Evaluation of Sidewalk-Mounted Steel Bridge Railing, NCHRP Test 4-11, SwRI Test No. NETC-2," Publication No. FHWA-RD-98-029, Federal Highway Administration, 1998.

⁴Kimball, C.E., and Mayer, J.B., "Full-Scale Crash Evaluation of Sidewalk-Mounted Steel Bridge Railing, NCHRP Test 4-12, SwRI Test No. NETC-3," Publication No. FHWA-RD-98-030, Federal Highway Administration, 1998.

TEST VEHICLE, CONTROLS, AND DATA SYSTEMS

Vehicle and Dummy

Pre-test photographs of the vehicles used are shown in Figures 5 through 7. For tests NETC-1 and NETC-2, an uninstrumented dummy was placed in the driver's seat of each vehicle and restrained with lap and shoulder belts; no dummy was used in test NETC-3.

Vehicle Controls

Target impact point of the vehicle for all tests was the centerline of post 6. Each vehicle was guided to that location using a 6.4-mm diameter x 457.2-m-long steel cable which passed through a guide tube/bracket attached to the left front wheel spindle. The cable was pretensioned and located alongside the run-up strip where it would not interfere with post-impact vehicle trajectory. Just prior to impact, the guide tube/bracket was sheared off allowing the vehicle free trajectory.

Braking of each test vehicle was accomplished by use of an air cylinder attached to its brake pedal. The air cylinder was activated by a gas-charged accumulator through an intermediate solenoid valve. The solenoid valve was remotely controlled by the test conductor.

Each test vehicle was towed into the barrier using a cable/pulley system for reverse towing, i.e., the tow vehicle moved away from the barrier as the test vehicle moved toward it. The tow cable was attached to the underside of the test vehicle and released just prior to impact. Vehicle impact speed control was achieved by means of an automatic controller attached to the engine distributor of the tow vehicle. After the tow vehicle accelerated to its predetermined test speed, the

controller pulsed the ignition, maintaining the tow vehicle at that speed.

Electronic Data Acquisition

The test vehicles were instrumented with multiple accelerometers and one rate gyro; locations of these transducers in each vehicle are described in table 3. The accelerometers were oriented to obtain data in directions parallel to the longitudinal, lateral, or vertical axes of the vehicle, whereas the rate gyro was oriented to measure the yaw angular rate change the vehicle experienced during the impact sequence. All transducer data was recorded by a Pacific Instruments Model 5600 Data Acquisition System (DAS) which contained signal conditioners, amplifiers, appropriate SAEJ211 filters and digitizers with onboard memory for up to 32 data channels at programmable sample rates to 100 kilohertz per channel. Digitized data was recorded in solid state non-volatile memory with a capacity of 65,000 data points per channel.

In addition to the above, two accelerometers were mounted on the back flange of post 7 of the barrier installation. These were located 51 mm and 533 mm below the top of the post and were oriented to obtain data in a lateral direction to the barrier. These two transducers were connected to a signal conditioning unit for power, calibration and balancing, and their signals recorded during each test by digital computer at a rate of 1 kilohertz.

Film Data Acquisition

In addition to the electronic data, highspeed film coverage of all three tests included a camera onboard the vehicle (tests NETC-1 and NETC-2 only) as well as cameras adjacent to and overhead of the barrier installation (all tests).

Data Processing

Vehicle transducer data were downloaded to a personal computer after each test and processed through an Institute-developed computer program. This program utilized accelerometer and rate gyro data to determine vehicle acceleration (in longitudinal, lateral, and vertical directions), heading angle, velocity, and displacement as a function of time during each event. In addition, this data provided input to the program for calculation of the highest 50-millisecond average accelerations for the vehicle as well as occupant risk data, including impact velocities (with the interior of the vehicle) and 10-millisecond average ridedown accelerations. The output of this data was provided in both tabular or graphical form.

Data from the two accelerometers mounted on post 7 were transferred to a floppy disk after each test, and then imported to a Microsoft Excel spreadsheet. These data were then converted to standard engineering units (g's) and output in both tabular and graphical form.

TEST DESCRIPTION

Test NETC-1.

This was the first test of the series and utilized a small car as the test vehicle. As shown in the test summary diagram of figure 8, the vehicle traversed the sidewalk and impacted the barrier 610 mm downstream of post 6, maintaining contact with the longitudinal rails for 1.83 m as it was redirected, exiting the installation at a 6.6° angle (calculated from measured tire marks). Figures 9 and 10 show the redirection sequence of the vehicle from overhead as well as behind the barrier viewpoints. The post-impact trajectory of the vehicle was such that it traveled in a relatively straight line after loss of contact, coming to a stop 77 m downstream of initial

impact point (brakes had been applied immediately after loss of contact with the barrier). Two of the vehicle accelerometers, the lateral accelerometer at the c.g. and the longitudinal accelerometer mounted on the instrument panel, malfunctioned at impact, resulting in no data on those channels. Data from film analysis indicated maximum 50 msec average accelerations of -3.4 g's in the longitudinal direction and 6.9 g's in the lateral direction. Occupant risk values showed that the dummy did not travel the required hypothetical distance in the longitudinal direction, and a value of 1.4 m/sec occupant impact velocity is reported at the maximum displacement of 0.2 m. Lateral impact velocity is calculated from film analysis as 6.4 m/sec. Maximum ridedown acceleration was 6.4 g's lateral.

Test NETC-2. In this pickup truck test, as shown in figure 11, the vehicle traversed the sidewalk and impacted the barrier 610 mm downstream of post 6, maintaining contact with the longitudinal rails for 3.96 m as it was redirected, exiting the installation at an 8.2 degree angle (calculated from measured tire marks). Figures 12 and 13 show the redirection sequence of the vehicle from overhead as well as behind the barrier viewpoints. The post-impact trajectory of the vehicle was such that it traveled in a relatively straight line after loss of contact, coming to a stop 62 m downstream of the initial impact point (brakes had been applied immediately after loss of contact with the barrier). Three of the vehicle accelerometers, the lateral accelerometer at the c.g. and the longitudinal accelerometers mounted on the instrument panel and bottom of the engine, malfunctioned at impact, resulting in no data on those channels. The net effect of the data loss from the lateral accelerometer was that the 50 msec average vehicle acceleration and occupant risk values in the lateral direction could not be calculated. However, the more important (for this test) longitudinal factors could be calculated and were as follows:

(1) maximum 50 msec average acceleration in the longitudinal direction was -6.12 g's, (2) the occupant impact velocity was 3.99 m/sec, and (3) the maximum occupant ridedown acceleration was -2.55 g's.

Test NETC-3. As shown in the test summary diagram of figure 14, the singleunit van truck traversed the sidewalk and impacted the barrier 610 mm upstream of post 6, deflecting the two top rails approximately 25 mm at the splice between posts 6 and 7 while maintaining contact with the longitudinal rails for 12.19 m as it was redirected. The vehicle then exited the barrier at a 4.1 degree angle (calculated from measured tire marks). Figures 15 and 16 show the redirection sequence of the vehicle from overhead as well as behind the barrier viewpoints. Since the front axle was dislodged during the impact, the vehicle veered hard to the right after exiting and stopped 84 m downstream and 91 m normal to the test installation. Although some of the vehicle accelerometers had interruptions in their data due to the impact, only one, the longitudinal accelerometer mounted on the bottom of the engine, suffered complete data loss. Maximum 50 msec average accelerations in the longitudinal and lateral directions were -2.72 g's and -5.79 g's, respectively. Occupant risk values were as follows: (1) the occupant impact velocities were 1.65 m/sec in the longitudinal direction and -2.89 m/sec in the lateral direction, and (2) the maximum occupant ridedown accelerations were -8.95 g's in the longitudinal direction and 14.30 g's in the lateral direction.

BARRIER DAMAGE

Test NETC-1. Damage to the barrier, as shown in figure 17, consisted of scuffing of the longitudinal rails which only required repainting prior to further testing. There was

no measurable dynamic or permanent deflection of the barrier.

Test NETC-2. Damage to the barrier, as shown in figure 18, occurred mostly at post 7. The top of post 7 and the top rail section attached to it had 13 mm of permanent deflection, and the baseplate of the post was raised upward at the center approximately 3.5 mm. The remainder of the damage consisted of scuffing of the longitudinal rails which only required repainting prior to further testing. The top rail was straightened, but post 7 required replacement prior to subsequent testing.

Test NETC-3. Barrier damage is shown in figure 19. Maximum permanent rail deflection occurred at the splice upstream of post 7 and was measured as 13 mm. Two sections of the top rail had permanent deflection (deflection occurred between posts 6 and 7), and posts 6 and 7 were tilted back; the base plates of both posts were raised upward at the center approximately 3.5 mm. The remainder of the damage consisted of scuffing of all longitudinal rails between posts 6 and 11.

VEHICLE DAMAGE

Test NETC-1. As shown in figure 20, the test vehicle sustained damage to the left front fender and along the left side, as well as damage to headlight/grill area. The left side of the front bumper was deformed rearward, and the left front suspension/wheel/tire displaced rearward. All tires except the right rear were either blown out or deflated as a result of the impact. The exterior vehicle damage scale was estimated to be 11-FL-2 using the VDS system and 11FLEE2 using the CDC system. The interior deformation of the occupant compartment was LF0000000 using the OCDI system. There was no deformation or intrusion into the occupant compartment.

Test NETC-2. Figure 21 shows that the test vehicle sustained extensive damage to the left front fender and along the left side, as well as damage to the headlight/grille area. The left side of the front bumper was deformed rearward, and the left front suspension/wheel/tire displaced rearward. Contact with the edge of the sidewalk damaged the right front suspension also. All tires except the right rear were either blown out or deflated as a result of the impact. The exterior vehicle damage scale was estimated to be 11-FL-3 using the VDS system and 11FLEE3 using the CDC system. The interior deformation of the occupant compartment was LF0000000 using the OCDI system. There was no deformation or intrusion into the occupant compartment.

Test NETC-3. The test vehicle, as shown in figure 22, sustained extensive damage. As described previously, the entire front axle (axle/brakes/wheels/tires, etc.) was dislodged by the impact and later separated during vehicle run out. In addition, the left corner of the front bumper was deflected rearward, a portion of the left front fender was torn away (the vehicle had a one-piece, fiberglass front clip), the left step under the driver's door was torn away, the left rear, outside wheel was damaged, the cargo box was racked toward the left side, and the antiunderride assembly was fractured at the left rear corner. Since the exterior damage scales, i.e., the VDS system and the CDC system, are not applicable to this class of test vehicle, no assessment of that type was made. The OCDI system is also not applicable; however, there was no deformation or intrusion into the occupant compartment.

EVALUATION OF TEST RESULTS

Performance evaluation of the barrier design is based on the criteria shown in table 5.1 titled "Safety Evaluation Guidelines," of

NCHRP Report 350. The specific requirements applicable for each of the test types, i.e. 4-10, 4-11, and 4-12, are shown in tables 4 through 6 together with the test results. Although the data loss of the vehicle lateral accelerometer during test NETC-1 (small car) precluded any occupant risk calculations and subsequent assessments (see table 4) from those calculated values, it was conjectured by SwRI project personnel that the barrier performance would have passed those criteria also. This was based on a comparison of vehicle damage and shallow exit angle for this test with those tests performed previously. Table 5 for test NETC-2 (pickup truck) indicates that the barrier passed in all categories of assessment, but table 6 for test NETC-3 (singleunit van truck) indicates a failure in the category applicable to vehicle intrusion into adjacent traffic lanes. This was a result of the loss of the front axle assembly causing the vehicle to veer sharply to the right, and it would have been a hazard to adjacent traffic.

CONCLUSIONS

From these tests and the evaluations described in the preceding section, the NETC 4-bar, sidewalk-mounted steel bridge railing appears to meet most of the requirements for a longitudinal barrier. The exception being, of course, the intrusion by the vehicle into adjacent traffic lanes as described for test NETC-3 in the previous section.

Table 1. Summary of test conditions.

Barrier Evaluation	Length of need; occupant risk	Barrier strength	Barrier strength (heavy vehicle)
Impact Angle (deg)	20	25	15
Impact Velocity (km/h)	100	100	08
Vehicle Weight (kg)	820	2000	8000
Vehicle Type	Small Car (1991 Ford Festiva)	Pickup Truck (1991 Ford F-250)	Single-Unit Van Truck (1993 IH 4600-LP)
Test Designation and NCHRP 350 Test Type	NETC-1 (4-10)	NETC-2 (4-11)	NETC-3 (4-12)

Table 2. Installation bill of material.

Bill of Material

Item	Quantity
TS 4 x 4 x 1/4 - 7.31 M long rail	12
TS 8 x 4 x 5/16 - 7.31 M long rail	4
TS 4 x 4 x 1/4 - 3.66 M long rail	3
TS 8 x 4 x 5/16 - 3.66 M long rail	1
W6 x 25 - 1.05 M high post	14

Table 3. Vehicle data transducer locations.

Туре	Location	Orientation	Applicability
Accelerometer	Center of gravity	Longitudinal axis	All tests
Accelerometer	Center of gravity	Lateral axis	All tests
Accelerometer	Center of gravity	Vertical axis	All tests
Rate Gyro	Center of gravity	Longitudinal axis	All tests
Accelerometer	Over rear axle	Longitudinal axis	All tests
Accelerometer	Over rear axle	Lateral axis	All tests
Accelerometer	Over rear axle	Vertical axis	All tests
Accelerometer	Top engine block	Longitudinal axis	All tests
Accelerometer	Bottom of engine block	Longitudinal axis	All tests
Accelerometer	Right front disc brake caliper	Longitudinal axis	All tests
Accelerometer	Left front disc brake caliper	Longitudinal axis	All tests
Accelerometer	Center of instrument panel	Longitudinal axis	All tests
Accelerometer	Right rear brake backing plate	Vertical axis	Test NETC-3 Only
Accelerometer	Left rear brake backing plate	Vertical axis	Test NETC-3 Only

Table 4. Test assessment summary - NCHRP Report 350 test designation 4-10 - SwRI test number NETC-1.

Dociomotion	L					
Designation	Factor		Description		Test Results	Accommond
O	Structural Adequacy	Test article should contain and redirect the vehicle; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	nd redirect the vehicl ride the installation all is acceptable.	e; the vehicle should not though controlled lateral	Vehicle contained and redirected.	PASS
Ω	Occupant Risk	Detached elements, fragments, or other debris from the test article shall not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformation of, or intrusions into, the occupant compartment that could cause serious injuries shall not be permitted.	ts, or other debris fron for penetrating the ocher traffic, pedestrian trusions into, the occashall not be permitted	n the test article shall not cupant compartment, or s, or personnel in a work upant compartment that 1.	This article and its elements did not penetrate the occupant compartment or present undue hazard to adjacent traffic or others. There was no deformation or intrusion into the	PASS
Ĺ	Occupant Risk	The vehicle should remain upright during and after collision although moderate roll, pitching, and yawing are acceptable.	upright during and a	after collision although e.	Vehicle remained upright during and	PASS
I	Occupant Risk	Occupant impact velocities should satis Occupant Impact Velocity Limits (m/s)	velocities should satisfy the following: Velocity Limits (m/s)	owing:	ared the complete.	
		Component	Preferred	Maximum		
		Longitudinal	6	.12	1.4	2014
		Lateral	6	12		rass
-	Occupant Risk	Occupant ridedown accelerations should satisfy the following:	ions should satisfy th	e following:	6,4	NONE
		Disconnect amendance	anon cimits (G's)			
		Component	Preferred	Maximum		
		Longitudinal	15	20	*0	DAGG
		Lateral	15	20	6.4	2007
×	Vehicle Trajectory	After collision, it is preferable that the vehicle's trajectory not intrude into adjacent traffic lanes.	that the vehicle's tra		Vehicle did not intrude into adjacent	PASS
X	Vehicle Trajectory	The exit angle from the test article preferably should be less than 60 percent of test impact angle, measured at time of vehicle loss of contact with test device.	ticle preferably shoul	+	Vehicle exit angle was 6.6 degrees.	PASS
*],					

Table 5. Test assessment summary - NCHRP Report 350 test designation 4-11 - SwRI test number NETC-2.

Designation	Factor	Descr	Description	Test Results	Assessment
A	Structural Adequacy	Test article should contain and redirect the penetrate, underride, or override the install deflection of the test article is acceptable.	Test article should contain and redirect the vehicle; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	Vehicle contained and redirected.	PASS
Ω .	Occupant Risk	Detached elements, fragments, or other debris from the tenderate or show potential for penetrating the occupan present an undue hazard to other traffic, pedestrians, work zone. Deformation of, or intrusions into, the occupantat could cause serious injuries shall not be permitted.	Detached elements, fragments, or other debris from the test article shall not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformation of, or intrusions into, the occupant compartment that could cause serious injuries shall not be permitted.	This article and its elements did not penetrate the occupant compartment or present undue hazard to adjacent traffic or others. There was no deformation or intrusion into the occupant compartment.	PASS
íz.	Occupant Risk	The vehicle should remain upright during and after moderate roll, pitching, and yawing are acceptable.	The vehicle should remain upright during and after collision although moderate roll, pitching, and yawing are acceptable.	Vehicle remained upright during and after the collision.	PASS
ħ	V e hicle Trajectory	Occupant longitudinal impact veloci should satisfy the following:	tudinal impact velocity and ridedown acceleration he following:	Occupant longitudinal impact velocity and ridedown acceleration values were:	
		Component	Maximum		
		Longitudinal impact velocity	12 m/sec	3.99 m/sec	PASS
		Longitudinal ridedown acceleration	20 G's	2.55 G's	PASS
ጟ	Vehicle Trajectory	After collision, it is preferable that the vehicle's trajectory not intrude into adjacent traffic lanes.	e vehicle's trajectory not intrude	Vehicle did not intrude into adjacent traffic lanes.	PASS
Z	Vehicle Trajectory	The exit angle from the test article preferably should be less than 60 percent of test impact angle, measured at time of vehicle loss of contact with test device.	from the test article preferably should be less than 60 mpact angle, measured at time of vehicle loss of contact	Vehicle exit angle was 6.6 degrees.	PASS

Table 6. Test assessment summary - NCHRP Report 350 test designation 4-12 - SwRI test number NETC-3.

Designation	Factor	Description	Test Results	Assessment
A	Structural Adequacy	Test article should contain and redirect the vehicle; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	Vehicle contained and redirected.	PASS
D	Occupant Risk	Detached elements, fragments, or other debris from the test article shall not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformation of, or intrusions into, the occupant compartment that could cause serious injuries shall not be permitted.	This article and its elements did not penetrate the occupant compartment or present undue hazard to adjacent traffic or others. There was no deformation or intrusion into the occupant compartment.	PASS
Ð	Occupant Risk	It is preferable, although not essential, that the vehicle remain upright during and after the collision.	Vehicle remained upright during and after the collision.	PASS
×	Vehicle Trajectory	After collision, it is preferable that the vehicle's trajectory not intrude into adjacent traffic lanes.	Vehicle intruded into adjacent traffic lanes.	DID NOT PASS
×	Vehicle Trajectory	The exit angle from the test article preferably should be less than 60 percent of test impact angle, measured at time of vehicle loss of contact with test device.	Vehicle exit angle was 4.1 degrees.	PASS

Figure 1. Barrier installation.

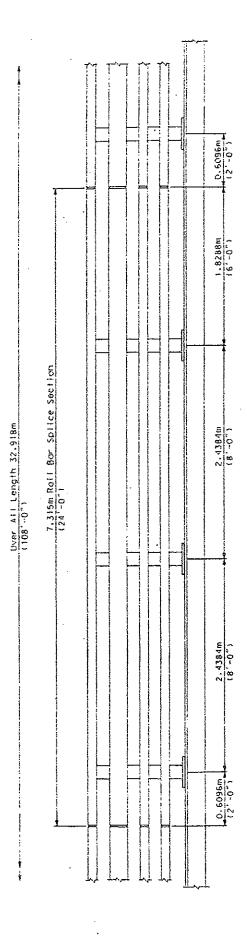


Figure 2. Barrier elevation drawing.

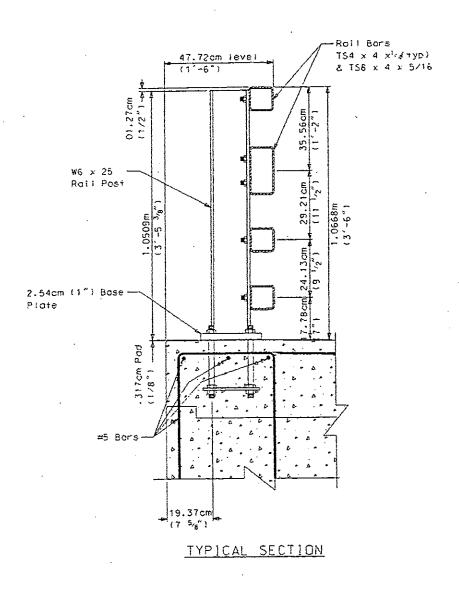
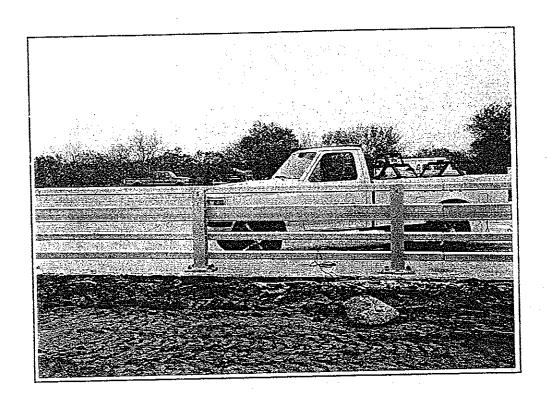


Figure 3. Barrier cross-section drawing.

Figure 4. Barrier photographs.

Figure 5. Vehicle photographs - Test NETC-1.



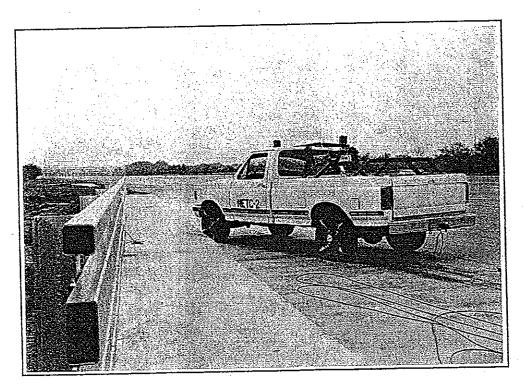
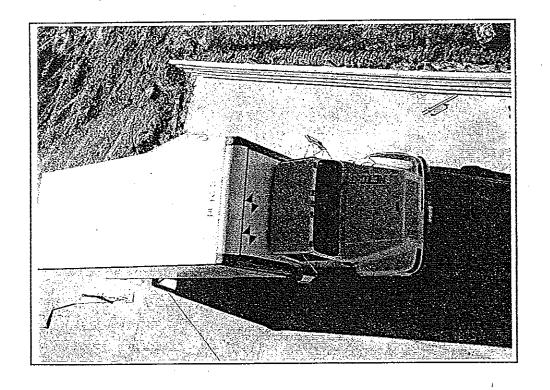
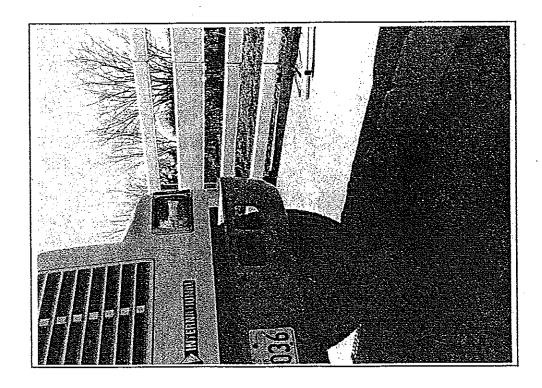
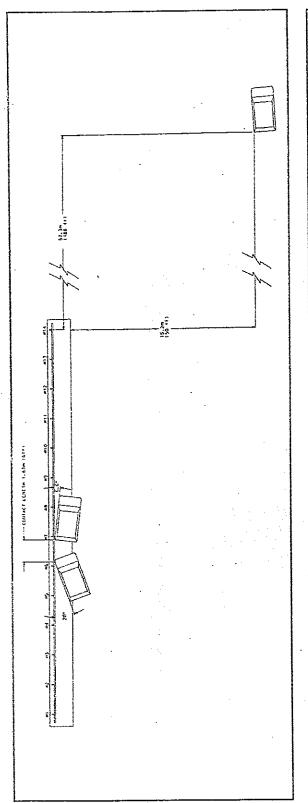


Figure 6. Vehicle photographs - Test NETC-2.







	-				
4. General Information		7. Test Vehicle (Continued)		10, Ridedown Acecleration (g's)	
Test Agency	Southwest Research Institute	Mass (kg) Dunnay(s)	75	y-direction	*
Test Number	NETC-1	Mass (kg) Gross Static	902	11. Test Article Deflection (m)	
Test Date	11/18/97	8. Impact Conditions		Dynamic	0
5. Test Article		Speed (km/lı)	100.0	Permanent	0
Type	Bridge Rail	Angle (deg)	20.0	12. Vehicle Damage	
Installation Length (m)	32.9	9. Exit Conditions		Exterior	
Barrier	4 Steel Rails	Speed (km/h)	18.3	VDS	11-FL-2
6. Soll Type and Condition	N/A	Angle (deg)	6,6	CDC	11FLEE2
7. Test Vchicle		10. Occupant Risk Values		Interior	
Type	Production	Impact Velocity (m/s)		OCDI	LF0000000
Designation	820C	x-direction	•	13. Post-Impact Vehicular Behavior	
Model	1991 Ford Festiva	y-direction	¥	Maximum Roll Angle (deg)	10 Appreximate
Mass (kg) Curb	82.7	Ridedown Acceleration (g's)		Maximum Pitch Angle (deg.)	5 Approximate
Mass (kg) Test Inertial	827	X-direction	4	Maximum Yaw Angle (deg)	34 Approximate

*No occupant risk data - lateral accelerometer malfunctioned during test.

Figure 8. Impact sequence and summary of test conditions and results - Test NETC-1.

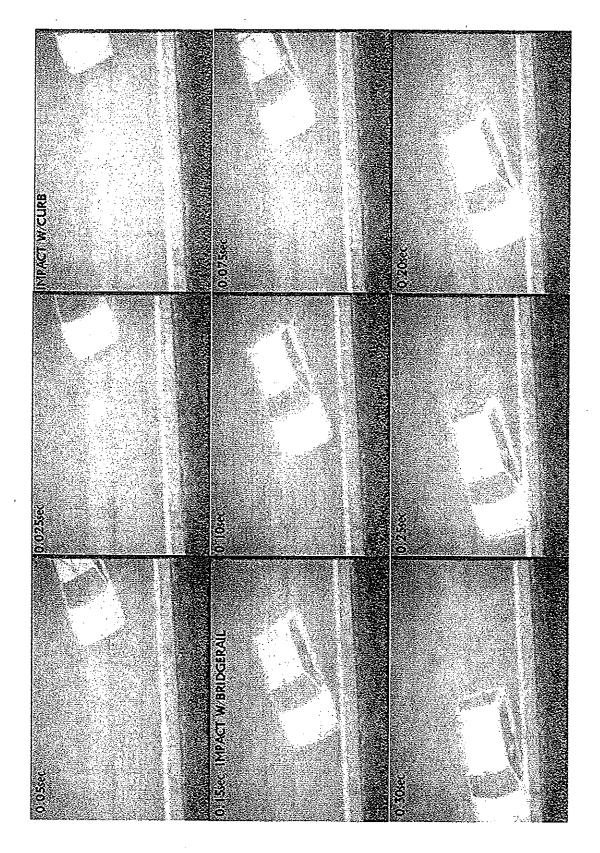


Figure 9. Overhead sequential photographs - Test NETC-1.

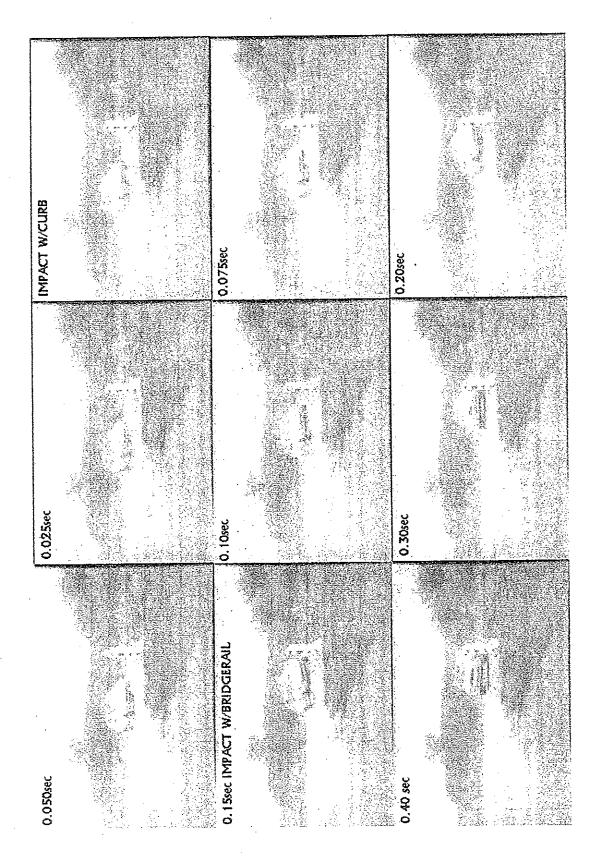
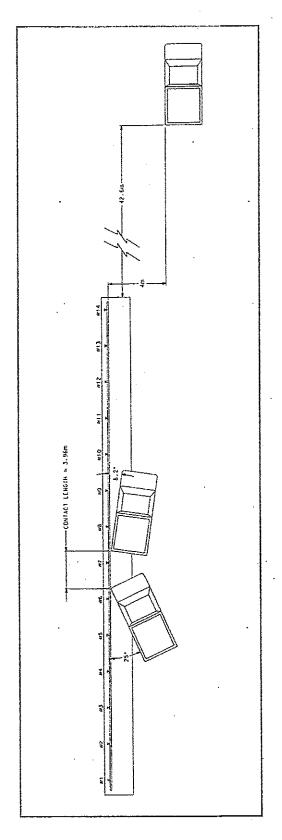


Figure 10. Sequential photographs - Test NETC-1.



4. General Information		7. Test Vehiele (Continued)		10. Ridedown Acceleration (g's)	
Test Agency	Southwest Research Institute	Mass (kg) Dummy(s)	75	y-direction	*
Test Number	NETC-2	Mass (kg) Gross Static	2,109	11. Test Article Descetion (mm)	
Test Date	11/20/97	8. Impact Conditions		Dynamic	25 (est.)
S. Test Article		Speed (km/h)	100.0	Permuncut	13
Туре	Bridge Rail	Angle (deg)	25.0	12. Vehiele Damage	
Installation Length (m)	34.1	9. Exit Conditions		Exterior	
Barrier	4 Bar, Sidewalk-Mounted	Speed (km/h)	17	VDS	11-FL-3
6. Soll Type and Condition	N/A	Angle (deg)	8.2	CDC	11FLEE3
7. Test Vehicle		10. Occupant Risk Values		Interior	
Type	Production	Impact Velocity (m/s)		OCDI	LF0000000
Designation	2000P	x-direction	3.99	13. Post-Impact Vehicular Behavior	
Model	1991Ford F-250	y-direction	*	Maximum Roll Angle (deg)	20 Approximate
Mass (kg) Curb	2,034	Ridedown Acceleration (g's)		Maximum Pitch Angle (deg)	15 Approximate
Mass (kg) Test Inertial	2,034	X-direction	-2.55	Maximum Yaw Angle (deg)	NA

*No data - vehicle lateral accelerometer malfunctioned during test.

Figure 11. Impact sequence and summary of test conditions and results - Test NETC-2.

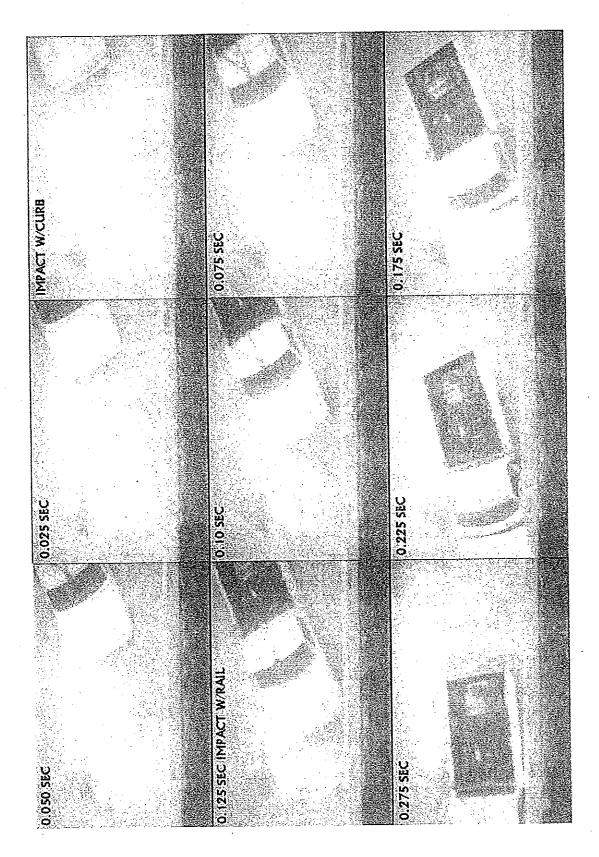


Figure 12. Overhead sequential photographs - Test NETC-2.

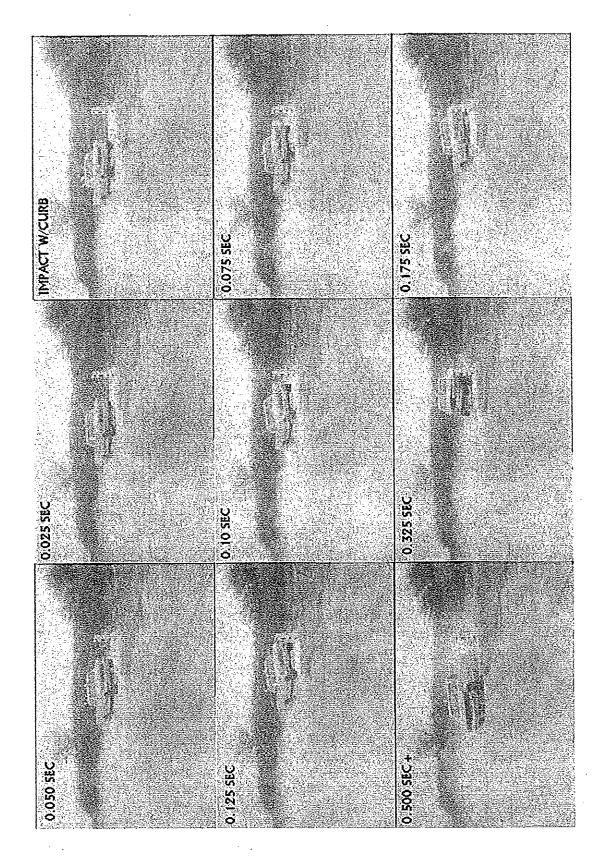
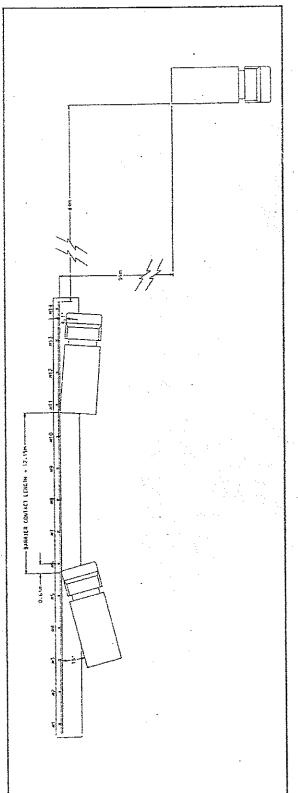


Figure 13. Sequential photographs - Test NETC-2.



4. General Information		7. Test Vehicle (Continued)		10, Ridedown Acceleration (g's)	
Test Agency	Southwest Research Institute	Mass (kg) Dummy(s)	N/A	y-direction	14,30
Test Number	NETC-3	Mass (kg) Gross Static	8,108	11. Test Article Deflection (mm)	
Test Date	12/18/07	8. Impact Conditions		Dynamic	25
5. Test Article		Speed (km/h)	80	Permanent	13
Type	Bridge Rail	Angle (deg)	15.0	12. Vehiele Damage	
Installation Length (m)	34.1	9, Exit Conditions		Exterior	
Barrier	4 Rails, Sidewalk-Mounted	Speed (km/h)	57.6	VDS	N/A
6. Soil Type and Condilion	N/A	Angle (deg)	4.1	CDC	N/A
7. Test Vehicle		10. Occupant Risk Values		Interior	
Type	Production	Impact Velocity (m/s)		OCDI	NA
Designation	80008	x-direction	1.65	13. Post-Impact Vehicular Behavior	
Madel	1993 International 4600 L.P	y-direction	-2,89	Maximum Roll Angle (deg)	20 Approximate
Mass (kg) Curb	8,108	Ridedown Acceleration (g's)		Maximum Pitch Angle (deg)	5 Approximate
Mass (kg) Test Inertial	8,108	X-direction	-8.95	Maximum Yaw Angle (deg)	N/Λ

Figure 14. Impact sequence and summary of test conditions and results - Test NETC-3.

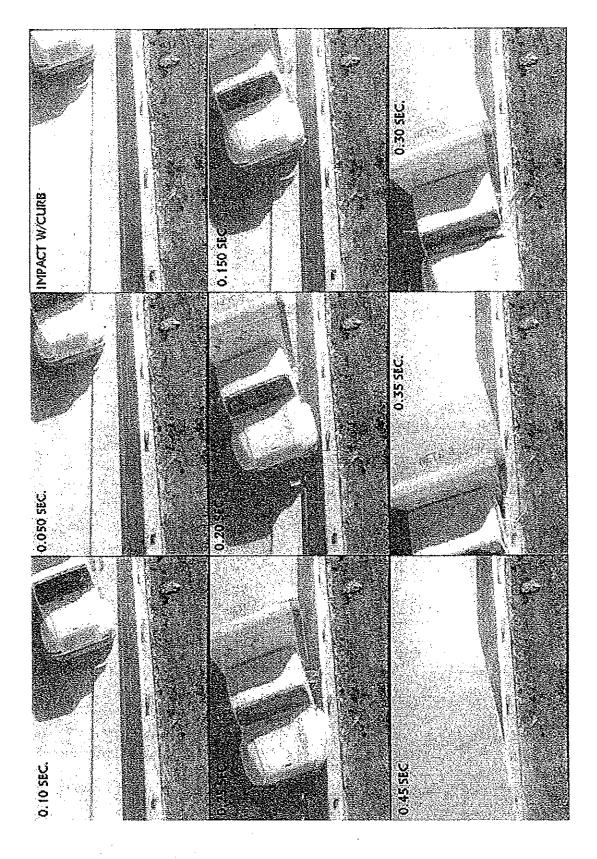
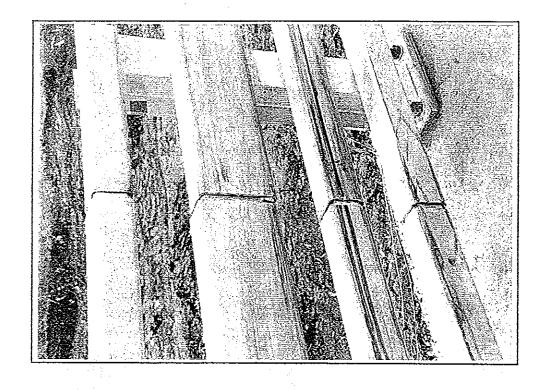


Figure 15. Overhead sequential photographs - Test NETC-3.

Figure 16. Sequential photographs - Test NETC-3.



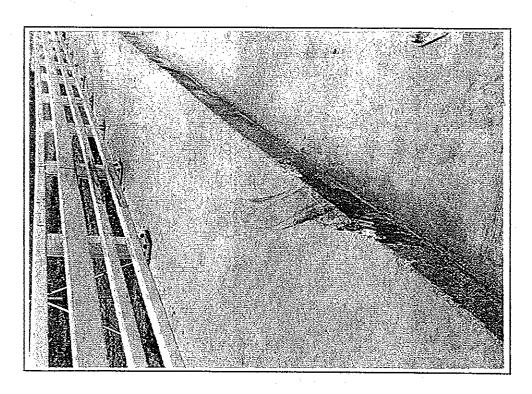
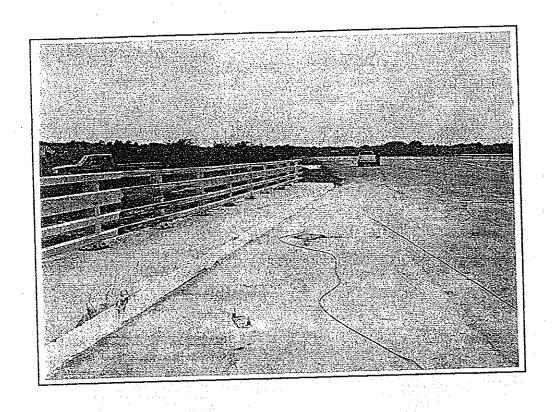


Figure 17. Barrier damage photographs - Test NETC-1.



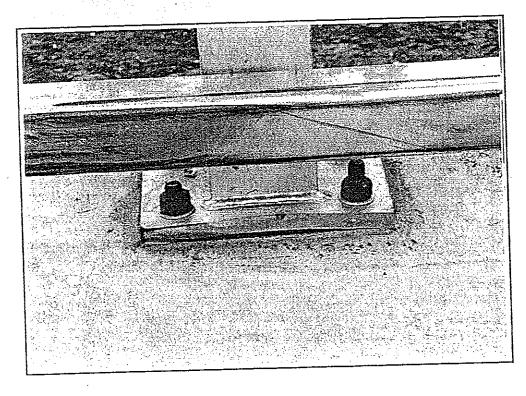
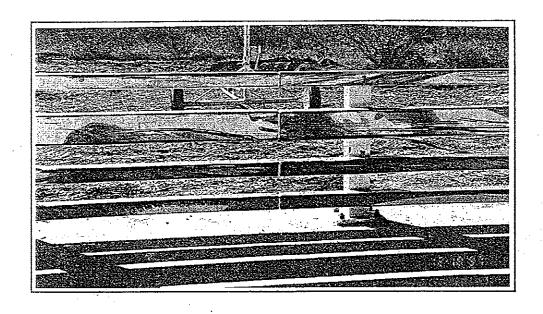


Figure 18. Barrier damage photographs - Test NETC-2.



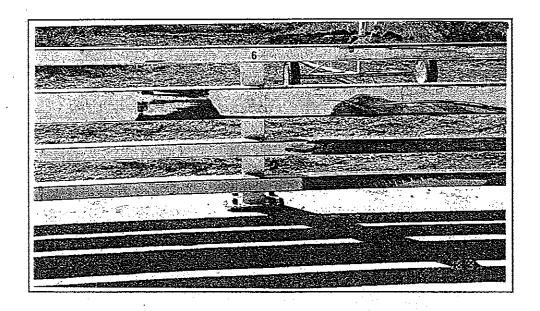
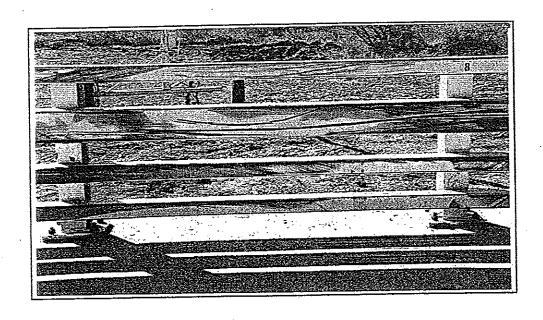


Figure 19. Barrier damage photographs - Test NETC-3.



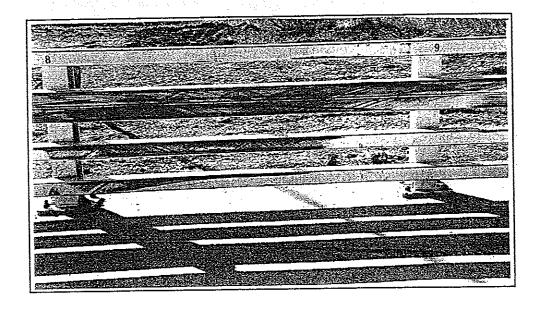
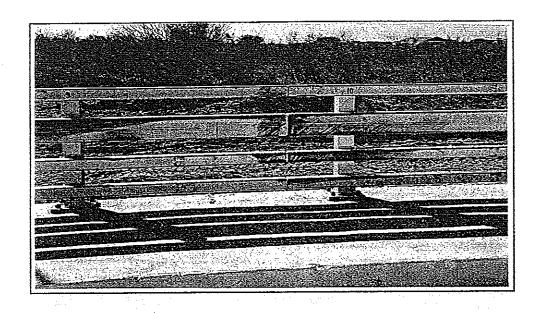


Figure 19. Barrier damage photographs - Test NETC-3 (continued).



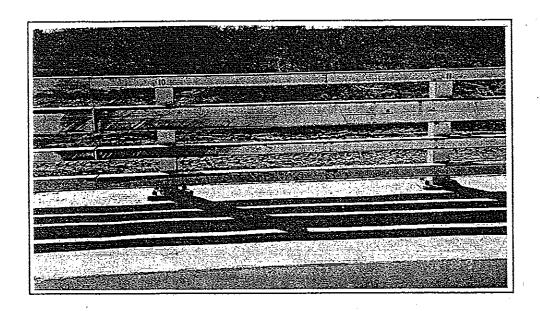
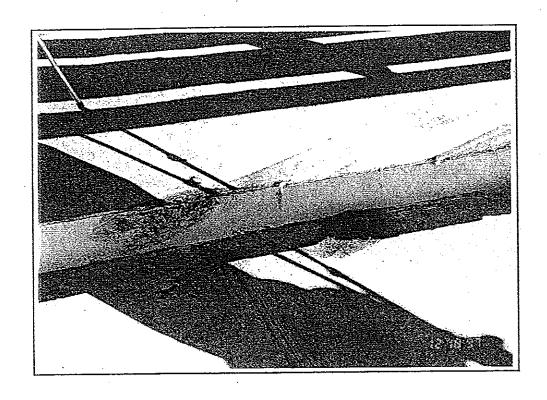


Figure 19. Barrier damage photographs - Test NETC-3 (continued).



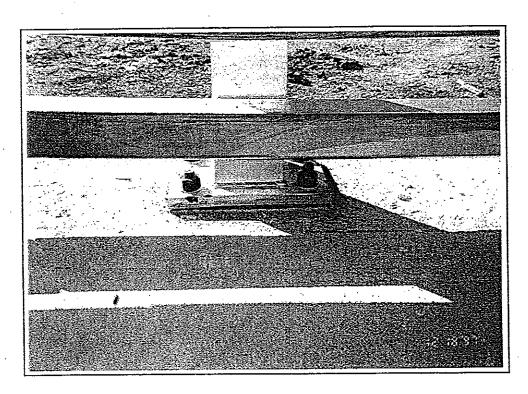


Figure 19. Barrier damage photographs - Test NETC-3 (continued).





Figure 20. Vehicle damage photographs - Test NETC-1.



Figure 20. Vehicle damage photographs - Test NETC-1 (continued).





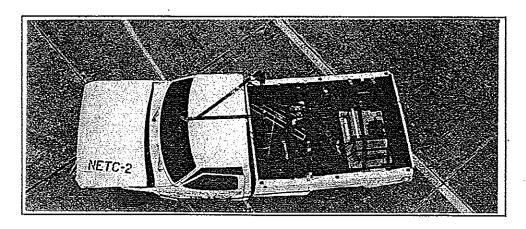


Figure 21. Vehicle damage photographs - Test NETC-2.



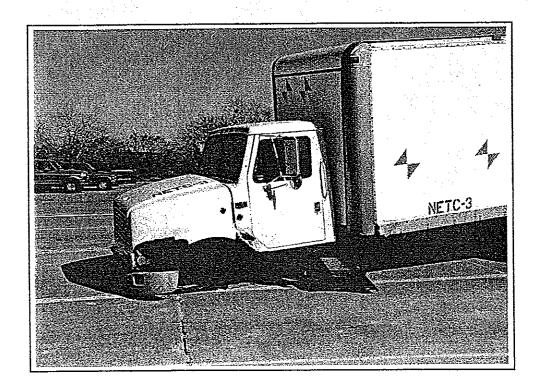


Figure 22. Vehicle damage photographs - Test NETC-3.

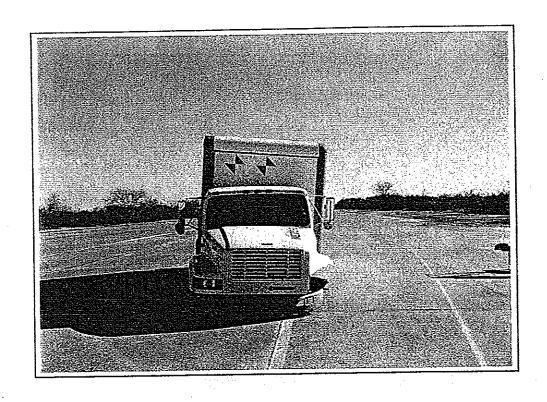
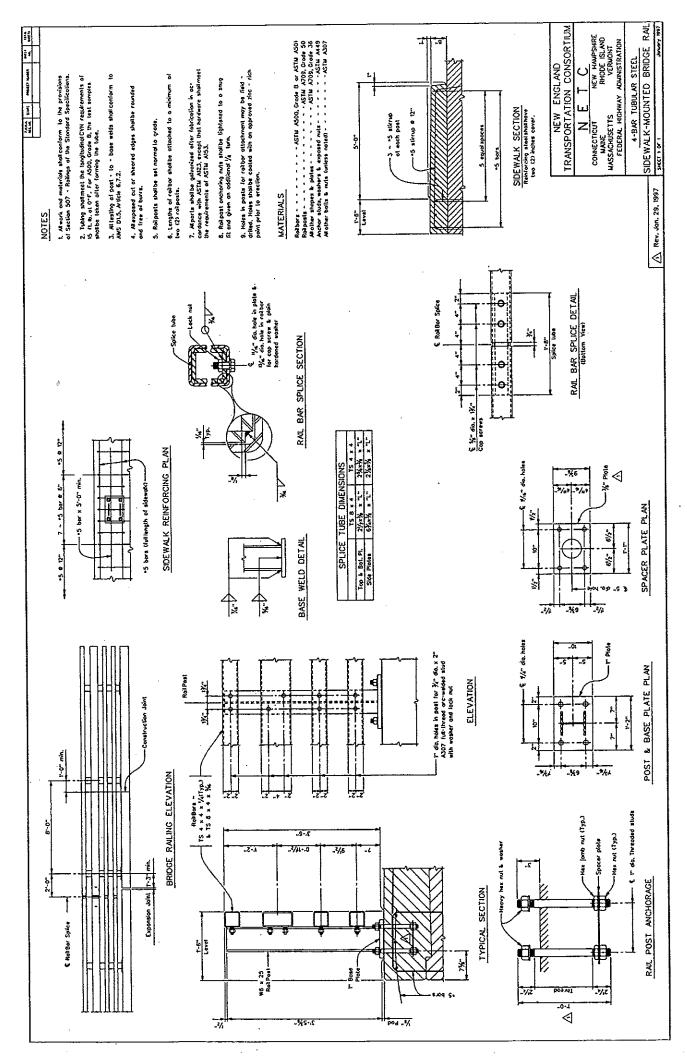
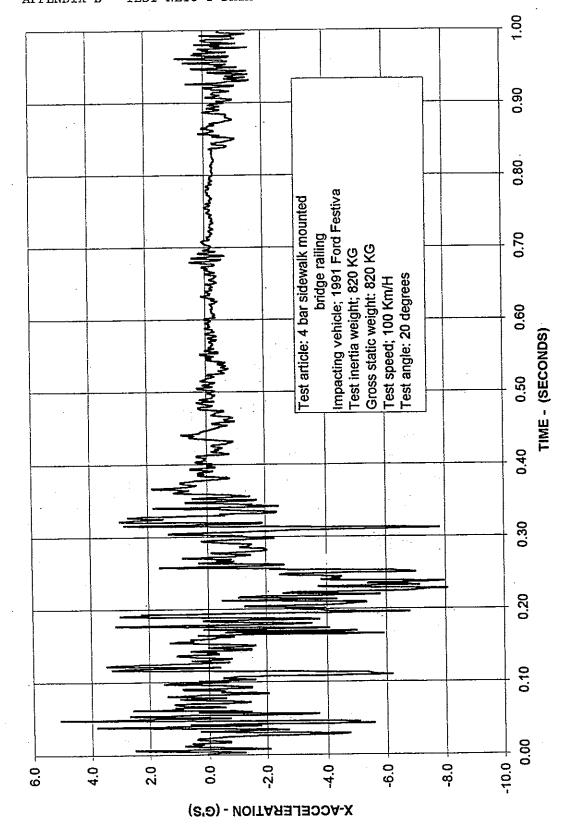




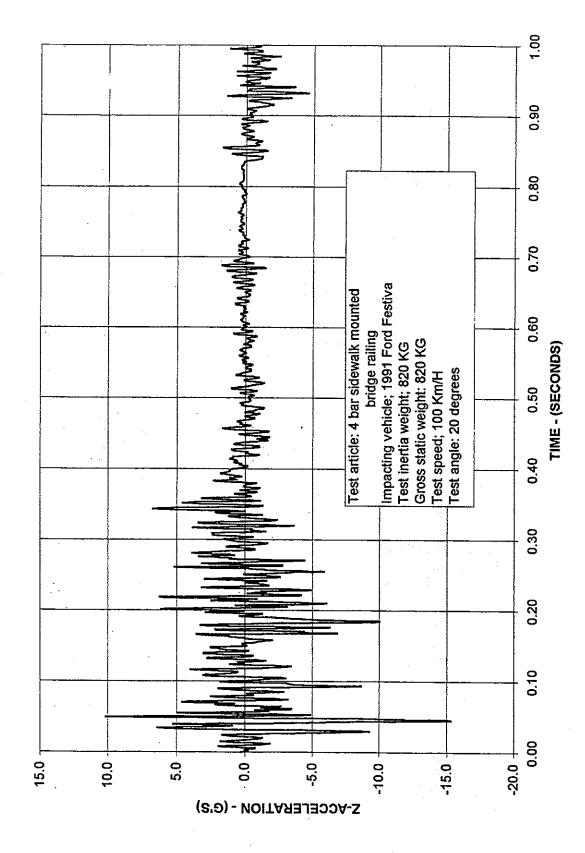
Figure 22. Vehicle damage photographs - Test NETC-3 (continued).



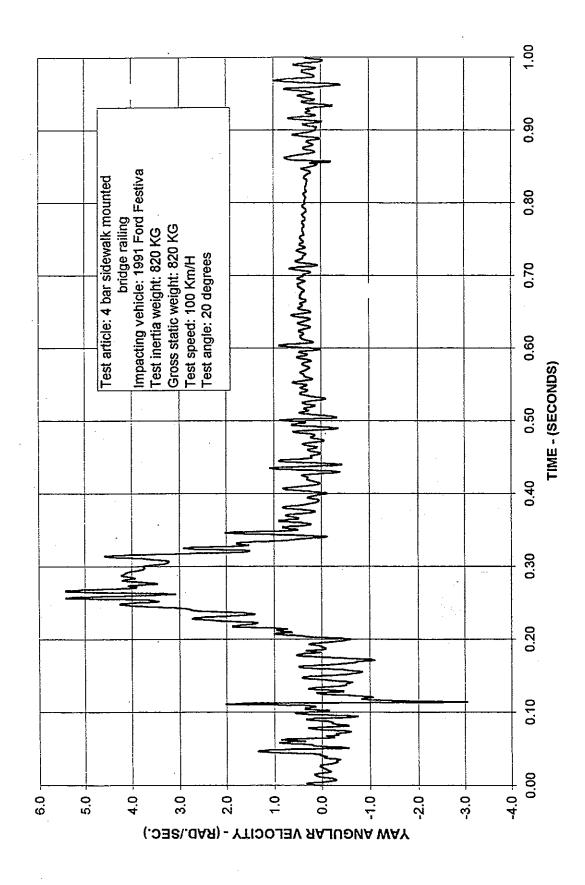
APPENDIX A - NETC CRASH TEST STEEL BRIDGE RAILING DRAWING



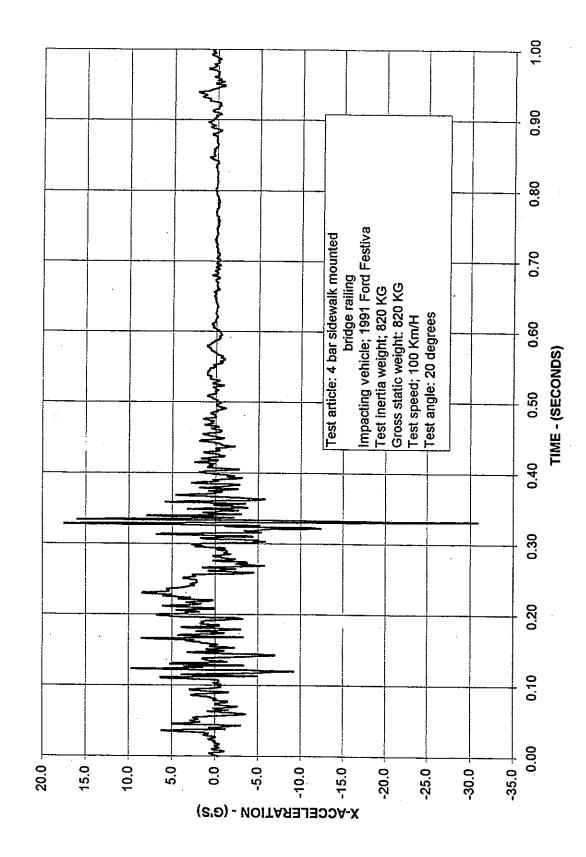
Vehicle C.G. longitudinal accelerometer plot - Test NETC-1.



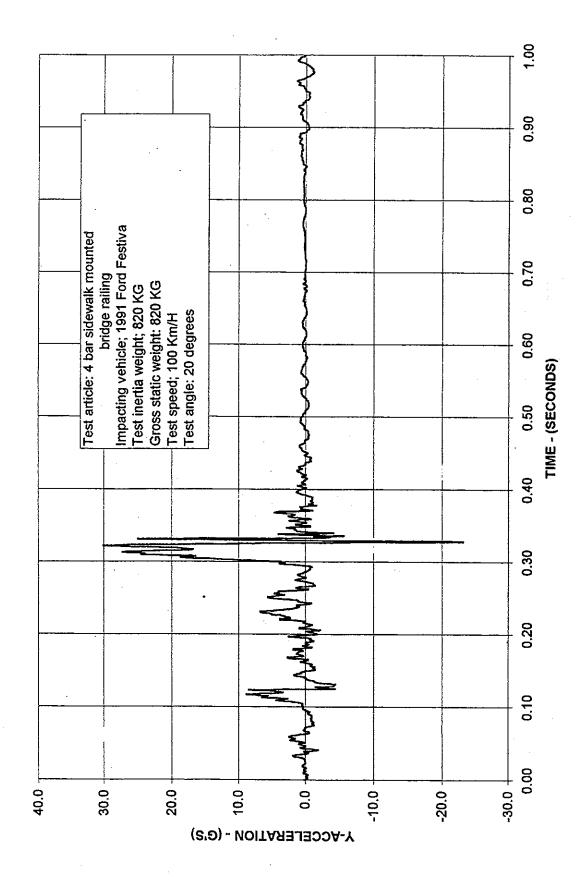
Vehicle C.G. vertical accelerometer plot - Test NETC-1.



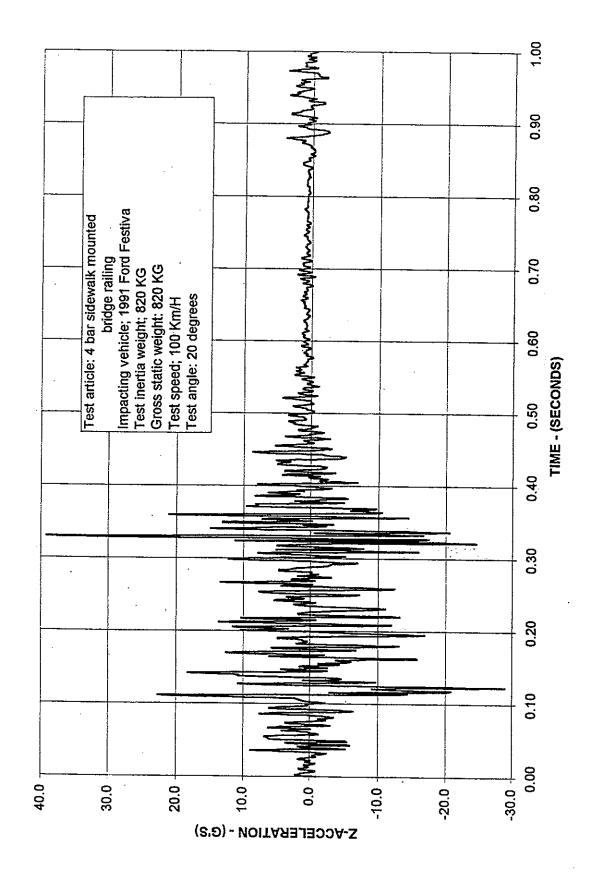
Rate gyro plot - Test NETC-1.



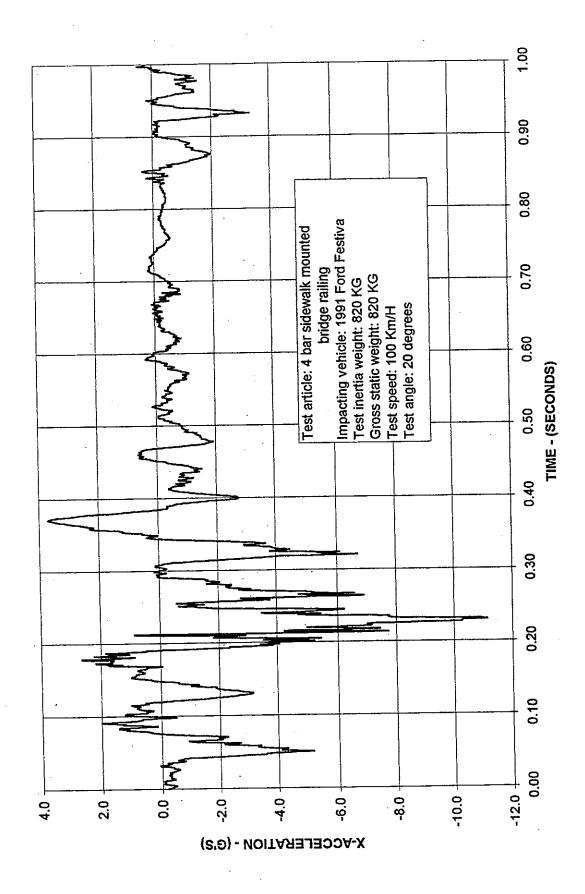
Rear axle longitudinal accelerometer plot - Test NETC-1.



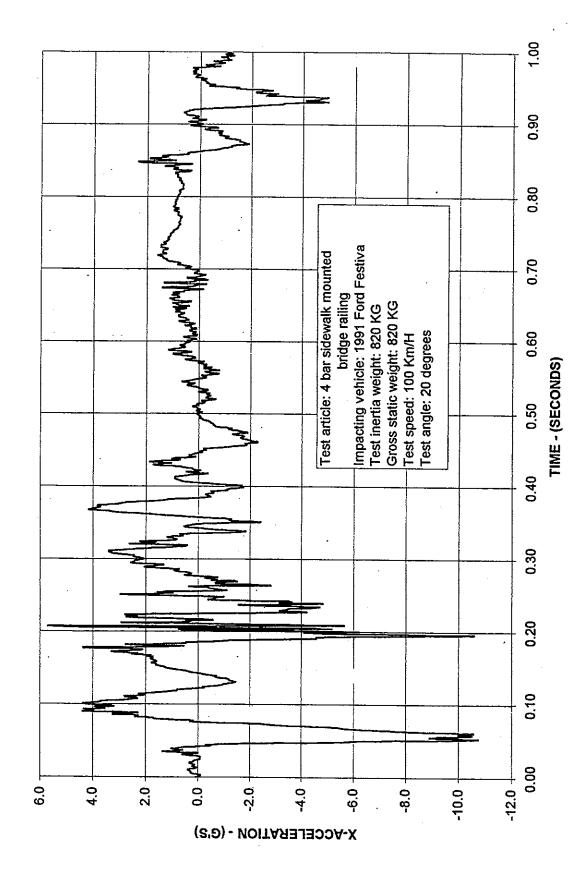
Rear axle lateral accelerometer plot - Test NETC-1.



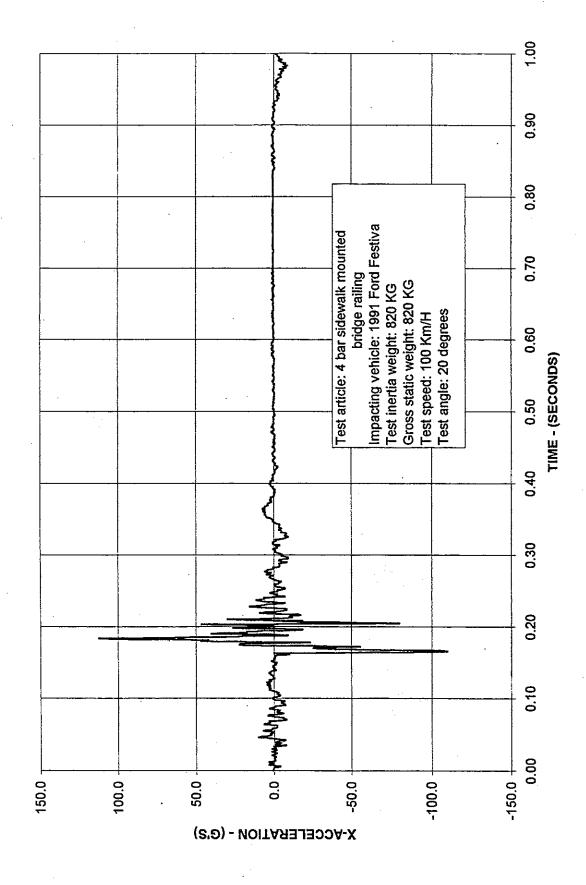
Rear axle vertical accelerometer plot - Test NETC-1.



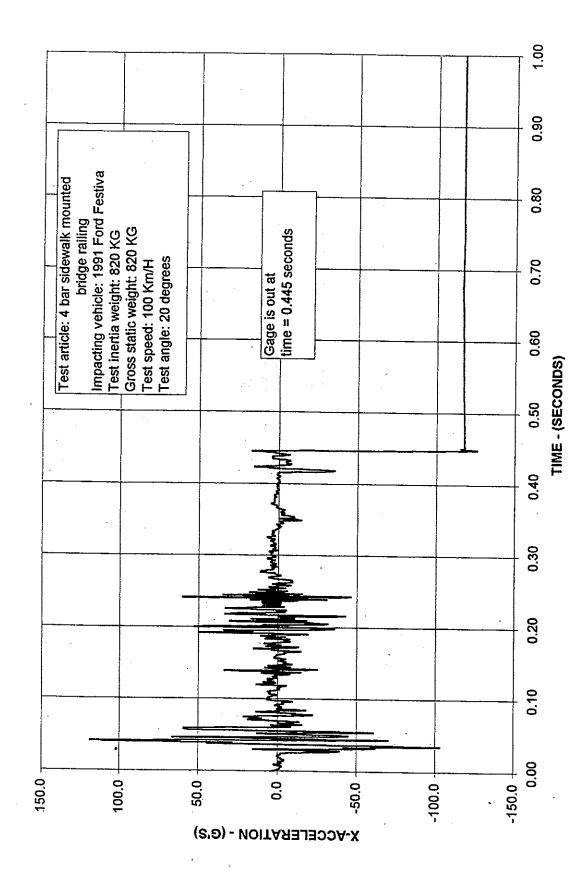
Top of engine longitudinal accelerometer plot - Test NETC-1.



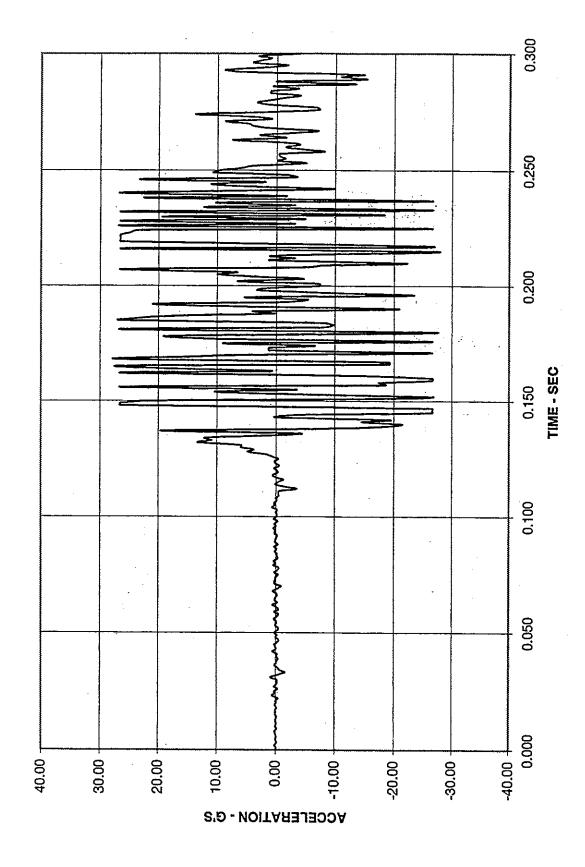
Bottom of engine longitudinal accelerometer plot - Test NETC-1.



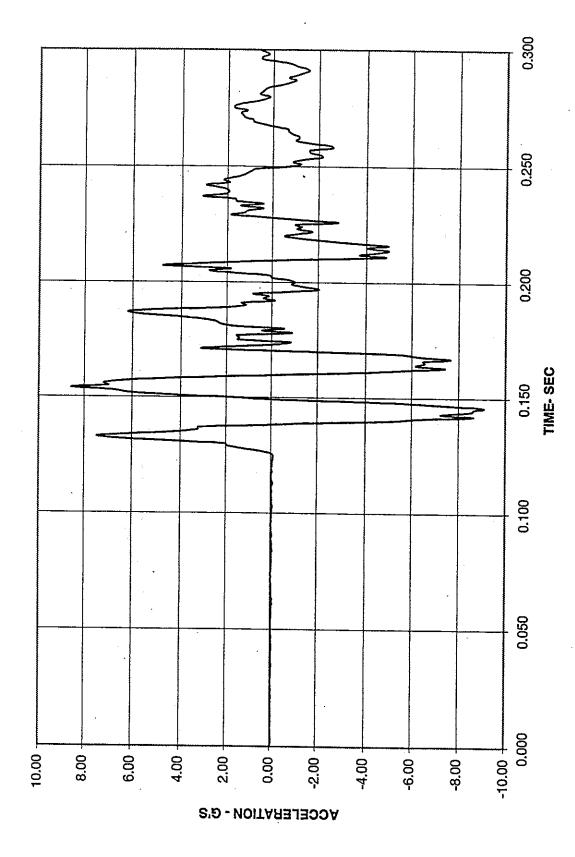
Right front disc brake longitudinal accelerometer plot - Test NETC-1.



Left front disc brake longitudinal accelerometer plot - Test NETC-1.



Top of post 7 lateral accelerometer plot - Test NETC-1.



Bottom of post 7 lateral accelerometer plot - Test NETC-1.

APPENDIX B - TRANSDUCER DATA WITH CALCULATED VEHICLE KINETICS AND OCCUPANT RISK SUMMARIES

Test ID	NETC-1
Test Date	11/18/97
Vehicle Type	820 C
Occupant Risk Summ	ary from Film Analsyis

Time	Vehicle Acce	N. (G'S)	Occup, Vel.	(FPS)	Occup. Disp	. (F)
(S)	LONG.	LAT.	LONG.	LAT.	LONG.	LAT.
0.000	-2.02	3.73	0.00	0.00	0.00	0.00
0.010	-2.61	4.32	0.33	-0.94	0.00	0.00
0.020	-3.05	4.92	0.80	-2.10	0.01	-0.02
0.030	-3.36	5.48	1.39	-3.51	0.02	-0.05
0.040	-3.54	5.97	2.06	-5.12	0.03	-0.09
0.050	-3.58	6.37	2.72	-7.01	0.04	+0.14
0.060	-3.51	6.68	3.39	-9.02	0.08	-0.22
0.070	-3.33	6.67	3.95	-11.26	0.11	-0.35
0.080	-3.07	6.87	4.45	-13.30	. 0.15	-0.46
0.090	-2.74	6.92	4.89	-16.61	0.17	-0.62
0.100	-2,37	6.80	5.10	-18.48	0.17	-0.80
0.110	-1.98	6.62	5.22	-20.95	0.22	-1.00
0.120	-1.58	6.37	5.20	-23.36	0.25	-1.23
0.130	-1.20	5.80	5.10	-25.65	0.26	-1.50
0.140	-0.86	5.35	4.84	-27.85	0.28	-1.75
0.150	-0.55	4.82	4.56	-27.85 -29.85	0.27	-2.03
0.160	-0.29	4.23	4.21	-23.65 -31.65	0.27	-2.05 -2.35
0.170	-0.08	3.65	3.82	-33,35	0.26	-2.55 -2.68
0.180	0.07	3.12	3.45	-34.70	0.25	-2.00 -3.02
0.190	0.17	2.56	3.04	-35.95	0.23	
0.200	0.17	2.05	2.71	-35,96	0.23	-3.40
0.210	0.22	1.58			0.20	-3.81
0.220	0.19	1.20	2.40	-37.80	0.19	-4.15
0.230	0.19	0.86	2.12	-38.52	0.18	-4.51
0.240	0.12	0.55	1.90	-39.05	0.15	-4.92
0.250	-0.10		1.72	-39.42	0.14	-5.32
0.260		0.37	1.62	-39.70	0.12	-5.70
0.270	-0.24 -0.39	0.23	1.58	-39.92	0.09	-6.12
0.280	-0.55	0.16	1.58	-40.01	0.09	-6.46
0.290	-0.72	0.15	1.60	-40.15	0.07	-6.91
		0.16	1.65	-40.23	0.06	-7.25
0.300	-0.87	0.25	1.78	-40.25	0.05	-7.83
0.310	-1.02	0.35	2.00	-40.53	0.05	-8.12
0.320	-1.16	0.50	2.10	-40.54	0.04	-8.50
0.330	-1.28	0.65	2.30	-40.72	0.02	-8.87
0.340	-1.38	0.78	2.52	-40.92	0.00	-9.11
0.350	1.45	0.93	2.71	-41.20	-0.02	-9.25
0.360	-1.49	1.07	2.96	-41.51	-0.04	-9 .86
0.370	-1.51	1.15	3,20	-41.81	-0.07	-10.15
0.380	-1.50	. 1.21	3,35	-42.18	-0,09	-10.89
0.390	-1.47	1.20	3,54	-42.57	-0.10	-11.35
0.400	-1.41	1.22	3.70	-42.89	-0.13	-11.78
0.410	-1.33	1.13	3.87	-43.36	-0.16	-12.20
0.420	-1.24	0.98	4.05	-43.78	-0.19	-12.73
0.430	-1.13	0.85	4.15	-44.09	-0.24	-13.01
0.440	-1.02	0.63	4.23	-44,37	-0.27	-13.55
0.450	-0.90	0.40	4.35	-44.56	-0.32	-13.68
0.460	-0.80	0.15	4.38	-44.75	-0.39	-14.03
0.470	-0.70	-0.11	4.45	-44.81	-0.44	-14.53
0.480	-0.62	-0.32	4.46	-44.82	-0.46	-14.92
0.490	-0.57	-0.49	4.50	-44.72	-0.47	-15.40
0.500	-0.53	-0.65	4.55	-44.58	-0.50	-15.98
Occup, Risk Fact	ors		Time (S)		Valocity (FPS	٠ .

Occup. Risk Factors	Time (S)	Velocity (FPS)	Convert to M/S	
Long. Vel. after 2.0 ft. Disp. Lat, Vel after 1.0 ft. Disp.	0.500 4.55° 0.110 -20.95		1.39 6.39	
Max. Accel. after Occup, impact	Time (S)	ACC. (G's)		
Lat. Acceleration	0.120	6.37		

^{*} Occup, did not travel req'd hypothetical distance

Test ID -- NETC-1 Test Date -- 11/18/97 Vehicle Typ: 820C

TIME (S)	Vehicle Accel. (G's)		Heading	Veh. Ve		Veh. Disp (M)		
(0)	LONG. L	AT.	Angle (deg)	LONG.	LAT.	x	у	
0.000	-2.05	3.63	19.85	27.56	0.30	-1.69	4.40	
0.010	-2.63	4.35	19.19	27.33	0.38	-1.53	-1.16	
0.020	-3.08	4.69	18.32	27.06	0.44 ⁻	-1.30	-1.08 -1.01	
0.030	-3.36	5.43	17.30	26.75	0.46	-1.07	-0.93	
0.040	-3.56	5.97	16.12	26.42	0.50	-0.77	-0.87	
0.050	-3.58	6.37	15.08	26.09	0.48	-0.52	-0.81	
0.060	-3.50	6.36	14.30	25.72	0.52	-0.27	-0.76	
0.070	-3.21	6.67	12.56	25.43	0.52	-0.03	-0.71	
0.080	-3.02	6.95	10.65	25.10	0.51	-0.01	-0.68	
0.090	-2.81	6.90	9.20	24.88	0.51	0.00	-0.64	
0.100	-2.35	6.81	7.53	24.62	0.50	0.46	-0.60	
0.110	-1.97	5.33	5.62	24.42	0.48	0.71	-0.59	
0.120	-1.59	4.80	3.25	24.26	0.46	0.94	-0.58	
0.130	-1.21	4.24	2.36	24.14	0.43	1.17	-0.59	
0.140	-0.86	3.65	1.11	24.04	0.40	1.42	-0.61	
0.150	-0.55	3.12	0.06	24.02	0.34	1.65	-0.62	
0.160	-0.29	2.65	0.03	23.95	0.29	1.89	-0.64	
0.170	-0.12	5.03	-0.06	23.60	0.21	2.12	-0.65	
0.180	-0.07	1.62	-0.13	23.64	0.14	2.36	-0.66	
0.190	-0.02	1.20	-1.10	23.96	0.05	2.58	-0.67	
0.200	0.12	0.86	-2.36	23.97	0.03	2.81	-0.68	
0.210	0.22	0.56	-2.96	24.00	0.01	3.05	-0.70	
0.220	0.23	0.39	-3.45	24.01	-0.01	3.27	-0.74	
0.230	0.19	0.23	-3.98	24.03	-0.03	3.51	-0.76	
0.240	0.12	0.15	-4.33	24.03	-0.31	3.74	-0.76	
0.250	0.02	0.14	-5.79	24.02	-0.50	3.97	-0.81	
0.260	0.09	0.18	-6,45	24.00	-0.62	4.21	-0.82	
0.270	-0.05	0.25	-7.56	23.97	-0.61	4.43	-0.85	
0.280	-0.20	0.35	-8.86	23.89	-0.75	4.74	-0.88	
0.290 0.300	-0.53	0.52	-9.88	23.86	-0.83	4.83	-0.93	
0.300	-0.86	0.63	-10.10	23.47	-0.90	4.97	-0.93	
0.310	-1.02	0.82	-10.31	23.68	-0.95	5.36	-0.96	
0.320	-1.15 1.25	0.93	-10.51	23.57	-1.02	5.59	-0.98	
0.340	-1.25 1.22	1.03	-10.73	23.44	-1.11	5.82	-1.06	
0.350	-1.32 -1.45	1.15	-10.76	23.31	-1.13	6.04	-1.09	
0.360	-1.45 -1.49	1.18	-11.26	23.16	-1.15	6.27	-1.18	
0.370	-1.49 -1.51	1.23	-11.45	23.01	-1.17	6.54	-1.16	
0.380	-1.50	1.22	-11.47	22.86	-1.18	6.72	-1.19	
0.390	-1.49	1.15	-11.77	22.68	-1.18	6.93	-1.21	
0.400	-1.49 -1.41	1.20	-12.02	22.55	-1.21	7.16	-1.23	
0.410	-1.41 -1.33	1.19	-12.02	22.37	-1.20	7.46	-1.26	
0.420	-1.33 -1.23	1.12 1.00	-13.06	22.26	-1.21-	7.59	-1.28	
J. 120	- 1, <u>2</u> 0	1,00	-13.25	22.13	-1.23	7.80	-1.34	

TIME	Vehicle Accel. (G's)		Heading	Veh. Vel.	(M/S)	Veh. Disp (M)		
(S)	LONG. 1	_AT.	Angle (deg)	LONG. L	LONG. LAT.		У	
		 . ,						
0.430	-1.12	0.90	-13.49	22.00	-1.27	7.71	-1.37	
0.440	-1.02	0.85	-14.01	21.89	-1.31	8.22	-1.46	
0.450	-0.95	0.65	-14.23	21.81	-1.37	8.44	-1.51	
0.460	-0.90	0.39	-14.56	21.79	-1.44	8.65	-1.53	
0.470	-0.70	0.13	-14.87	21.70	-1.47	8.98	-1.57	
0.480	-0.62	-0.01	-15.00	21.61	-1.53	9.07	-1.59	
0.490	-0.55	-0.40	-14.98	21.54	-1.64	9.28	-1.66	
0.500	-0.61	-0.61	-15.15	21.47	-1.91	9.43	-1.71	
0.510	-0.65	-0.66	-15.35	21.41	-2.09	9.61	-1.76	
0.520	-0.55	-0.65	-15.63	21.35	-2.21	9.88	-1.81	
0.530	-0.60	-0.50	-15.82	21.29	-2.27	10.10	<i>-</i> 1.83	
0.540	-0.63	-0.07	-15.87	21.23	-2.45	10.30	-1.89	
0.550	-0.77	0.09	-15.88	21.16	-2.60	10.45	-1.91	
0.560	-0.75	0.54	-15.97	21.10	-2.65	10.68	-1.94	
0.570	-0.96	1.09	-16.06	20.99	-2.67	10.91	-1.99	
0.580	-1.01	1.63	-16.23	20.89	-2.16	11.10	-2.05	
0.590	-1.06	2.08	-16.41	20.78	-2.08	11.31	-2.10	
0.600	-1.03	2.23	-16.56	20.66	-2.06	11.71	-2.12	
0.610	-0.97	2.41	-16.77	20.55	-1.90	11.91	-2.15	
0.620	-0.69	1.93	-16.86	20.44	-1.86	12.17	-2.19	

HIGHEST 50-MS AVG. ACCEL.

		TIMI	E (SEC)
	G'S	START	END
	***************************************	·	
LONG.	-3.43	0.025	0.075
LAT.	6.94	0.065	0.115

TEST ID ----- NETC-1
TEST DATE ---- 11-18-97
VEHICLE CLASS - 820C
IMPACT SPEED -- 27.78 M/S

TIME (SEC)	(VEL. X	CG ACC	CEL(G' Z	S)) R	(VEL.	REAR Y	ACCEL	(G'S)) R
.410	.2	.0	.7	.8	.4	.5	-1.7	1.8
.420	4	. 0	-1.0	1.1	1.7	1	3,9	4.2
.430	7	.0	7	1.0	.8	1.0	5.0	5.1
.440	.7	.0	-1.6	1.8	7	7	-5.2	5.3
.450	3	.0		.3	4	3	-2.0	2.1
.460	9	.ŏ	1 .1	1.0	6	.9	1	1.1
.470	3	.0	3	.4	.3	4	.2	.6
.480	1	.ŏ	.0	.1	.1	4	1	.4
.490	.1	.0	.3	.3	7	.4	2.3	2.5
.500	2	.0	2	.3	4	.5	.2	.7
.510	.1	.0	8	.8	.8	1	2.7	2.8
.520	2	.0	-1.1	1.2	.2	4	2.9	3.0
.530	6	.0	6	.8	3	.4	1	.6
.540	6	.0	4	.7	1.1	.1	.5	1.2
.550	1	.0	.2	.2	.1	3	4	.5
.560	3	.0	.4	.5	-1.0	.6	1.6	2.0
.570	2	.0	.2	.3	.2	.3	.8	.9
.580	.0	.0	4	.4	1.1	2	.8	1.4
.590	2	.0	.7	.7	4	.1	.3	.5
.600	.0	.0	.0	. 6	3	.4	1.0	
.610	2	.0	.0	.4	s .5	.0		1.1
.620	2	.0	.3	.4	.5 1		1.5	1.6
.630	1	.0	.1	.1	.0	.0 .4	.8	.8
.640	2	.0	.4	. <u>1</u> . 4			.8	1.0
.650	3	.0	.1	.4	.0 .3	1 1	.5	.5
.660	4	.0	~.6	.3 .7	3 3		1.2	1.2
.670	1	.0	.4	.4	3 1	.3	.7	.8
.680	.3	.0	1.3	1.4		.1 2	.6	.7
.690	1	.0	.0	.1	.5		1.4	1.5
.700	2	.0	3	.3	1 3	.2	.2	.3
.710	1	.0	.5	. 3 . 5		.1	1.1	1.2
.720	3	.0	.3	.4	3	.0	.3	.4
.730	2	.0	.1	.2	.1	.0	.6	.6
.740	3	.0	.3	. 4 . 4	.3	.1	1.0	1.1
.750	2	.0	.4	.4	.0	. 2	.7	. 7
.760	1	.0	.2	.2	1	.1	.7	. 7
.770	2	.0	.3		.0	.3	. 9	.9
.780	2 1			.4	. 2	.4	.7	.8
.790	1 2	.0	.2	.2	1	.1	.9	.9 .8
.800	3	.0	.0	.2	1	.1	.8	.8
.810	3 3	.0	.3 .2	.4	.2	.3	.7	.8
.820	3 3	.0	.2	.3	.0	.3	.5	.6
	3 3	.0		.4	.1	.3	.8	.8
.830		.0	.3	.4	.1	.3	.5	. 6
.840	8	.0	-1.1	1.4	.0	. 2	.1	.2

TIME	(VEL.		CEL(G				ACCEL.~	(G'S) ~	-)
(SEC)	X	Y	Z	R	X	Y	z	R	
.850	-1.0	.0	-1.5	1.9	.3	.4	.5	.7	
.860	3	.0	7	.8	.3	.7	2	. 8	
.870	4	.0	5	.6	.2	.5	.3	.6	
.880	8	.0	1	.8	.6	.8	4.0	4.1	
.890	6	.0	5	.7	. 8	.9	-2.1	2.4	
.900	7	.0	3	.7	.6	4	.6	. 9	
.910	~.6	.0	.0	.6	.1	.4	1.1	1.2	
.920	1	.0	5	.5	4	.8	.3	. 9	
.930	-1.5	.0	-1.1	1.8	1.0	. 9	6	1.5	
.940	-1.3	.0	-3.5	3.8	1.7	4	3.3	3.7	
.950	6	.0	3	.7	2	.0	1.3	1.3	
.960	.5	.0	-1.6	1.6	.3	1.0	1.9	2.1	
.970	8	.0	3	.8	.3	2	5	. 6	
.980	.3	.0	-1.3	1.3	.2	-1.0	1.2	1.6	
.990	-1.0	.0	6	1.2	.3	.6	.6	.9	
MAXIM	NUM VALUES	AND TI	ME OF	CCURANCE					
			SEC	Y	-SEC	Z	SEC	R	SEC
- VEL. CG ACCE	L(G'S) -	8.1	.228	.0 1	.000 -	-15.8	.046	16.8	.046
VEL. REAR ACC	EL(G'S)	-32.1	.332	30.1	.322	41.1	.330	43.3	.329

TEST ID ----- NETC-1
TEST DATE ---- 11-18-96
VEHICLE CLASS - 820C
IMPACT SPEED -- 27.78 M/S

			BRAKE	
TIME (S)	ENGIN BLOC TOP BOT	K CAL TOM RIGHT	IPERS LEFT	INSTRUMENT PANEL
.000 .010 .020 .030 .040 .050 .060 .070 .080 .090 .100 .110 .120 .130 .140 .150 .160 .170 .180 .200 .210 .220 .240 .250 .250 .260 .270 .280 .300 .310 .320 .330 .340	2136 -5.2 -2.2 -10 -2.2 -4 .9 1.5 .6 .82 -3.1 -1.4 .3 .5 1.7 1.3 .4 -3.6 -2.9 -5.0 -11.1 -3.6 -1.2 -3.2 -5.0 -1.5 -6 -1.2 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6	.1 1.1 .4 .4 .3 .0 .4 1.6 .8 -1.5	3.0 -1.4 15.2 -38.7 32.7	
.350	.4 -	1.3 1.4	-10.8	.0

		AC	CELERATIO		
				BRAKE	
TIME		BLOCK		IPERS	INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
.360	2.2	1.0	6.6	-1.5	.0
.370	3.6	3.9	4.3	1.9	.0
.380	1.5	1.7	2.2	2.4	.0
.390	4	- 4	4	.7	.0
.400	-2.8	-1.7	2.2	.9	.0
.410	6	. 9	.4	6	.ŏ
.420	6	.5	-1.7	-14.5	
.430	7	1.8	.0	-4.3	.0
.440	-1.3	.3	.7	-6.5	.0
.450	3	3	.5	-115.4	
.460	.6	-2.0			.0
.470	2		.3	-117.7	- 0
		-1.7	1.0	-117.7	.0
.480	-1.7	-1.3	.7	-117.6	.0
.490	-1.3	4	.1	-117.5	.0
.500	8	.1	1	-117.4	.0
.510	-,2	.3	. 4	-117.2	.0
.520	5	6	1	-117.1	.0
.530	2	.0	.5	-117.1	.0
.540	-,2	. 5	.2	-117.1	.0
.550	4	3	.6	-116.9	.0
.560	6	8	1	-116.8	.0
.570	9	.0	5	-116.8	.0
.580	5	.5	1.1	-116.8	.0
.590	.0	.8	.3	-116.8	.0
.600	.1	.5	.3	-116.7	. 0
.610	4	.3	3	-116.7	.ŏ
.620	7	.3	.3	-116.6	.0
.630	5	.4	.2	-116.5	.0
.640	2	.8	.8	-116.5	
.650	2	. 8	.6	-116.5	.0
.660	.0	1.0	.0	-116.2	.0
.670	. o	.6	.2	-116.2	.0
.680	6	.8			.0
.690	8		1.1	-116.3	.0
.700	- 4	.0	.5	-116.4	.0
	.0	. 4	.3	-116.4	.0
.710		1.1	.6	-116.5	.0
.720	.2	1.5	.5	-116.6	.0
.730	.1	1.5	.7	-116.6	.0
.740	.0	1.2	.7	-116.7	.0
.750	3	1.1	.8	-116.8	0
.760	5	.9	.7	-116.8	.0
.770	4	. 8	.7	-116.7	.0
.780	2	.9	.8	-116.6	.0
.790	2	1.0	.5	-116.6	.0
.800	3	.9	.4	-116.6	.0

		ACC	ELERATIO	N-(G'S)	
			DISK	BRAKE	
TIME	ENGIN	BLOCK	CALI	PERS	INSTRUMENT
.(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
.810	4	.7	.6	-116.6	.0
.820	4	.7	.6	-116.6	.0
.830	3	.9	.8	-116.6	.0
.840	3	. 9	6	-116.5	.0
.850	1	1.0	1.1	-116.6	.0
:860	6	.5	.9	-116.6	.0
.870	-1.6	-1.2	1.5	-116.6	.0
.880	-1.6	-1.1	.8	-116.6	.0
.890	-1.2	9	.7	-116.6	.0
.900	3	1	1.0	-116.6	.0
.910	~.2	.1	.6	-116.6	.0
.920	2	.3	6	-116.6	.0
.930	-2.1	-3.8	.2	-116.7	.0
.940	9	-2.5	-2.3	-116.7	.0
.950	.2	-1.4	-1.1	-116.7	.0
.960	-1.1	2	-3.3	-116.7	.0
.970	-1.1	.3	-3.1	-116.7	.0
.980	-1.0	8	-8.0	-116.7	.0
. 990	1	-1.1	-3.4	-116.8	. 0

POST NO. 7 ACCELEROMETER DATA

<u> </u>	ACCELER	OMETER E	ATA -TES	T NETC-1	1
	}				
		POST 7	POST 7		
	<u> </u>	TOP	BOTTOM		İ
	TIME	ACCEL	ACCEL		<u> </u>
·	(SEC)	(G'S)	(G'S)		
					<u> </u>
	0.000	0.00	0.02		
	0.001	-0.05	-0.05		
	0.002	0.14	-0.06		
	0.003	-0.10	-0.06		
	0.004	-0.06	-0.06		
	0.005	0.03	-0.05	<u> </u>	
	0.006	-0.05	-0.05		
	- 0.007	0.04	-0.05		
<u> </u>	0.008	0.17	-0.03		
	0.009	-0.12	-0.05	· - ·	
	0.010	0.04	-0.05		
	0.011	-0.06	-0.06		
	0.012	-0.01	-0.05		
	0.013	0.00	-0.06		
	0.014	-0.12	-0.05		· 1
	0.015	0.04	-0.05		
	0.016	0.05	-0.05		
	0.017	0.04	-0.03		
	0.018	-0.09	-0.03		
	0.019	0.12	-0.05		i
	0.020	-0.06	-0.03		
	0.021	-0.03	-0.06		<u></u>
	0.022	-0.35	-0.06		
	0.023	0.53	-0.05		
	0.024	0.16	-0.06		
	0.025	0.22	-0.05	-	
	0.026	-0.30	-0.05		
	0.027	0.25	-0.03		
	0.028	-0.18	-0.03		
	0.029	-0.17	-0.03		
	0.030	-0.10	-0.05		
	0.031	0.80	-0.05		
	0.032	-0.43	-0.06		
	0.033	-1.54	-0.06		
	0.034	-0.65	-0.06		
	0.035	-0.35	-0.08		
	0.036	0.16	-0.06		
	0.037	-0.06	-0.05		-
	0.038	-0.14	-0.05		
, ·	0.039	-0.31	-0.05		
	0.040	-0.12	-0.05		
	0.041	-0.14	-0.06		
	Total Control of the				-
	0.042	0.49	-0.06		

			<u> </u>	
	0.043	-0.03	-0.06	1
	0.044	0.06	-0.06	,
	0.045	0.22	-0.05	
	0.046	-0.26	-0.05	
 -	0.047	-0.45	-0.05	
_	0.048	0.03	-0.05	
	0.049	-0.18	-0.03	
	0.050	0.25	-0.03	
	0.051	-0.21	-0.03	
-	0.052	-0.47	-0.03	
	0.053	0.08	-0.03	
	0.054	-0.04	-0.03	
	0.055	-0.04	-0.05	11.11.
	0.056	0.30	-0.05	
	0.057	-0.22	-0.06	
	0.057	-0.47	-0.05	
		0.21	-0.06	
	0.059	-0.44	-0.06	
-	0.060	-0.44	-0.08	
	0.061		-0.06	
	0.062	0.49		-
	0.063	-0.22	-0.08	
	0.064	0.14	-0.06	
	0.065	0.04	-0.05	
	0.066	-0.14	-0.05	
	0.067	-0.04	-0.05	
	0.068	0.45	-0.05	
	0.069	-0.35	-0.05	
	0.070	-0.91	-0.03	
	0.071	0.12	-0.02	
	0.072	0.22	-0.02	
	0.073	0.05	-0.03	
	0.074	0.00	-0.02	
	0.075	-0.36	-0.03	
	0.076	0.25	-0.05	
	0.077	-0.29	-0.05	
	0.078	-0.43	-0.05	
	0.079	0.36	-0.06	
	0.080	0.10	-0.06	
	0.081	0.32	-0.05	
	0.082	-0.31	-0.05	
······································	0.083	-0.09	-0.06	
	0.084	-0.17	-0.08	
. :-	0.085	0.16	-0.06	
	0.086	-0.09	-0.06	
	0.087	0.27	-0.06	
	0.088	-0.31	-0.05	
<u> </u>	0.089	0.12	-0.03	
	0.090	0.12	-0.06	
			-0.06	
	0.091	-0.08		
	0.092	-0.18	-0.05	
	0.093	0.25	-0.03	<u> </u>

	0.0041	0.40	0.02	1
	0.094	0.10	-0.03	
	0.095	0.40	-0.02	
	0.096	0.00	-0.03	
	0.097	0.19	-0.03	
	0.098	-0.30	-0.05	
	0.099	0.31	-0.05	
	0.100	-0.08	-0.05	
	0.101	-0.16	-0.06	
	0.102	-0.01	-0.06	
	0.103	-0.14	-0.08	
	0.104	0.62	-0.06	
	0.105	0.25	-0.05	
	0.106	0.29	-0.05	
	0.107	-0.10	-0.05	
	0.108	0.00	-0.03	
	0.109	-0.43	-0.05	
	0.110	-0.40	-0.05	
	0.111	-0.52	-0.03	
	0.112	-3.46	-0.06	
	0.113	-1.44	-0.08	
	0.114	0.06	-0.06	
	0.115	-0.44	-0.03	
	0.116	-1.21	-0.02	
	0.117	-0.04	-0.03	
	0.118	0.54	-0.06	
	0.119	-0.30	-0.03	
	0.120	-0.18	-0.05	
	0.121	0.30	-0.05	
	0.122	-0.57	-0.05	
	0.123	0.06	-0.08	
	0.124	0.19	-0.08	
	0.125	-0.38	-0.09	
	0.126	0.60	0.03	
	0.127	1.59	0.54	
	0.128	4.61	1.39	
	0.129	3.68	1.94	
<u> </u>	0.130	5.82	2.05	
	0.131	5.81	4.21	
	0.132	13.19	6.63	
	0.133	10.89	7.45	
	0.134	12.08	6.01	
	0.135	3.10	4.26	
	0.136	-3.76	3.21	
	0.137	19.63	3.19	-
	0.137	-5.53	0.45	
		-17.61	-1.62	
	0.139		-5.15	
	0.140	-21.47		
	0.141	-14.59	-6.28	
	0.142	-19.13	-8.62	
	0.143	0.09	-7.23	
	0.144	-3.72	-8.53	

	0.145	-26.54	-8.66		1
	0.146	-26.54	-9.05		-
ļ	0.140			-	
		-26.54	-7.25		!
	0.148	26.53	-5.01		f
	0.149	26.53			<u> </u>
	0.150	20.37		· · · · · · · · · · · · · · · · · · ·	
	0.151	-14.14	4.56		
	0.152	-26.54	6.12		
	0.153	-0.89	6.83		
ļ	0.154	10.39	8.57		
	0.155	-3.20	6.98		
	0.156	26.53	7.18		
	0.157	-18.62	6.35		
	0.158	-17.49	4.58		
	0.159	-26.54	1.99		
	0.160	-26.54	-0.76		
	0.161	-13.54	-3.92		
	0.162	26.53	-5.57		
	0.163	0.76	-7.42		
	0.164	17.83	-6.20		
	0.165	26.53	-6.55		
	0.166	-19.23	-6.49		
	0.167	-19.18	-7.65		
	0.168	26.53	-6.24		
	0.169	15.01	-5.44		
	0.170	3.52	-1.26		
	0.171	-26.54	2.98		
	0.172	1.17	1.74		
	0.173	1.21	-0.25	· · · · · · · · · · · · · · · · · · ·	
	0.174	-6.44	-0.82		
	0.175	8.59	1.50	· · · · · · · · · · · · · · · · · · ·	
	0.176	-26.54	1.43		
	0.177	10.55	1.54	 ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' 	
<u> </u>	0.178	18.88	-0.88		
	0.179	-6.62	0.43		
	0.180	-26.54	-0.52		
	0.181	26.53	1.74		
	0.182	-8.02	2.31		
	0.183	-9.84	2.48		
	0.184	-7.76	3.04		
	0.185	26.53	4.16		
	0.186	22.22	5.75	·	
	0.187	15.98			
	0.188	0.40	6.17		
<u> </u>			4.92		
	0.189	3.68	2.02	-	
 	0.190	-20.90	1.17		
	0.191	6.58	1.34		
	0.192	20.76	-0.11		
	0.193	-1.65	0.37		
	0.194	-5.30	0.15		
	0.195	4.85	0.82		

				
	0.196	-23.14	-0.93	
	0.197	-9.60	-2.02	
	0.198	2.99	1.37	
	0.199	1.36	-0.88	
	0.200	-7.44	-1.00	
	0.201	-7.33	-0.76	
	0.202	6.56	0.00	
	0.203	-4.63	0.12	
	0.204	3.72	1.70	
	0.205	10.02	2.78	
	0.206	6.82	1.88	
	0.207	26.53	4.75	
-	0.208	-3.94	3.11	
· · · · · · · · · · · · · · · · · · ·	0.209	-8.53	1.11	<u> </u>
	0.210	-22.13	-1.33	
	0.211	0.83	-4.78	
	0.212	-3.16	-3.73	
	0.213	0.91	-4.50	
	0.214	-11.33	-4.95	
	0.215	-26.54	-4.02	
	0.216	26.53	-4.95	
	0.217	-25.63	-3.52	
	0.218	-10.44	-2.39	
	0.219	26.53	-1.19	
	0.220	26.53	-0.56	:
<u> </u>	0.221	26.53	-1.14	
	0.222	26.53	-1.73	
	0.223	24.75	-1.09	
	0.224	23.42	-1.30	
	0.225	-26.54	-1.03	
	0.226	26.53	-2.81	
	0.227	-3.06	-1.40	
	0.228	26.53		
	0.229	-4.85	0.19	
	0.229	19.33	1.80	
	+		1.28	
 	0.231	-18.45	1.13	
	0.232	26.53	0.42	
	0.233	-26.54	1.42	
	0.234	11.77	0.42	
	0.235	-3.14	1.59	
	0.236	9.80	1.67	
	0.237	-26.54	3.07	
	0.238	22.04	2.11	
	0.239	-1.70	1.94	
	0.240	26.53	2.02	
	0.241	10.00	2.42	
	0.242	-9.80	2.90	
	0.243	4.09	1.94	
	0.244	11.13	2.16	-
	0.245	2.13	1.83	
	0.246	23.20	1.39	
	 			

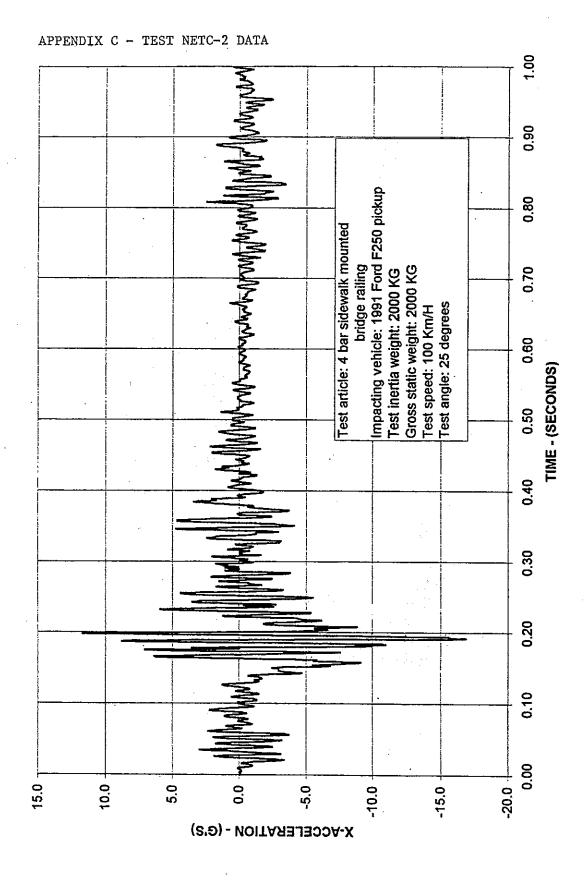
	·			
	0.247	-3.27	1.19	
	0.248	-1.49	0.96	
	0.249	10.60	0.71	
	0.250	9.38	-0.68	
	0.251	5.88	-1.22	
	0.252	3.91	-0.89	
	0.253	-4.95	-1.36	
·	0.254	-0.22	-2.13	
	0.255	-1.44	-2.05	
	0.256	-0.56	-1.63	
	0.257	-0.47	-1.62	
	0.258	-8.11	-2.56	
	0.259	-4.37	-2.45	
-	0.260	-1.53	-1.67	
	0.261	-3.93	-1.02	
	0.262	-0.65	-1.13	
	0.263	7.43	-1.11	
	0.264	-1.46	-0.85	
	0.265	2.81	-0.69	
	0.266	-2.89	-0.65	·
	0.267	-6.97	-0.17	
	0.268	0.53	0.35	
	0.269	3.90	0.85	
	0.270	4.78	0.91	
	0.271	8.63	1.26	
	0.272	0.95	1.34	
	0.273	5.26	1.43	
	0.274	13.81	1.17	
	0.275	0.45	1.70	
	0.276	-7.24	1.71	
	0.277	-6.74	1.37	
	0.278	1.21	0.68	
	0.279	3.20	0.32	
	0.280	1.21	0.17	
-	0.281	-1.11	0.59	
	0.282	-3.90	0.46	
	0.283	1.00	0.40	
	0.284	0.89	0.19	
	0.285	-3.69	-0.37	
	0.286	0.40	-0.76	
	0.287	-13.49	-0.76	
	0.288	0.18	-0.69	
	0.289	-15.03	-0.09	
	0.209	-10.03	-1.33	
-	0.290	-14.57		
	0.291		-1.56	
		4.39	-1.42	
	0.293	8.82	-1.03	
	0.294	1.72	-0.76	
	0.295	-1.76	-0.20	
	0.296	3.84	0.49	
ı í	0.297	2.73	0.51	! 1

	298 0.92		
	299 2.88		
0.3	300 -3.97	0.60	
0.3	301 -4.60	0.11	
0.3	302 -5.46	-0.93	
0.3	303 -1.70	-0.77	
0.3	304 -3.21	-0.03	
0.3	305 1.35	0.34	
0.3	306 1.96	0.28	
0.3	307 1.45	0.05	
0.3	308 -2.06	0.08	
0.3	3.58	0.31	,
0.3	310 0.40	0.12	
0.3	11 4.68	0.25	
0.3	312 -2.40	0.60	
0.3	5.13	0.40	
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0.3	3.33		
0.3	7.52		
0.3	6.80	0.48	
0.3	21 1.23	0.09	
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0.3	24 -0.84		
0.3			
0.3	26 7.31	0.02	
0.3	27 -3.54	0.11	
0.3	28 7.92		
0.3	29 3.11	-0.12	
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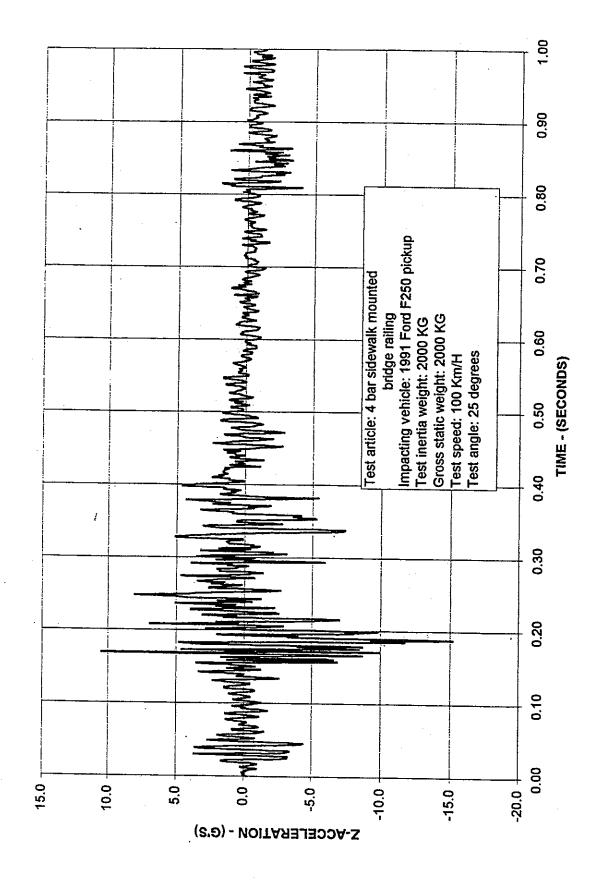
	0.0401	5.67	0.001	
	0.349	-3.07	0.62	
ļ	0.350	-0.05	0.35	
	0.351	0.12	0.11	
	0.352	1.39	-0.06	
	0.353	0.44	-0.34	
	0.354	2.53	-0.35	
	0.355	3.37	-0.23	
ļ	0.356	-1.30	-0.08	
	0.357	-1.08	-0.12	
	0.358	-1.33	-0.28	
	0.359	0.73	-0.39	
	0.360	0.22	-0.45	
	0.361	1.44	-0.39	
	0.362	-0.26	-0.32	
	0.363	1.50	-0.32	
	0.364	0.78	-0.22	
	0.365	-1.45	-0.14	
	0.366	-0.16	-0.14	
	0.367	-0.12	0.00	
	0.368	1.35	-0.02	
	0.369	-1.19	-0.09	
	0.370	0.13	-0.06	
	0.371	0.87	-0.02	
	0.372	1.78	-0.05	
	0.373	2.28	-0.08	
	0.374	1.10	0.12	
	0.375	0.06	0.34	
	0.376	-1.04	0.14	
	0.377	-0.35	0.00	
	0.378	-0.04	0.03	
	0.379	0.18	0.14	
	0.380	1.75	0.31	
	0.381	-0.65	0.40	
	0.382	-2.58	0.32	i.
	0.383	1.35	0.20	
	0.384	-1.23	-0.03	
	0.385	1.74	-0.35	
	0.386	0.32	-0.39	
	0.387	1.06	-0.28	
	0.388	-0.76	-0.32	
	0.389	1.57	-0.40	
	0.390	-0.51	-0.25	
	0.391	1.26	-0.02	
	0.392	-2.05	-0.09	
	0.393	1.72	-0.17	
	0.394	1.50	-0.05	
	0.395	1.46	0.09	
	0.396	-1.33	0.06	1
	0.397	-0.52	-0.06	
	0.398	-0.76	-0.15	
 	0.399	-0.83	-0.11	
<u> </u>	0.0001	0.00	-0.11	<u> </u>

	0.400	-0.75	-0.15	
	0.401	-2.02	-0.22	
	0.402	0.31	-0.17	
	0.403	-0.58	-0.11	
	0.404	1.89	0.02	
	0.405	-0.93	0.15	
	0.406	0.31	0.05	
	0.407	0.26	-0.15	Į į
	0.408	-1.00	-0.19	
	0.409	0.09	0.06	
	0.410	1.30	0.31	
	0.411	0.73	0.28	
	0.412	1.13	0.22	
	0.413	-0.65	0.20	
	0.414	0.83	0.08	
. ,	0.415	0.17	-0.08	
	0.416	1.02	-0.02	
	0.417	-0.32	0.15	
	0.418	1.01	0.11	
	0.419	-1.63	-0.02	
	0.420	0.12	-0.29	
	0.421	-0.34	-0.52	
	0.422	-0.86	-0.56	
	0.423	-0.80	-0.48	:
	0.424	-1.14	-0.42	
	0.425	1.65	-0.31	
	0.426	1.49	-0.11	
	0.427	-1.01	-0.06	
•	0.428	0.04	-0.02	
	0.429	0.00	0.02	
	0.430	1.83	0.11	
	0.431	0.58	0.20	<u> </u>
	0.432	-0.69	0.14	
-	0.433	-0.08	0.08	
	0.434	0.26	0.05	
	0.435	0.16	0.06	
	0.436	-0.67	0.06	
	0.437	-1.10	-0.02	
	0.438	-0.66	-0.11	
	0.439	0.87	-0.06	-
-	0.440	0.66	0.02	
	0.441	-0.54	0.02	
	0.441	-0.60	0.06	
-	0.442	0.25	0.06	
<u> </u>	0.444	-0.57	0.02	
<u> </u>	0.444	-0.43		
 		 	0.02	
	0.446	-0.92	0.00	<u> </u>
ļ	0.447	0.58	0.03	1
	0.448	-0.41	0.00	<u> </u>
	0.449	0.31	-0.14	
	0.450	-0.08	-0.15	

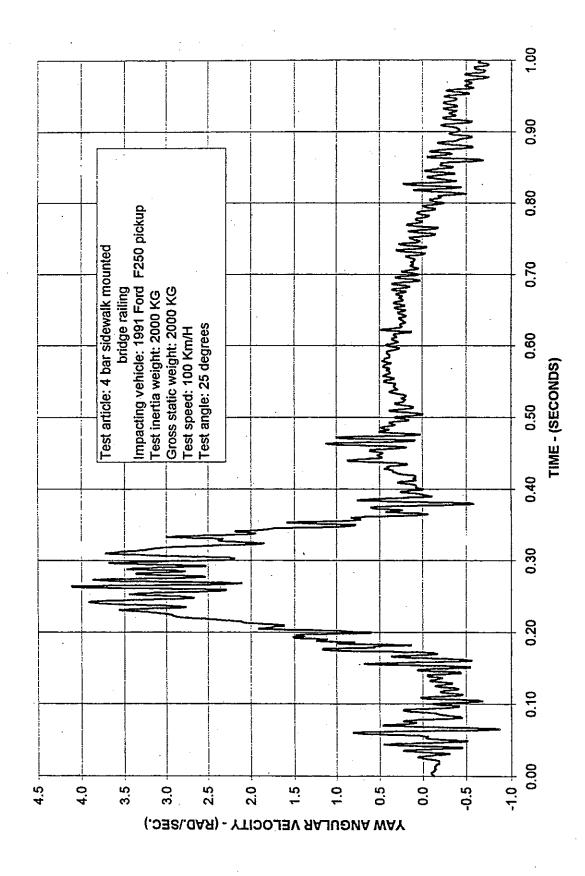
0.451					
0.453	ĺ	0.451	-2.01	-0.17	
0.454 -0.65 -0.20 0.455 -0.96 -0.17 0.455 -0.44 -0.29 0.457 0.45 -0.28 0.458 -0.84 -0.14 0.459 -0.36 -0.11 0.460 1.22 -0.05 0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.79 0.14 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.475 0.25 -0.12 0.476 0.36 -0.06 0.477 0.03 0.12 0.479 <t< td=""><td>1</td><td>0.452</td><td>1.00</td><td>-0.25</td><td></td></t<>	1	0.452	1.00	-0.25	
0.455 -0.96 -0.17 0.456 -0.44 -0.29 0.457 0.45 -0.28 0.458 -0.84 -0.14 0.459 -0.36 -0.11 0.460 1.22 -0.05 0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.79 0.14 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.474 -1.27 -0.11 0.475 0.25 -0.12 0.477 0.03 -0.12 0.479 <		0.453	-0.39	-0.26	
0.456 -0.44 -0.29 0.457 0.45 -0.28 0.458 -0.84 -0.14 0.459 -0.36 -0.11 0.460 1.22 -0.05 0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.96 0.09 0.467 0.21 0.14 0.468 -0.79 0.14 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.474 -1.27 -0.11 0.475 0.25 -0.12 0.477 0.03 0.12 0.479		0.454	-0.65	-0.20	į
0.456 -0.44 -0.29 0.457 0.45 -0.28 0.458 -0.84 -0.14 0.459 -0.36 -0.11 0.460 1.22 -0.05 0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.96 0.09 0.467 0.21 0.14 0.468 -0.79 0.14 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.474 -1.27 -0.11 0.475 0.25 -0.12 0.477 0.03 0.12 0.479			-0.96		
0.457 0.45 -0.28 0.458 -0.84 -0.14 0.459 -0.36 -0.11 0.460 1.22 -0.05 0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.96 0.09 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.474 -1.27 -0.11 0.475 0.25 -0.12 0.476 0.36 -0.06 0.477 0.03 0.12 0.478 0.19 0.15 0.479 1.31 0.02 0.480 0.					
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0.461 -0.14 0.12 0.462 0.78 0.17 0.463 -0.01 0.14 0.464 0.19 0.17 0.465 0.06 0.17 0.466 0.96 0.09 0.467 0.21 0.14 0.468 -0.79 0.14 0.469 -0.62 -0.03 0.470 0.32 -0.22 0.471 0.48 -0.14 0.472 0.69 -0.02 0.473 -0.34 -0.08 0.474 -1.27 -0.11 0.475 0.25 -0.12 0.476 0.36 -0.06 0.477 0.03 0.12 0.478 0.19 0.15 0.479 1.31 0.02 0.480 0.05 -0.08 0.481 0.39 -0.08 0.482 -0.95 -0.20 0.483 -1.23 -0.37 0.484 -0					
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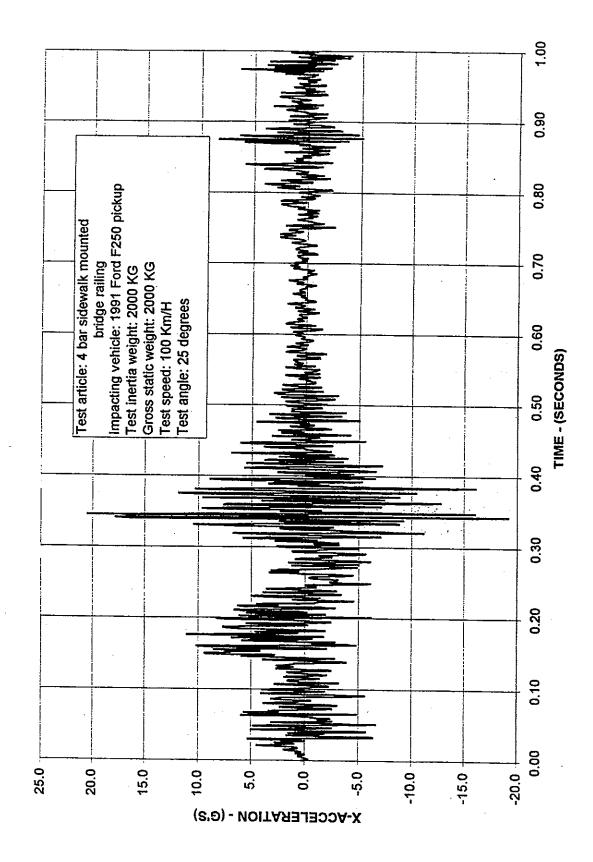
Vehicle C.G. longitudinal accelerometer plot - Test NETC-2.



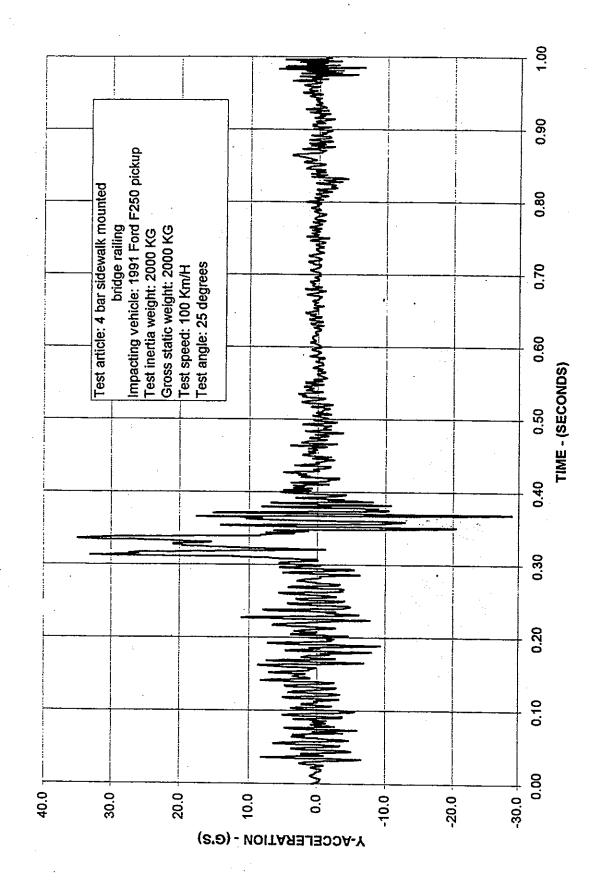
Vehicle C.G. vertical accelerometer plot - Test NETC-2.



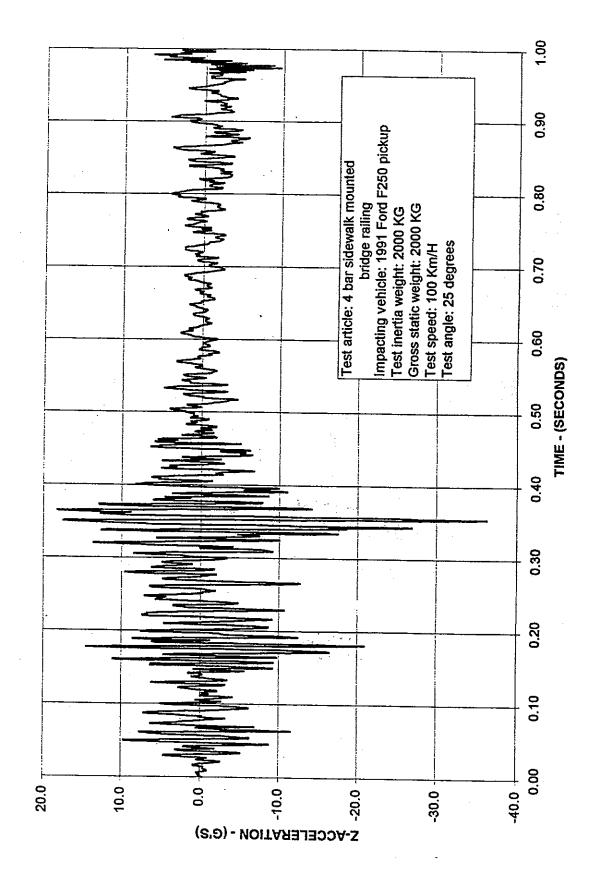
Rate gyro plot - Test NETC-2.



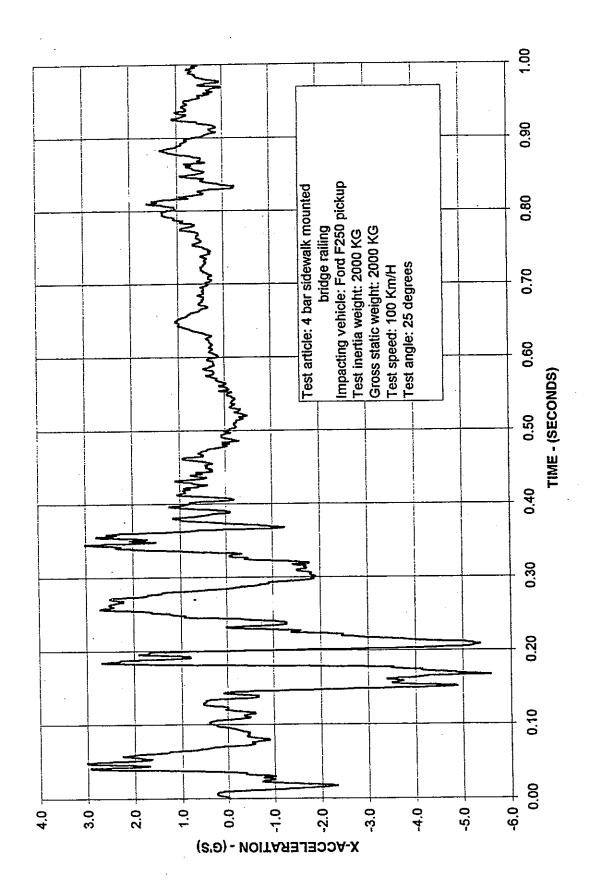
Rear axle longitudinal accelerometer plot - Test NETC-2.



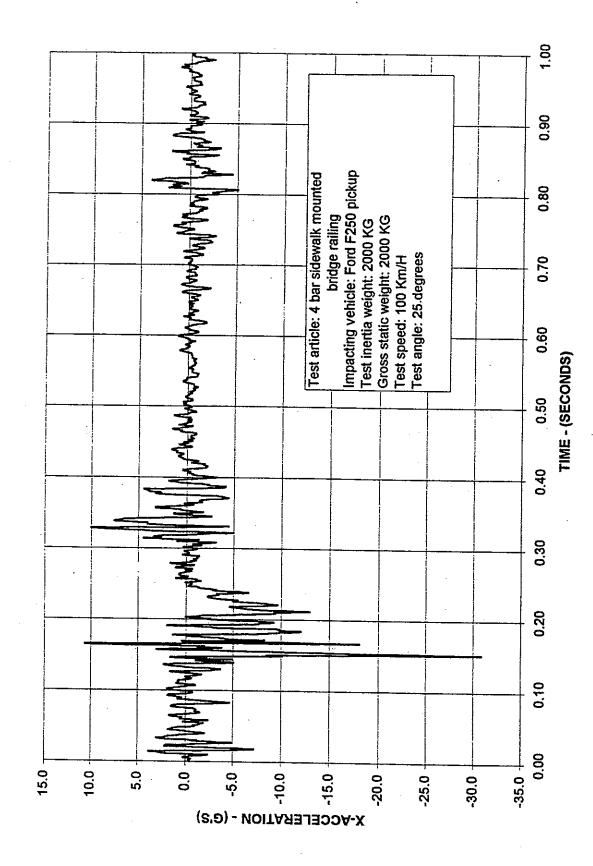
Rear axle lateral accelerometer plot - Test NETC-2.



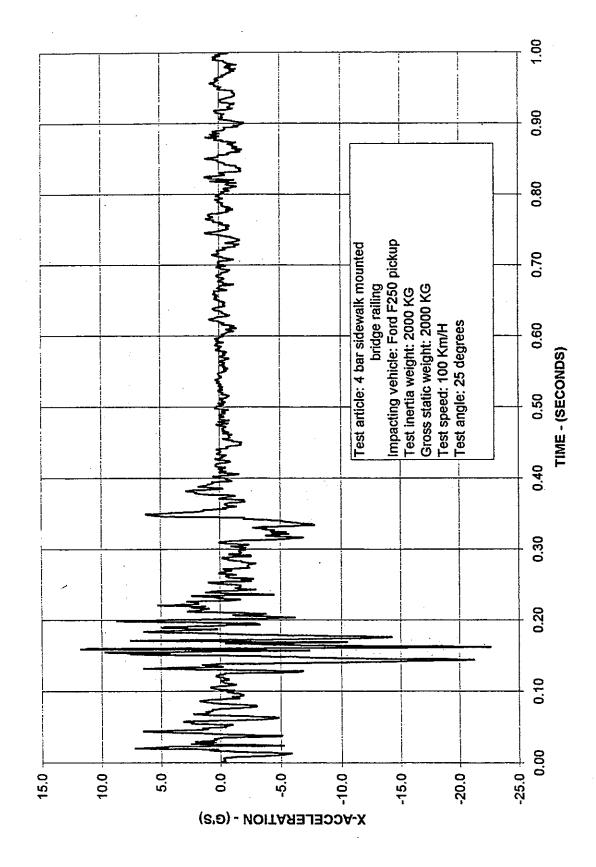
Rear axle vertical accelerometer plot - Test NETC-2.



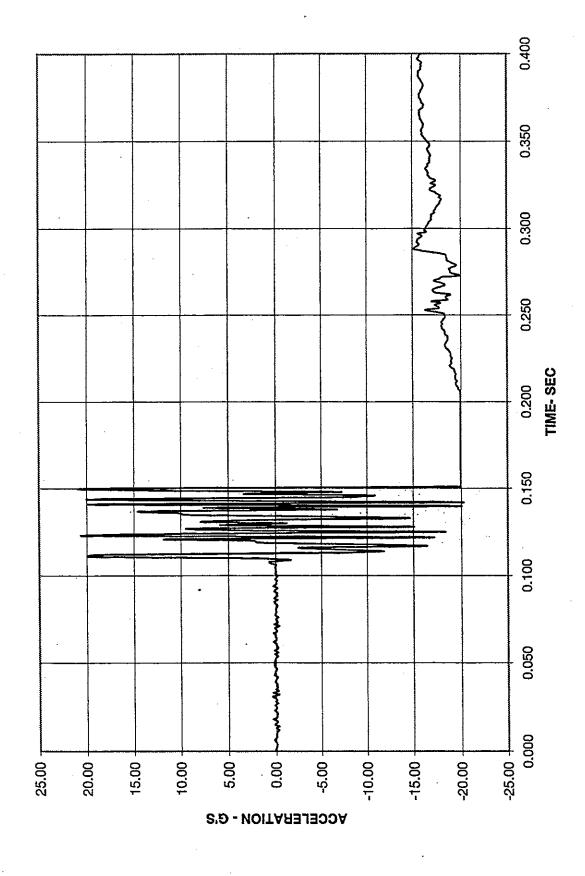
Top of engine longitudinal accelerometer plot - Test NETC-2.



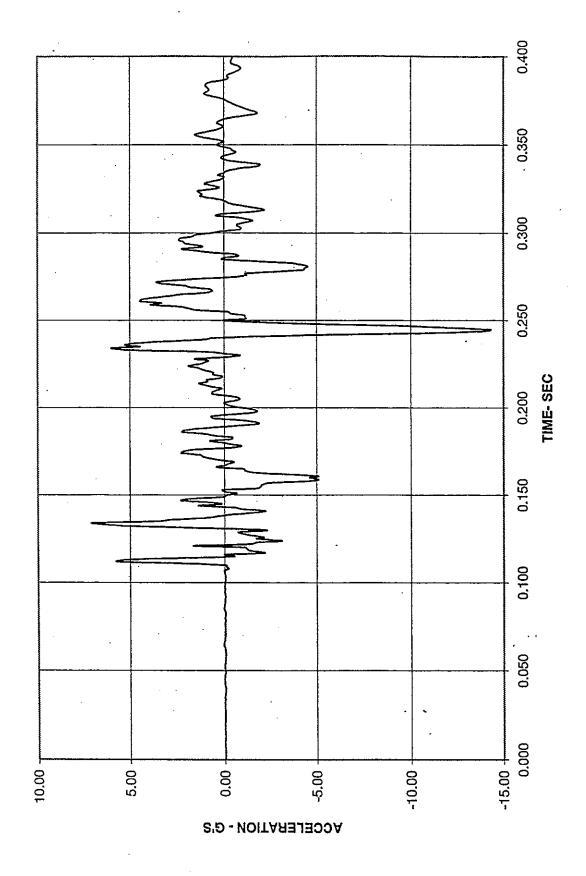
Right front disc brake longitudinal accelerometer plot - Test NETC-2.



Left front disc brake longitudinal accelerometer plot - Test NETC-2.



Top of post 7 lateral accelerometer plot - Test NETC-2.



Bottom of post 7 lateral accelerometer plot - Test NETC-2.

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TRANSDUCER DATA WITH CALCULATED VEHICLE KINETICS AND OCCUPANT RISK SUMMARIES

TEST ID ----- NETC-2
TEST DATE ---- 11-20-96
VEHICLE CLASS - 2000P
IMPACT SPEED -- 27.78 M/S

VEHICLE KINETICS SUMMARY NOTE: VALUES ARE INSTANTANEOUS AT TIME

TIME (S)	ACC		J'S) VERT.	- HEAD. ANG(D)	VELC		(MPS) VERT.	D	ISP. Y	(M)
										~
.000	1	.0	4	25.0	27.8	.0	.0	.0	.0	.0
.010	1	.0	-1.8	25.1	27.8	.0	.0	.3	.1	.0
.020	-4.8	.0	2.2	25.2	27.6	.1		.5	.2	.0
.030	-4.6	.0	7.5	25.2	27.5	.1		.8	.4	
.040	-3.8	.0	5.3	25.3	27.5	.1		1.0	.5	.0
.050	8	.0	3.3	25.3	27.4	.1	3	1.3	.6	.0
.060	3.0	.0	-1.9	25.2	27.2	.1	3	1.5	.7	.0
.070	-1.0	.0	.5	25.3	27.4	. 2	4	1.7	. 8	.0
.080	.5	.0	5	25.2	27.3	.1	3	2.0	.9	.0
.090	3.7	.0	-3.0	25.4	27.4	.2	3	2.2	1.0	0
.100	.2	.0	-1.8	25.4	27.4	.2	4	2.5	1.2	.0
.110	.5	.0	2	25.6	27.3	.3	4	2.7	1.3	.0
.120	-1.4	.0	1.6	25.8	27.3	.4	4	3.0	1.4	.0
.130	-2.2	.0	2.5	26.0	27.3	.5	3	3.2	1.5	.0
.140	-1.2	.0	.3	26.0	27.1	.5	3	3.5	1.6	.0
.150	-3.6	.0	-1.5	26.1	26.6	.5	2	3.7	1.7	-0
.160	-7.6	.0	-15.1	26.2	25.6	.6	2	4.0	1.8	.0
.170	-4.5	.0	-4.6	26.2	25.6	.6	3	4.2	2.0	.0
.180	-16.4	.0	4.6	25.9	25.6	.4	-1.1	4.4	2.1	
.190	-9.0	.0	-3.6	25.4	25.2	.2	-1.9	4.7	2.2	1 1
.200	1.2	.0	-10.4	24.7	24.5	1	-2.6	4.9	2.3	1
.210	-3.1	.0	-2.7	23.8	23.6	4	-2.5	5.1	2.3	1
.220	-7.9	.0	4.0	22.6	23.0	ĝ	-2.8	5.3	2.5	1
,230	4.1	.0	-2.3	20.9	22.6	-1.6	-2.6	5.5	2.5	
.240	-4.7	.0	2.6	19.0	22.7	-2.4	-2.5	5.7	2.7	2 2
.250	-8.0	.0	4.9	17.1	22.5	-3.1	-1.9	5.9	2.8	
.260	-5.5	.0	2.8	15.5	22.5	-3.8	-1.8	6.1	2.9	2
.270	-1.8	.0	3.7	13.7	22.3	-4.5	-1.5	6.3	3.0	2
.280	. 9	.0	-1.3	11.9	22.2	-5.2	-1.4	6.5	3.0	3
.290	.7	.0	1.6	10.1	21.8	-5.9	-1.2	6.7	3.1	3
.300	~.7	.0	.1	8.3	21.7	-6.5	-1.3	7.0		3
.310	1.2	.0	-1.7	6.8	21.6	-7.1	-1.2	7.2	3.2	3
.320	-1.1	. 0	1.9	4.9	21.3	-7.8	-1.1	7.4	3.3	3
.330	-3.8	.0	6.4	3.6	20.9	-8.3	8	7.4	3.4	3
.340	-2.5	.0	1	2.2	20.8	~8.8	-1.2		3.5	3
.350	-5.9	.0	.5	1.4	20.7	-9.1	-1.2	7.8	3.6	3
	•				~0.7	Э. Т	- I . I	8.0	3.7	3

360 3.5 .0 1.7 .8 20.7 -9.3 -1.6 8.2 3.8 4 .370 -3.0 .0 -1.8 .6 20.6 -9.4 -1.4 8.4 3.9 4 .380 .2 .0 1.6 .5 20.2 -9.4 -1.2 8.6 4.0 4 .390 -7 .0 1.6 .4 20.5 -9.5 -1.3 8.8 4.1 -4 .400 -2.9 .0 5.8 3.20.4 -9.5 -1.0 9.0 4.2 -4 .410 -1.6 .0 4.1 .3 20.4 -9.5 8 9.2 4.2 4 .420 -1.3 .0 2.2 .2 20.3 -9.5 5 9.4 4.4 4 .440 3 .0 -3 -3 20.3 -9.7 4 9.6 4.5 4 .450 9 <th>TIME (S)</th> <th>ACC</th> <th>CEL. (G</th> <th></th> <th>HEAD. ANG (D)</th> <th>LONG.</th> <th>LAT.</th> <th>(MPS) VERT.</th> <th>D</th> <th>ISP. Y</th> <th>(M) Z</th>	TIME (S)	ACC	CEL. (G		HEAD. ANG (D)	LONG.	LAT.	(MPS) VERT.	D	ISP. Y	(M) Z
380 .2 .0 1.6 .5 20.2 -9.4 -1.2 8.6 4.0 4 .390 7 .0 1.6 .4 20.5 -9.5 -1.3 8.8 4.1 4 .410 -1.6 .0 4.1 .3 20.4 -9.5 -1.0 9.0 4.2 -4 .420 -1.3 .0 2.2 .2 20.3 -9.5 8 9.2 4.3 4 .430 3.1 .0 .1 .0 20.3 -9.5 5 9.4 4.4 4 .440 3 .0 3 3 20.3 -9.7 4 9.6 4.5 4 .440 3 .0 3 8 20.2 -9.9 3 10.0 4.7 4 .480 6 .0 .3 8 20.2 -9.9 3 10.0 4.9 4 .480	.360										
390 -7 .0 1.6 .4 20.5 -9.5 -1.3 8.8 4.1 4 400 -2.9 .0 5.8 .3 20.4 -9.5 -1.0 9.0 4.2 4 420 -1.3 .0 2.2 .2 22.03 -9.5 5 9.4 4.4 4 430 3.1 .0 .1 .0 20.3 -9.5 5 9.4 4.4 4 440 3 .0 3 3 20.3 -9.7 4 9.6 4.5 4 450 9 .0 -1.5 6 20.2 9.8 3 10.0 4.7 4 450 9 .0 -1.1 -1.4 20.2 -9.9 -3 10.2 4.8 4 470 .2 .0 .5 -1.2 20.2 -10.0 3 10.4 4.9 4 480								-1 2			
.400 -2.9		7									
.410			.0	5.8							
.420 -1.3 .0 2.2 .2 20.3 -9.5 -5 9.4 4.44 .4403 .0 -1 .0 20.3 -9.6 -4 9.6 4.54 .4509 .0 -1.56 20.2 -9.8 -3 10.0 4.7 -4 .4606 .0 .3 -8 20.2 -9.8 -3 10.0 4.7 -4 .470 .2 .0 .5 -1.2 20.2 -10.03 10.4 4.94 .480 .8 .0 -1.1 -1.4 20.1 -10.1 -4 10.6 5.04 .490 -1.3 .0 2.3 -1.7 20.1 -10.24 10.8 5.15 .500 .8 .0 1.8 -1.8 20.1 -10.24 10.8 5.15 .500 .8 .0 1.8 -1.8 20.1 -10.23 11.0 5.25 .510 1.3 .0 .0 -7 -2.1 20.1 -10.23 11.0 5.25 .5205 .0 -7 -2.1 20.1 -10.32 11.4 5.45 .550 .3 .0 .4 -2.2 20.0 -10.41 11.6 5.45 .550 .3 .0 .4 -2.2 20.0 -10.41 11.6 5.45 .550 .3 .0 .2 -2.5 19.8 -10.5 .1 12.0 5.65 .550 .3 .0 -2 -2.5 19.8 -10.5 .1 12.0 5.65 .550 .3 .0 -2 -2.5 19.8 -10.5 .1 12.0 5.65 .5 .550 -1.0 .06 -3.2 19.5 -10.7 .2 12.7 5.95 .550 -7 .0 -1.0 -3 -2.8 19.8 -10.6 .1 12.3 5.75 .550 -1 .0 .0 -6 -3.2 19.5 -10.7 .2 12.7 5.95 .550 -7 .0 -1.0 -3 -2.8 19.8 -10.5 .1 12.3 5.75 .550 -1 .0 .0 -6 -3.2 19.5 -10.7 .2 12.7 5.95 .5 .560 -1 .0 .0 .3 -2.8 19.8 -10.5 .1 12.3 5.75 .550 -7 .0 -1.0 -3.5 19.5 -10.8 .2 12.9 6.05 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .		-1.6					-9.5				
.430						20.3	-9.5				
.450				.1		20.3	-9.6		9.6	4.5	
.460											
.470				-1.5			-9.8				
. 480							-9.9				
.490									10.4		
.500 .8 .0 1.8 -1.8 20.1 -10.2 3 11.0 5.2 5 .510 1.3 .0 .0 -1.9 20.0 -10.3 2 11.2 5.3 5 .520 5 .0 .4 -2.2 20.0 -10.3 2 11.4 5.4 5 .530 .3 .0 .4 -2.2 20.0 -10.4 1 11.6 5.4 5 .540 1 .0 .3 -2.4 19.9 -10.4 0 11.8 5.5 5 .550 .3 .0 -2 -2.5 19.8 -10.5 .1 12.0 5.6 5 .570 -8 .0 .1 -3.0 19.7 -10.6 .2 12.5 5.8 5 .580 -1 .0 6 -3.2 19.5 -10.8 .2 12.9 6.0 5 .590 -7		-1.3				20.1	-10.2				
.510					-1.8	20.1	-10.2				
.520					-1.9	20.0	-10.3				
.530 .540 .540 .541 .00 .3 .2.44 .19.9 -10.44 .00 .11.8 .5.55 .5.5 .5.5 .5.60 -1.00 .00 .3 .2.8 .19.8 .10.6 .1 .1 .12.0 .5.66 .5.5 .5.5 .5.60 .7 .8 .00 .1 .3 .2.8 .19.8 .10.6 .1 .1 .12.3 .5.7 .5.8 .5.7 .5.8 .0 .1 .0 .0 .6 .3 .2 .19.5 .10.7 .2 .12.7 .5.9 .5.5 .5.9 .5.9 .7 .7 .0 .1.0 .3.5 .19.5 .10.7 .2 .12.7 .5.9 .5.5 .5.9 .5.7 .5.9 .5.9 .7 .7 .0 .1.0 .3.7 .19.5 .10.8 .2 .12.9 .6.0 .5 .5 .6.0 .5 .6.0 .8 .0 .5 .3.9 .19.3 .10.9 .1 .13.1 .6.1 .5 .6.1 .5 .6.3 .5 .6.3 .5 .6.3 .6.3 .6.3 .6.3					-2.1	20.1	-10.3				
.540			.0		-2.2				11.6		
.560 -1.0 .0 .3 -2.8 19.8 -10.6 .1 12.3 5.7 5 .570 8 .0 .1 -3.0 19.7 -10.6 .2 12.5 5.8 5 .580 1 .0 6 -3.2 19.5 -10.7 .2 12.7 5.9 5 .590 7 .0 -1.0 -3.5 19.5 -10.8 .2 12.9 6.0 5 .600 5 .0 -1.0 -3.7 19.4 -10.9 .1 13.1 6.1 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .620 -1.7 .0 1.4 -4.0 19.2 -11.0 .0 13.5 6.3 5 .630 -1.4 .0 .6 -4.2 19.1 -11.1 .0 13.7 6.4 5 .650 -1.4 .0 .5 -4.5 19.0 -11.1 .0 14.			. 0		-2.4	19.9	-10.4				
.570 8 .0 .1 -3.0 19.7 -10.6 .2 12.5 5.8 5 .580 1 .0 6 -3.2 19.5 -10.7 .2 12.7 5.9 5 .590 7 .0 -1.0 -3.5 19.5 -10.8 .2 12.9 6.0 5 .600 5 .0 -1.0 -3.7 19.4 -10.9 .1 13.1 6.1 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .620 -1.7 .0 1.4 -4.0 19.2 -11.0 .0 13.5 6.3 5 .630 -1.4 .0 .6 -4.2 19.1 -11.1 .0 13.7 6.4 5 .650 -1.4 .0 .5 -4.5 19.0 -11.1 .0 14.1 6.6 5 .670 9 .0 .3 -4.6 18.9 -11.2 .0 14.2		 -1 N			-2.5	19.8	-10.5				
.580 1 .0 6 -3.2 19.5 -10.7 .2 12.7 5.9 5 .590 7 .0 -1.0 -3.5 19.5 -10.8 .2 12.9 6.0 5 .600 5 .0 -1.0 -3.7 19.4 -10.9 .1 13.1 6.1 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .620 -1.7 .0 1.4 -4.0 19.2 -11.0 .0 13.5 6.3 5 .630 -1.4 .0 .6 -4.2 19.1 -11.1 .0 13.7 6.4 5 .650 -1.4 .0 .5 -4.5 19.0 -11.1 .0 14.1					-2.8 -3.0	19.8	-10.6				
.590 7 .0 -1.0 -3.5 19.5 -10.8 .2 12.9 6.0 5 .600 5 .0 -1.0 -3.7 19.4 -10.9 .1 13.1 6.1 5 .610 8 .0 .5 -3.9 19.3 -10.9 .1 13.3 6.2 5 .620 -1.7 .0 1.4 -4.0 19.2 -11.0 .0 13.5 6.3 5 .630 -1.4 .0 .6 -4.2 19.1 -11.1 .0 13.7 6.4 5 .640 .2 .0 8 -4.3 19.0 -11.1 .0 13.9 6.5 5 .650 -1.4 .0 .5 -4.5 19.0 -11.1 .0 14.1 6.6 5 .670 9 .0 2.0 -4.8 18.8 -11.2 .0 14.4 6.8 5 .680 8 .0 6 -4.9 18.7 -11.3 .0 14.					-3.0	19.7	-10.6 -10.7				
.600	.590				-3.5	19.5	-10.7 -10.8				
.610					-3.7						
.620 -1.7 .0 1.4 -4.0 19.2 -11.0 .0 13.5 6.3 5 .630 -1.4 .0 .6 -4.2 19.1 -11.1 .0 13.7 6.4 5 .640 .2 .0 8 -4.3 19.0 -11.1 .0 13.9 6.5 5 .650 -1.4 .0 .5 -4.5 19.0 -11.1 .0 14.1 6.6 5 .660 9 .0 .3 -4.6 18.9 -11.2 .0 14.2 6.7 5 .670 9 .0 2.0 -4.8 18.8 -11.2 .0 14.4 6.8 5 .680 8 .0 6 -4.9 18.7 -11.3 .0 14.6 6.9 5 .700 7 .0 5 -5.2 18.5 -11.4 1 15.0 7.1 5 .710 -1.3 .0 -1.0 -5.2 18.4 -11.4 2 1		8		.5	-3.9						
.630 -1.4						19.2	-11.0				
.640						19.1 -	-11.1				
.660						19.0	-11.1		13.9		
.670 9 .0 2.0 -4.8 18.8 -11.2 .0 14.4 6.8 5 .680 8 .0 6 -4.9 18.7 -11.3 .0 14.6 6.9 5 .690 1 .0 -1.1 -5.1 18.6 -11.3 .0 14.8 7.0 5 .700 7 .0 5 -5.2 18.5 -11.4 1 15.0 7.1 5 .710 -1.3 .0 -1.0 -5.2 18.4 -11.4 2 15.2 7.2 5 .720 -1.1 .0 4 -5.3 18.3 -11.4 2 15.4 7.3 5 .730 -1.9 .0 1.0 -5.4 18.2 -11.4 3 15.6 7.4 5 .740 -2.4 .0 1 -5.4 18.1 -11.5 3 15.8 7.5 5 .750 -1.6 .0 -1.1 -5.5 17.9 -11.5 5				.5	-4.5	19.0 -	11.1				
.680 8 .0 6 -4.9 18.7 -11.3 .0 14.4 6.8 5 .690 1 .0 -1.1 -5.1 18.6 -11.3 .0 14.8 7.0 5 .700 7 .0 5 -5.2 18.5 -11.4 1 15.0 7.1 5 .710 -1.3 .0 -1.0 -5.2 18.4 -11.4 2 15.2 7.2 5 .720 -1.1 .0 4 -5.3 18.3 -11.4 2 15.4 7.3 5 .730 -1.9 .0 1.0 -5.4 18.2 -11.4 3 15.6 7.4 5 .740 -2.4 .0 1 -5.4 18.1 -11.5 3 15.8 7.5 5 .750 -1.6 .0 -1.1 -5.5 17.9 -11.5 5 16.2 7.7 5 .770 3 .0 -1.4 -5.5 17.8 -11.5 5 <td></td> <td></td> <td></td> <td></td> <td>-4.6 -4.6</td> <td>18.9</td> <td>11.2</td> <td></td> <td></td> <td></td> <td></td>					-4.6 -4.6	18.9	11.2				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					-4.0	10.0	.11 2		14.4		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						18.6	11 3				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						18.5 -	11.4				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$											
.730 -1.9 .0 1.0 -5.4 18.2 -11.43 15.6 7.45 .740 -2.4 .01 -5.4 18.1 -11.53 15.8 7.55 .750 -1.6 .0 -1.1 -5.5 17.9 -11.54 16.0 7.65 .7601 .0 .1 -5.5 17.9 -11.55 16.2 7.75 .7703 .0 -1.4 -5.5 17.8 -11.55 16.4 7.85 .7907 .0 -2 -5.5 17.6 -11.56 16.6 7.95 .7907 .0 -2 -5.5 17.6 -11.56 16.6 7.95				4	-5.3						
.750 -1.6 .0 -1.1 -5.4 18.1 -11.53 15.8 7.55 .7601 .0 .1 -5.5 17.9 -11.54 16.0 7.65 .7703 .0 -1.4 -5.5 17.9 -11.55 16.2 7.75 .7802 .06 -5.5 17.8 -11.55 16.4 7.85 .7907 .0 -2 -5.5 17.6 -11.56 16.6 7.95								3			
.7601 .0 .1 -5.5 17.9 -11.54 16.0 7.65 .7703 .0 -1.4 -5.5 17.8 -11.55 16.2 7.75 .7802 .06 -5.5 17.7 -11.56 16.6 7.95 .7907 .02 -5.5 17.7 -11.56 16.6 7.95		-2.4 -1 C							15.8		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										7.6	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$											
$\frac{1}{100}$ $\frac{1}$											
		~.7	.0	2	-5.5 -5.5			6 7			
.800 -1.1 .09 -5.5 17.6 -11.57 16.7 8.05	.800	-1.1									

TIME				- HEAD.	VELO	CITY	(MPS)	D	ISP.	(M)
(S)	LONG.	LAT.	VERT.	ANG (D)	LONG.	LAT.	VERT.	X	Y	Z
.810	-1.0	.0	-4.0	-5.4	17.6	-11.4	8	17.1	8.1	5
.820	-3.2	.0	1.7	-5.2	17.5	-11.4	8	17.3	8.2	~.5
.830	1.1	.0	-5.5	-5.2	17.4	-11.4	9	17.5	8.3	5
.840	~.6	.0	-3.8	-5.1	17.1	-11.3	-1.1	17.7	8.4	5
.850	.1	.0	-3.5	-4.9	17.0	-11.3	-1.4	17.8	8.5	5
.860	-2.3	.0	2.5	-4.7	17.0	-11.2	-1.7	18.0	8.6	6
.870	-2.1	.0	1.0	-4.6	17.0	-11.2	-1.8	18.2	8.7	6
.880	1	.0	-3.2	-4.4	16.9	-11.1	-2.0	18.4	8.8	6
.890	2.3	.0	-2.2	-4.2	17.0	-11.1	-2.2	18.6	8.9	6
900	1.2	.0	9	-3.9	17.0	-11.0	-2.3	18.7	9.0	6
.910	-1.1	.0	-1.3	-3.7	16.9	-11.0	-2.3	18.9	9.1	7
.920	-1.1	0	8	-3.5	16.8	-10.9	-2.4	19.1	9.2	7
.930	9	.0	8	-3.3	16.8	-10.8	-2.6	19.3	9.3	7
.940	-1.6	.0	-2.5	-3.1	16.8	-10.8	-2.7	19.4	9.4	7
.950	-1.0	.0	-2.0	-2.9	16.7	-10.7	-2.8	19.6	9.5	8
.960	.0	.0	-1.5	-2.7		-10.6	-3.0	19.8	9.6	8
.970	5	.0	-2.6	-2.4		-10.6	-3.1	20.0	9.7	8
.980	9	.0	-2.9	-2.1		-10.5	-3.3	20.1	9.8	9
.990	.4	.0	-1.1	-1.7		-10.4	-3.4	20.3	9.9	9
									-	

HIGHEST 50.0-MS AVG. ACCEL.

		TIME	(SEC)
	G'S	START	END
LONG.	-6.12	.180	.230
LAT.	.00	.950	1.000

TEST ID ----- NETC-2
TEST DATE ---- 11-20-96
VEHICLE CLASS - 2000P
IMPACT SPEED -- 27.78 M/S

OCCUPANT RISK SUMMARY NOTE: INSTANTANEOUS 10-MS AVERAGE ACCELERATIONS

m x seri	(VEHICL	3)	(occ	UPANT)
TIME (S)	ACCEL. LONG.	(G'S) LAT.	ANG.VEL (RAD/S)	VEL. LONG.	(M/S) LAT.	DISP.	(M) LAT.
.000 .010 .020 .030 .040	12 62 -1.99 .06 .15	.00	13 15 19 26 45	.00 .04 .25 .52 .86	.00 .07 .18 .24 .37	.00 .00 .00 .00 .00	.00 .00 .00 .00 .00
.060 .070 .080 .090 .100 .110	75 16 .37 1.05 99 -1.01	.00 .00 .00 .00 .00	.81 .46 36 .18 12 11	-1.02 56 .87 11 .36	10 .10 .30 .24 .41	.01 .01 .02 .02	.00 .00 .00 .00 .00
.130 .140 .150 .160 .170	83 -3.74 -6.33 -7.30 1.01 -6.69	.00	39 27 06 36 49 17	.97 .74 .60 1.60 2.83 2.22 1.02	.86 .97 .98 1.18 1.24 1.17	.04 .05 .05 .06 .08 .10	.00 .00 .00 .00
.190 .200 .210 .220 .230 .240 .250	-8.07 08 -6.96 -4.50 .33 .29	.00 .00 .00 .00 .00	1.11 .60 1.62 2.74 3.48 3.71 2.84	.48 2.11 1.29 .01 94 -1.50	02 49 -1.60 -3.09 -4.89 -6.58	.12 .13 .14 .15 .14	.00 01 01 02 03 05
.260 .270 .280 .290 .300 .310 .320 .330	21 60 -1.73 .75 .05 .09 42 95	.00	2.54 2.70 3.13 3.11	.02 .42 .22 56 41 .48 -1.59 .05 .90	-7.95 -9.28 -10.87 -12.56 -14.10 -15.37 -17.10 -18.31 -19.20* -20.26	.12 .12 .11 .10 .09 .08 .07 .05 .06	10 12 14 17 19 22 24 27
.350	76	.00	.79	3.24	-20.48	.07	33 35

	(VEHTCT.E) ('	OCCT	JPANT	
TIME	ACCEL.		ANG.VEL	VEL.	(M/S)	DISP.	
(S)	LONG.		(RAD/S)	LONG.	LAT.	LONG.	LAT.
			(1012) 2)				
.360	2.12	.00	. 83	3.06	-20.97	.10	38
.370	-2.52	.00	.24	4.14	-20.89	.14	40
.380	1.04	.00	56	5.77	-20.69	.18	42
.390	1.14	.00	± .11	4.72	-20.96	.22	44
.400	-1.19	.00	01	4.67	-21.03	.27	47
.410	.10	.00	.25	4.24	-21.18	.31	49
.420	71	.00	.19	4.36	-21.20	.35	51
.430	1.13	.00	.39	4.06	-21.43	.39	53
.440	32	.00	.87	3.17	-21.79	.43	56
.450	.58	.00	.46	3.91	-21.90	.46	58
.460	.47	.00	.44	3.89	-22.08	.50	- 61
.470	- 46	.00	.66	3.47	-22.43	.53	63
.480	.37	.00	.50	3.75+		.57+	66
.490	23	.00	.32	4.01	-22.71	.60	69
.500	.25	.00	.32	3.97	-22.83	.64	71
.510	.09	.00	.38	3.89	-22.94	.68	74
.520	55	.00	.31	3.95	-23.01	.72	76
.530	09	.00	.19	4.20	-23.07	.76	79
.540	38	.00	.30	4.06	-23.23	.80	81
.550	39	.00	.44	3.86	-23.43	.84	84
.560	55	.00	.41	3.89	-23.60	87	- 87
.570	83	.00	.43	3.95	-23.78	.91	89
.580	53	.00	.44	3.99	-23.97	.94	92
.590	41	.00	.41	4.08	-24.13	.98	95
.600 .610	28 44	.00	.40	4.11	-24.28	1.02	- 98
.620	44	.00	.35 .13	4.21	-24.41	1.06	-1.01
.630	85	.00	.13	4.64	-24.45 -24.64	1.10	-1.04
.640	24	.00	.23	4.49 · 4.59	-24.64 -24.73	1.14	-1.07
.650	78	.00	.20	4.69	-24.73 -24.82	1.18 1.23	-1.10
.660	18	.00	.33	4.53	-24.02	1.23	-1.12
.670	59	.00	.24	4.70	-25.06	1.31	-1.15
.680	-1.12	.00	.31	4.65	-25.00	1.36	-1.18 -1.21
.690	94	.00	.11	5.05	-25.23	1.40	-1.21
.700	50	.00	.04	5.28	-25.28	1.45	-1.27
.710	90	.00	.10	5.21	-25.35	1.50	-1.30
.720	70	.00	.09	5.32	-25.40	1.55	-1.32
.730	49	.00	.01	5.55	-25.41	1.60	-1.35
.740	-1.63	.00	.12	5.46	-25.49	1.65	-1.38
.750	-1.18	.00	.14	5.61	-25.55	1.71	-1.41
.760	52	.00	.16	5.60	-25.56	1.77	-1.43
.770	98	.00	.17	5.67	-25.57	1.83	-1.46
.780	80	.00	03	6.04	-25.52	1.88	-1.48
.790	89	.00	12	6.27	-25.49	1.94	-1.51
.800	77	.00	25	6.58	-25.39	2.01	-1.53

	(VEHICLE	:)	(occ	UPANT		}
TIME (S)	ACCEL.	(G'S)	ANG.VEL (RAD/S)	VEL.	(M/S)	DISP. LONG.		,
.810 .820 .830 .840 .850 .860 .870 .880	88 -1.74 -1.57+ -1.619235 -1.2453	.00 .00 .00 .00 .00		7.15 7.44 8.08 7.49 7.98		2.15 2.22 2.29 2.36 2.44 2.52	-1.68	-
OCCUP.	RISK FA	CTORS			TIME (S)	VELOCITY (M/S)		
>LONO >LAT	S. VEL.	AFTER 0. AFTER 0.	.6 M DISP .3 M DISP		.489	3.99 19.17		
MAX. AC	CCEL. AF	TER OCCU	JPANT IMP	ACT	TIME(S)	ACC.(GS)		
>LONG >LAT.	·	ERATION ERATION		<u>-</u> -	.836 .900	-2.55		

TEST ID ----- NETC-2
TEST DATE ---- 11-20-97
VEHICLE CLASS - 2000P
IMPACT SPEED -- 27.78 M/S

3.

TIME (SEC)	(VEL. X	CG AC	CEL(G'S)) R	(VEL. X	REAR Y	ACCEL	(G'S)) R
.000 .010 .020 .030 .040 .050 .070 .080 .090 .100 .120 .130 .140 .150 .160 .170 .180 .200 .210 .220 .220 .240 .250 .250 .300 .310 .320 .330 .340 .350			-1.8 -1.296386706342748803974209	134312 21 1212838752422632 11 1413 				1.3 6.0 1.3 6.0 1.7 4.1 1.5 6.0 1.7 4.1 1.7 5.6 1.7 1.6 6.1 1.7 1.6 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7

TIME (SEC)	(VEL. X	CG AC	CEL(G	P'S):)(VEL	. REAR Y	ACCEL.	-(G'S)) R
(SEC)360 .370 .380 .400 .410 .420 .4430 .4450 .4460 .450 .510 .520 .550 .550 .550 .550 .560 .660 .6650 .6650 .6650 .6650 .6650 .700 .720 .730 .750 .750 .770 .780 .790	X 2.9 0.3 6.9 8.8 2.5 7.5 8.3 1.1 1.6 5.1 4.3 5.1 8.5 6.6 2.3 8.7 2.6 0.1 2.1 4.3 5.1 8.5 6.6 2.3 8.7 2.6 0.1 2.1 4.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1			2.2 2.2 1.0 1.0 4.0 2.6 1.7 1.8 .9 .4 .3 .7 1.4 1.2 .8 .5 .4 .2	7.3 -1.3 7.5 2.9 1 2.5	Y -10.2 -6.8 8.1 -3.9 5.4 1.6 .4 1 .2 1.4	2 12.8 9 5.7 -4.0 6.7 6.2 -5.3 -2.2 -5.9 1.2 3.5 -1.8 2.0 1.9	R 17.9 7.0 12.4 6.3 8.6 6.9 6.4 3.3 6.8 2.0 4.3 2.3
.800	7	.0	1 6	.4 .9	.7 .9	.0 1.9	1.6 4.1	1.8 4.6

TIME	(VEL.	CG AC	CEL (G	'S))	(VEL	REAR	ACCEL	(G'S) -	-)
(SEC)	X	Y	Z	R	X	Y	Z	R	•
.810	4	.0	-2.3						
.820	-1.8	.0	-2.3 .9	2.3 2.0	1.2	0	8	1.4	
.830	.4	.0	-3.1	3.1	-2.0	-2.4	.7	3.2	
.840	3	.ŏ	-2.3	2.3	.5 5.8	6		3.4	
.850	1	.0	-2.0	2.0	2	.0 .5		5.9	
.860	-1.4	.0	1.3	1.9	-1.9	1.3	-2.4	. 2.5	
.870	-1.5	.0	.4	1.5	4.2	5	1.1	2.6	
.880	2	.0	-2.0	2.0	6.3	- 6	-3.5		
.890	1.3	.0	-1.4	1.9	4.0	-1.4	8 -1.7		
.900	.7	.0		. 9	5	.2	1.9	4.6	
.910	- 6	.0	8	1.1	-1.0	3	4	2.0	
.920	7	.0	6	. 9	8	3	-3.2	1.1 3.3	
.930	6	.0	5	. 8	.6	9	-3.2 -3.0	3.3	
.940	-1.0	.0	-1.5	1.8	.8	.1	7	1.0	
.950	6	.0	-1.3	1.5	.6	2.3	-1.0	2.6	
.960	1	.0	-1.0	1.0	-1.0	2.0	6	2.3	
.970	3	.0	-1.8	1.8	. 5	1.2	-1.6	2.1	
.980	5	.0	-1.7	1.8	3.9	2.0	-5.1		
.990	.3	.0	- 9	1.0	-3.8	2.0	3.8	5.7	
MAXIM	M VALUES	דידי רואם	MTP OTP O	مارين المارين					
		Y	650						
- VEL. CG ACCEI	(G'S) -	-17.4	102		-SEC		SEC		-SEC
VEL. REAR ACCE	L(G'S)	21.1	341			-15.9	.188		.192
	,		. ~ 47	35.5	.220	-36.3	.355	38.2	.355

TEST ID ----- NETC-2
TEST DATE ---- 11-20-96
VEHICLE CLASS - 2000P
IMPACT SPEED -- 27.78 M/S

TIME (S)	ENGIN TOP		ELERATION DISK N CALIN	BRAKE	INSTRUMENT PANEL
.000 .010 .020 .030 .040 .050 .060 .070 .080 .100 .110 .120 .130 .140 .150 .160 .170 .180 .220 .230 .240 .250 .250 .260 .270 .280 .310 .320	-1.02.50.95.81.94.35.05.54.58.284.244.034.53.79.5.8 -4.3.50.55.4.58.284.24.4.034.53.7.9.5.8				PANEL
.330 .340 .350	1 2.3 2.1	.0	-1.8 6.9 7	-2.8 -5.0 5.0	.0 .0 .0

		ACC	CELERATION		
			DISK E		
TIME	ENGIN		CALIE	PERS	INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
÷					
.360	2.3	. 0	.7	-1.4	.0
.370	9	- 0	-3.8	-1.0	.0
.380	1.1	. 0	3.8	2.0	.0
.390	.0	.0	-2.4	1.1	.0
.400	.8	.0	-3.2	4	.0
.410	.5	.0	.4	3	.0
.420	. 8	.0	-1.2	.3	.ŏ
.430	. 9	.0	.8	1	.0
.440	. 6	.0	1.4	. 2	.0
.450	.4	.0	.3	-1.8	.0
.460	. 8		9	8	.0
.470	.5	.0	.5	3	.0
.480	.0	.0	3	3 4	
.490	.0				.0
.500	1	.0	1	2	.0
	2	.0	3	.2	.0
.510		.0	5	3	.0
.520	5	.0	2	3	. 0
.530	2	.0	7	.1	.0
.540	2	0	.1	.1	.0
.550	1	.0	4	3	.0
.560	.1	.0	7	3	.0
.570	.2	.0	4	2	.0
.580	.3	.0	.6	.3	.0
.590	.2	.0	2	1	.0
.600	.2	0	.9	4	.0
.610	.3	.0	2	9	.0
.620	.3	.0	-1.6	.0	.0
.630	.3	.0	3	6	.0
.640	.9	. 0	3	.3	.0
.650	1.0	.0	-1.0	.0	.0
.660	.7	.0	.2	.4	.0
.670	.4	.0	.2	.0	.0
.680	.4	0	2	3	:0
.690	.5	. 0	1	6	.0
.700	.4	.0	2	4	.0
.710	.3	.0	.5	4	.0
.720	.5	-0	.3	.2	.0
.730	.4	.0	-1.2	-1.1	.ŏ
.740	.3	.0	-2.5	9	.0
.750	.5	.0	5	6	.0
.760	.5	.ŏ	.7	1	.0
.770	.6	.0	.3	.8	.0
.780	.6	.0	-1.8	6	
.790	1.1	.0	5		.0
.800	1.2	.0	-2.9	.0	.0
	* • 4	.0	-4.9	1	.0

	AC(CELERATIO	N-(G'S)	
ENGIN	BLOCK			INSTRUMENT
TOP	BOTTOM	RIGHT	LEFT	PANEL
1.6	.0	1.8	-1.1	.0
.8	.0	3.9	-1.3	.0
.0	.0	-1.3	.0	.0
. 4	.0	9	-1.4	.0
.6	.0		1.1	.0
.8	0			.0
			-	.0
				.0
.9	.0			.0
			=	.0
				.0
				.0
				.0
				.0
				.0
		=		.0
				.0
• ** *7	.0	7.0	-T.0	.0
	TOP 1.6 .8 .0 .4 .6 .8 .5 1.2 .9 .6 .3 .6 .9 .8 .3 .0 .4	ENGIN BLOCK TOP BOTTOM 1.6 .0 .8 .0 .0 .0 .4 .0 .6 .0 .8 .0 .5 .0 1.2 .0 .9 .0 .6 .0 .3 .0 .6 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0 .8 .0 .9 .0	DISK: ENGIN BLOCK CALT: TOP BOTTOM RIGHT 1.6 .0 1.8 .8 .0 3.9 .0 .0 -1.3 .4 .09 .6 .0 .7 .8 .0 1.8 .5 .09 1.2 .04 .9 .0 .1 .6 .08 .3 .08 .3 .08 .6 .0 .8 .9 .0 -1.5 .8 .0 .0 .3 .07 .8 .0 .0 .3 .07 .4 .0 1.0	TOP BOTTOM RIGHT LEFT 1.6 .0 1.8 -1.1 .8 .0 3.9 -1.3 .0 .0 -1.3 .0 .4 .09 -1.4 .6 .0 .7 1.1 .8 .0 1.8 -1.8 .5 .09 -1.1 1.2 .04 1.1 .9 .04 1.1 .9 .0 .13 .6 .08 -2.0 .3 .08 -2.0 .3 .089 .9 .0 -1.52 .8 .07 -1.3 .8 .0 .07 -1.3 .8 .0 .07 -1.3 .8 .0 .07 -1.3 .8 .0 .07 -1.3 .8 .0 .07 -7 .4 .0 1.0 -1.0

APPENDIX C - POST NO. 7 ACCELEROMETER DATA

	1	POST 7	POST 7	i	
		TOP	BOTTOM		-
	716.65	ACCEL	ACCEL		
	TIME			-	••
	(SEC)	(G'S)	(G'S)		
<u>-</u>	0.000	0.00	0.01	<u> </u>	
	0.001	0.12	-0.03		
	0.001	-0.05	-0.02		
	0.003	-0.05	-0.03		•
 -	0.004	-0.06	-0.03		
•	0.005	0.01	-0.02		
	0.006	0.19	-0.02		
	0.007	0.12	-0.02		
	0.007	-0.03	-0.01		
	0.009	-0.02	-0.01		
	0.010	-0.02	-0.01		
	0.011	-0.12	-0.02		
	0.012	-0.26			
	0.012	0.00			
	0.014	-0.30			
	0.014	0.14	-0.02		
	0.016	-0.06			
	0.017	-0.10	-0.01		
	0.018	0.31			
	0.019	-0.04	-0.01		
	0.020	-0.07			
	0.021	-0.13			
	0.022	-0.07	-0.02	-	
	0.023	0.17	-0.03		
	0.024	-0.01	-0.03		
	0.025	-0.02			
	0.026	0.02			
	0.027	-0.18			
	0.028	0.03	<u> </u>		
	0.029			-	
	0.030	0.10			
	0.030	0.10			
	0.031	-0.32			<u> </u>
	0.032	0.27		 	<u> </u>
	0.033	-0.22		<u> </u>	
	0.035	0.02			-
	0.036	-0.16			
	0.037				-
		-0.10			<u>i</u>
•	0.038	-0.11			<u> </u>
	0.039	0.07			
	0.040	0.05			!
	0.041	-0.07	-0.02	Į.	1

.	0.042	0.17	-0.01	
	0.043	0.06	0.00	
	0.044		0.01	
	0.045	0.08	-0.01	
	0.046	-0.05	-0.01	
	0.047	-0.03	-0.03	
	0.048	0.13		
	0.049	0.14	-0.04	
	0.050	0.17	-0.02	
	0.051	0.15	-0.01	
	0.052	0.06	-0.01	
	0.053	0.01	-0.01	
	0.054	-0.20	-0.03	
	0.055	0.11	-0.03	
	0.056	-0.21	-0.04	
	0.057	0.14	-0.04	<u> </u>
	0.058	-0.17	-0.04	
	0.059	-0.20	-0.06	
	0.060	-0.05	-0.06	
	0.061	0.01	-0.03	
Ĭ	0.062	0.25	-0.02	
	0.063	0.00	0.00	
·	0.064	-0.04	0.02	
	0.065	0.08	0.02	
	0.066	0.04	0.02	
	0.067	0.22	0.00	
	0.068	-0.12	-0.01	
	0.069	-0.01	-0.02	
	0.070	0.12	-0.03	
	0.071	-0.33	-0.03	
	0.072	0.16	-0.03	
	0.073	-0.16	-0.02	
	0.074	-0.10	-0.02	
<u> </u>	0.075	0.01	-0.02	
	0.076	-0.25	-0.02	
·	0.077	0.03	-0.03	
	0.078	0.03	-0.04	
	0.079	-0.05	-0.04	
	0.080	-0.01	-0.03	
 	0.081	-0.01	-0.04	
-	0.082	-0.09	-0.04	
	0.083	-0.15	-0.04	
	0.084	0.12	-0.01	
<u> </u>	0.085	0.14	0.02	
<u> </u>	0.086	-0.18	0.01	
	0.087	0.19	0.01	
<u> </u>	0.088	-0.09	0.00	
ļ	0.089	-0.09	-0.02	
	0.090	-0.12	-0.02	
		0.12	-0.03	
<u></u>	0.091		-0.03	
	0.092	-0.02		
	0.093	-0.15	-0.03	<u>11</u>

	0.0941	0.22	-0.02	
!	0.095	-0.05	-0.01	<u> </u>
;	0.096	-0.03	-0.02	
<u> </u>	0.097	-0.11	-0.01	
<u> </u>	0.097	0.08	-0.01	<u>i</u>
 -	0.098	-0.10	-0.02	
l	0.100	-0.10	-0.02	· · · · · · · · · · · · · · · · · · ·
<u> </u>	0.100	0.07	-0.02	
<u> </u>	0.101	-0.03	-0.04	
	0.102	0.03	-0.04	
	0.103	0.02	-0.04	<u> </u>
	0.104	0.04	-0.03	
<u> </u>		-0.04	-0.03	
<u> </u>	0.106	0.53	0.00	
<u> </u>	0.107	0.65	-0.22	
	0.108			
 	0.109	-1.57 2.54	-0.10 -0.10	
	0.110	19.94		
<u> </u>	0.111		2.48	
	0.112	19.55	5.73	
	0.113	-6.13	5.14	
<u> </u>	0.114	-11.82	2.42	
	0.115	-7.02	-0.50	
	0.116	-2.82	-0.01	·
<u>.</u>	0.117	-16.32	-2.13	
	0.118	-7.53	-1.48 -1.25	·
	0.119	1.94 2.24	-1.25	
	0.120 0.121	11.22	1.71	
ļ	0.121	-17.06	-1.36	
	0.122	19.94	-1.75	
ļ	0.123	12.19	-3.14	
	0.124	-18.26	-1.74	
	0.125	3.30	-2.14	<u> </u>
	0.126	9.00	-1.39	
<u> </u>	0.127	-15.08	-0.94	
<u> </u>		5.52	-0.94	
<u> </u>	0.129 0.130	-1.20	-2.29	
 	0.131	7.91	0.24	
	0.131	0.35	4.30	
 	0.132	-14.65	6.13	
	0.133	-14.05	7.00	
	0.134	9.55	3.53	
		10.04	2.88	
ļ	0.136			
	0.137 0.138	14.13	0.93	
		-6.66	0.37	
	0.139	7.43	-0.54	
	0.140	-19.95	-1.54	
	0.141	19.94	-2.21	
	0.142	-19.95	-0.94	
	0.143	2.02	-0.53	
	0.144	19.94	1.42	

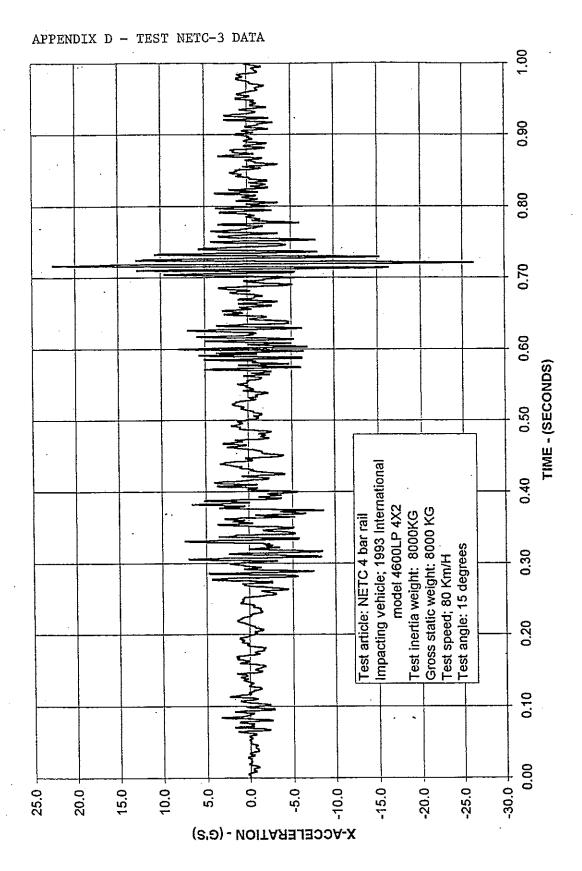
	0.4451	0.041	0.16.	
	0.145	-6.84	0.16	
	0.146	-10.80	0.99	
	0.147	3.34	2.34	
	0.148	-7.13	1.61	
	0.149	12.16	0.06	
	0.150	19.94	-0.15	
	0.151	-19.95	-0.68	
	0.152	-19.95	-0.04	
	0.153	-19.95	0.09	
	0.154	-19.95	-1.81	
	0.155	-19.95	-1.98	
	0.156	-19.95	-2.05	
	0.157	-19.95	-2.43	
i	0.158	-19.95	-4.48	
	0.159	-19.95	-5.09	
1441	0.160	-19.95	-4.62	
	0.161	-19.95	-5.05	
	0.162	-19.95	-3.24	
	0.163	-19.95	-1.59	
	0.164	-19.95	-1.10	
	0.165	-19.95	-1.07	
	0.166	-19.95	0.39	-
	0.167	-19.95	0.00	
	0.168	-19.95	-0.23	
. 1	0.169	-19.95	-0.50	
	0.170	-19.95	0.22	
	0.171	-19.95	0.86	
	0.172	-19.95	1.17	
	0.173	-19.95	1.29	
	0.174	-19.95	2.30	
	0.175	-19.95	2.19	
	0.176	-19.95	1.61	
	0.177	-19.95	-0.09	
	0.178	-19.95	-0.93	
	0.179	-19.95	-0.42	
	0.180	-19.95	0.05	
	0.181	-19.95	0.79	
<u> </u>	0.182	-19.95	-0.35	
	0.183	-19.95	-0.44	
	0.184	-19.95	0.51	
	0.185	-19.95	1.15	
	0.186	-19.95	2.27	
	0.187	-19.95	2.18	
 	0.187	-19.95	1.37	<u> </u>
	0.189	-19.95	0.25	
	0.189	-19.95	-1.10	
 	0.191	-19.95	-1.88	
	0.192	-19.95	-1.53	
	0.193	-19.95	-0.71	
	0.194	-19.95	0.59	
<u> </u>	0.195	-19.95	0.69	

			0.40	
	0.196	-19.95	-0.13	
į	0.197	-19.95	-1.42	
	0.198		-1.80	
1	0.199	-19.95	-1.52	
į	0.200	-19.95	-0.96	
	0,201	-19.95	-0.38	
	0.202	-19.95	-0.09	
	0.203	-19.95	-0.01	
	0.204	-19.95	-0.56	
	0.205	-19.95	-0.85	
•	0.206	-19.95	-0.68	1
	0.207	-19.79	0.03	<u>.</u> 1
	0.208	-19.75	0.63	
	0.209	-19.61	0.63	
	0.210	-19.45	0.42	
	0.211	-19.45	0.13	
	0.212	-19.59	0.68	
	0.213	-19.38	1.09	
	0.214	-19.44	1.37	
	0.215	-19.39	0.91	
	0.216	-19.48	0.94	
	0.217	-19.37	0.23	
	0.218	-19.34	0.10	
	0.219	-19.22	0.60	
	0.220	-18.91	0.58	
	0.220	-18.82	0.91	
	0.221	-18.97	1.19	
		-18.98	1.51	
	0.223		1.94	· · · · · · · · · · · · · · · · · · ·
	0.224	-18.96	1.34	<u> </u>
	0.225	-19.08		
	0.226	-18.95	1.08	
	0.227	-18.93	0.87	
	0.228	-18.91	1.59	
	0.229	-18.80	0.12	
	0.230	-18.68	-0.87	
	0.231	-18.47	-0.04	
<u></u>	0.232	-18.37	1.01	
	0.233	-18.30	4.87	
	0.234	-18.42	6.01	
·	0.235	-18.54	4.47	<u> </u>
	0.236	-18.60	5.25	
	0.237	-18.61	4.62	
	0.238	-18.57	3.24	
	0.239	-18.35	1.11	
	0.240	-18.29	0.61	[
	0.241	-18.25	-2.51	}
		-18.06	-6.58	
l .	0.242	- 10.001		
			-10.99	
	0.243	-18.00	-10.99 -14.06	
			-10.99 -14.06 -14.30	

	0.247	-18.10	-9.74		
	0.248	-18.22	-4.81		
	0.249	-18.35	-2.14		
	0.250	-18.29	0.02		
	0.251	-18.17	-1.21!		
	0.252	-17.20	-1.13		
	0.253	-16.29	-1.11		
	0.254	-17.67	-0.38		
	0.255	-17.55	-0.17		
	0.256	-17.26	1.48		
	0.257	-17.84	2.00		
	0.258	-16.96	2.45		
	0.259	-18.61	3.87		
	0.260	-18.43	3.31		
	0.261	-18.47	4.43		
	0.262	-18.91	4.33		
· ·	0.263	-17.35	3.75		
	0.264	-17.09	2.85	:	
	0.265	-17.11	2.28		
	0.266	-17.58	1.01		
-	0.267	-18.22	0.64		[
	0.268	-18.29	0.79	:/	
	0.269	-17.67	1.85	i	
	0.270	-17.20	2.13		
	0.271	-17.78	3.30		
	0.272	-18.00	3.56		}
	0.273	-19.95	2.71		
	0.274	-19.21	1.16		
	0.275	-18.90	-0.48		i
	0.276	-18.87	-1.24		
	0.277	-18.81	-1.17		
	0.278	-19.28	-2.95		
	0.279	-19.55	-4.32		<u> </u>
 	0.280	-19.19	-4.35		
	0.281	-18.78	-4.55	<u> </u>	
	0.282	-18.54	-4.20		
	0.283	-18.55	-3.38		
	0.284	-18.45	-1.65		
	0.285	-18.37	0.09		
	0.286	-17.32	-0.06		
-	0.287	-16.34	-0.79		
	0.288	-15.21	-0.54		
	0.289	-15.23	0.70		
	0.290	-15.59	1.66		
	0.291	-15.69	2.26		
	0.291				<u> </u>
<u> </u>	0.292	-15.49	1.20		
<u></u>		-15.52	1.43		1
	0.294	-15.57	2.07		<u> </u>
	0.295	-15.88	2.17		
	0.296	-15.95	2.42		
j	0.297	-15.57	2.31		i

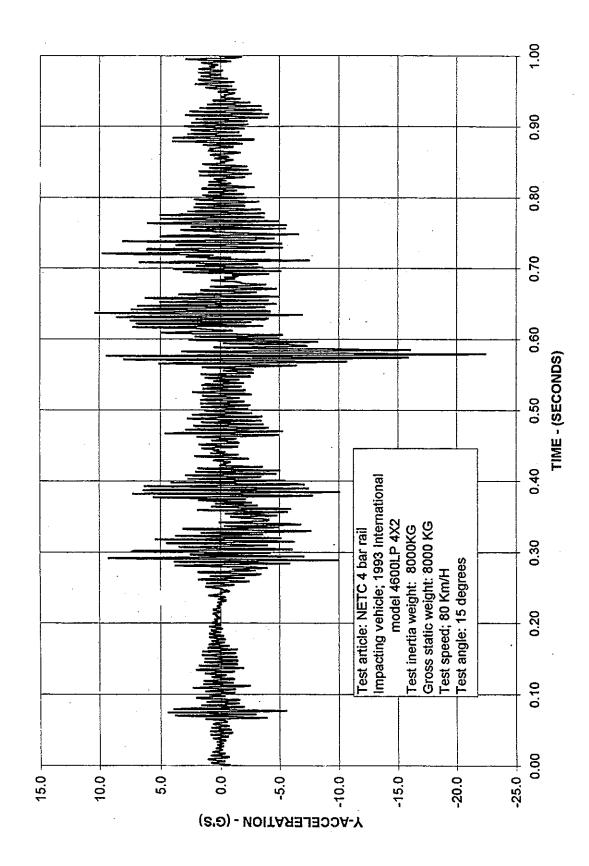
	0.298	-16.40	1.75	[
	0.299	-16.24	1.51	į	
	0.300	-16.38	0.68		
	0.301	-16.41	0.22		
	0.302	-16.58	-0.87	į	
	0.303	-16.65	-0.94	1	
	0.304	-16.76	-0.72		\neg
	0.305	-16.94	-0.73		
	0.306	-16.89	-1.17	į	
	0.307	-16.98	-1.55		
	0.308	-16.91	-1.26		
	0.309	-17.27	-0.61		
7	0.310	-17.19	0.42		
	0.311	-17.33	-0.10		
	0.312	-17.39	-1.39	•	
	0.313	-17.53	-2.18		
	0.314	-17.71	-1.86		
	0.315	-17.78	-1.37		
	0.316	-17.90	-0.70		
	0.317	-17.98	-0.29		
	0.318	-17.71	-0.10		
	0.319	-17.88	0.15		
	0.320	-17.49	0.85		
	0.321	-17.29	1.28		
	0.322	-16.89	1.18	,	
	0.323	-16.86	1.34	-	\dashv
	0.324	-17.12	1.40		
-	0.325	-17.35	0.57		
	0.326	-16.91	0.24	-	
	0.327	-17.31	0.66		
	0.328	-17.34	1.04		
	0.329	-16.88	0.81		
	0.330	-16.73	0.31		_
	0.331	-16.61	0.08		
	0.332	-16.64	0.00		
	0.333	-16.56	0.30		
	0.334	-16.42	0.00		
	0.335	-16.41	-0.10		
	0.336	-16.61	-0.42		
	0.337	-16.59	-1.05		
· ·	0.338	-16.78	-1.84		
	0.339	-16.79	-1.94		
	0.340	-16.79	-1.23		
	0.341	-16.82	-0.31		
	0.342	-16.88	0.02		
	0.343	-16.82	0.02		-
	0.344	-16.68	-0.04		
	0.345	-16.61	-0.04		
	0.345	-16.58			
			-0.66		
	0.347	-16.74	-0.48	<u> </u>	'
	0.348	16.77	-0.34		

0.349	-16.75	0.06	
0.350	-16.58	0.35	.,
0.351	-16.40	0.22	
0.352	-16.28	0.00	
0.353	-16.13	0.38	
0.354	-15.99	0.96	
0.355	-16.02	1.45	
0.356	-15.96	1.55	<u> </u>
0.357	-16.00	1.08	:
0.358	-16.11	0.65	
0.359	-16.13	0.32	
0.360	-16.17	0.07	<u> </u>
0.361	-16.05	0.06	
0.362	-15.95	0.31	!
0.363	-15.86	0.34	<u> </u>
0.364	-15.80	0.11	· · · · · · · · · · · · · · · · · · ·
0.365	-15.76	-0.17	
0.366	-15.75	-0.66	<u> </u>
0.367	-15.78	-1.41	
0.368	-15.79	-1.82	
0.369	-16.10	-1.62	
0.370	-16.13	-1.33	
0.371	-16.20	-1.02	
0.372	-16.01	-0.77	
0.373	-15.95	-0.59	
0.374	-15.88	-0.33	
0.375	-15.74	-0.16	
0.376	-15.74	0.02	
0.377	-15.71	0.39	
0.378	-15.86	0.90	
0.379	-15.88	1.08	
0.380	-16.02	0.92	
0.381	-16.07	0.80	
0.382	-16.17	0.86	
0.383	-16.09	0.97	
0.384	-16.01	1.00	
0.385	-15.90	0.85	
0.386	-15.73	0.38	Í
0.387	-15.67	-0.08	
0.388	-15.66	-0.24	
0.389	-15.65	-0.17	
0.390	-15.67	-0.28	
0.391	-15.89	-0.53	
0.392	-15.87	-0.77	
0.393	-15.97	-0.91	!
0.394	-15.89	-0.91	
0.395	-16.00	-0.73	
0.396	-15.74	-0.42	:
0.397	-15.58	-0.38	:
0.398	-15.67	-0.40	
0.399	-15.74	-0.46	
0.400	-15.99	-0.44:	•
0.700;	10.00	<i>-</i> ∿,44.	

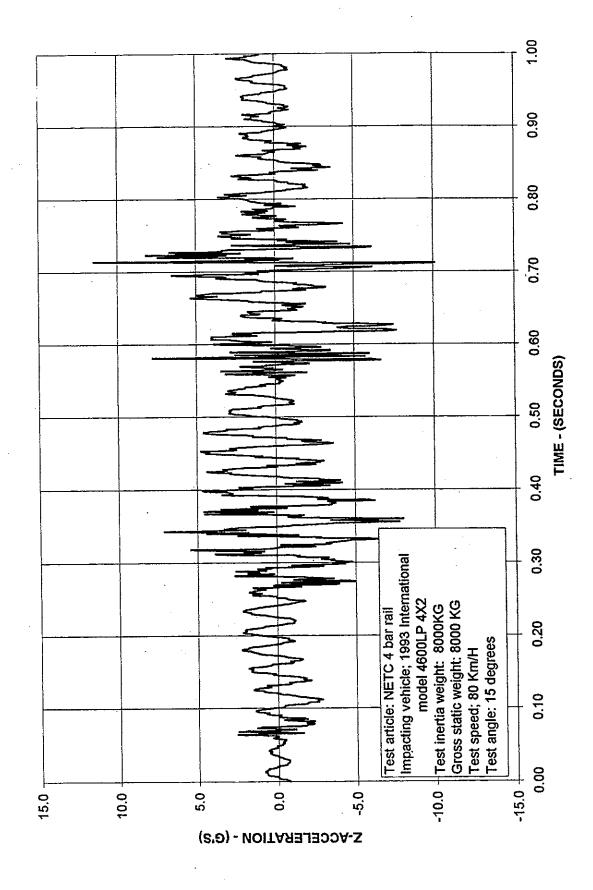


Vehicle C.G. longitudinal accelerometer plot - Test NETC-3.

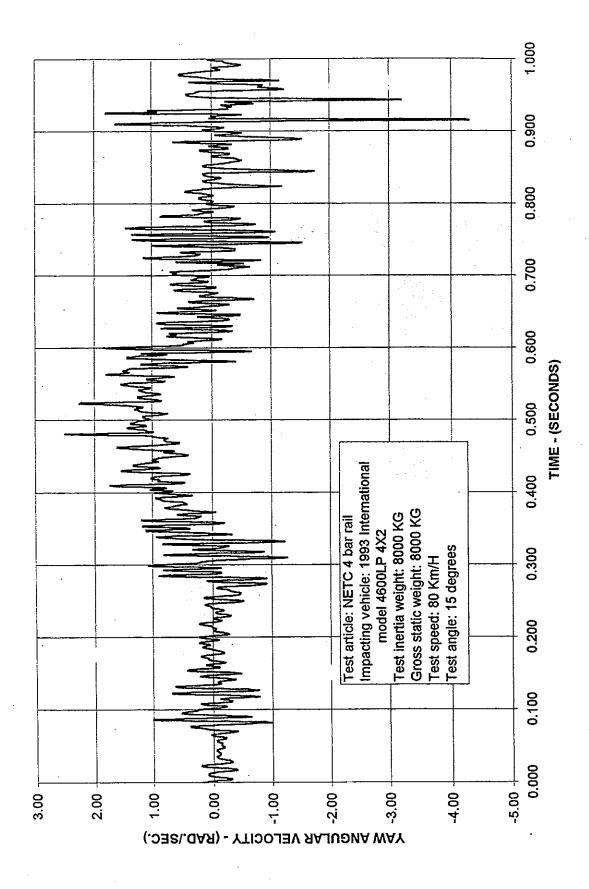
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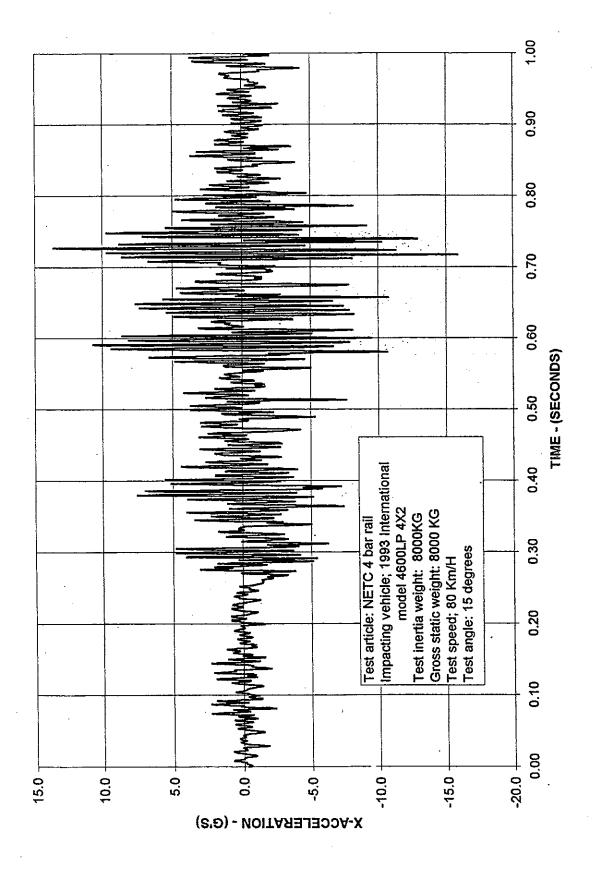
Vehicle C.G. lateral accelerometer plot - Test NETC-3.



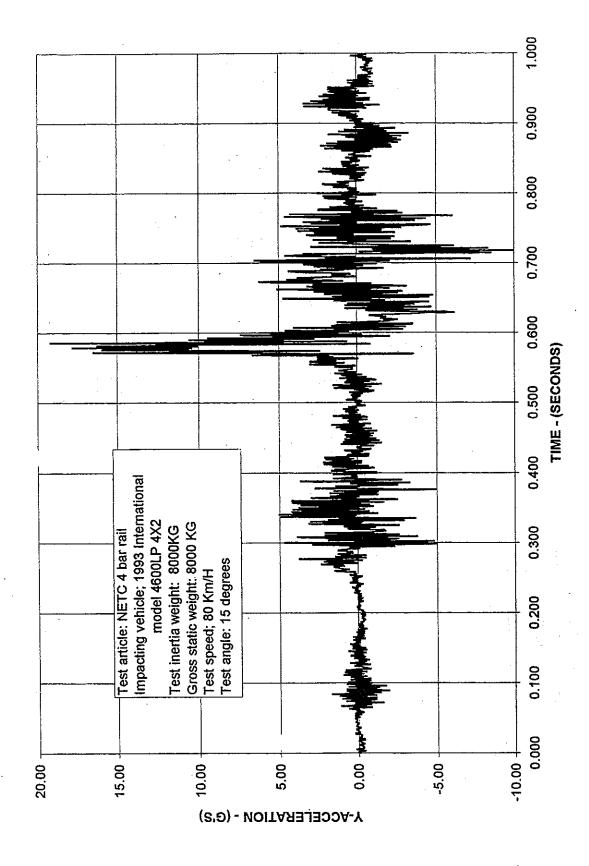
Vehicle C.G. vertical accelerometer plot - Test NETC-3.



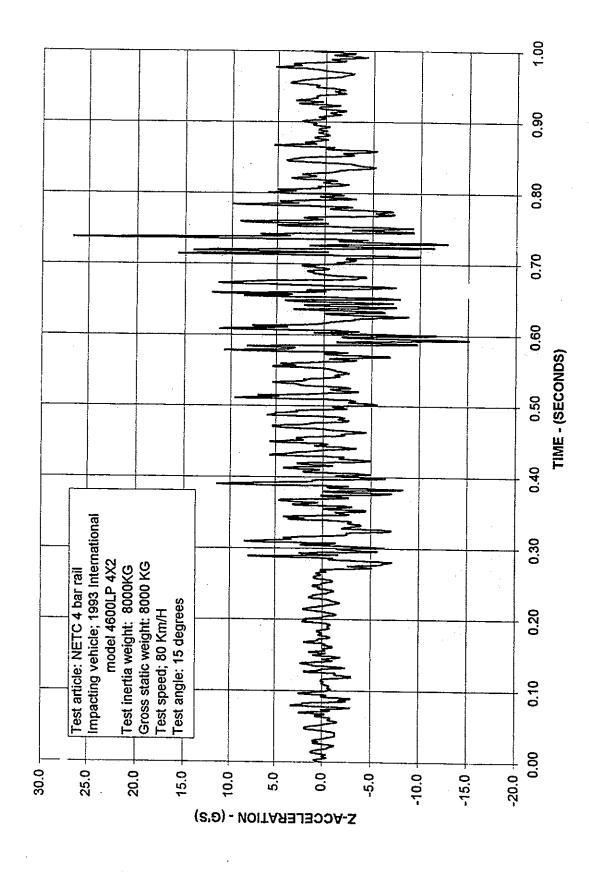
Rate gyro plot - Test NETC-3.



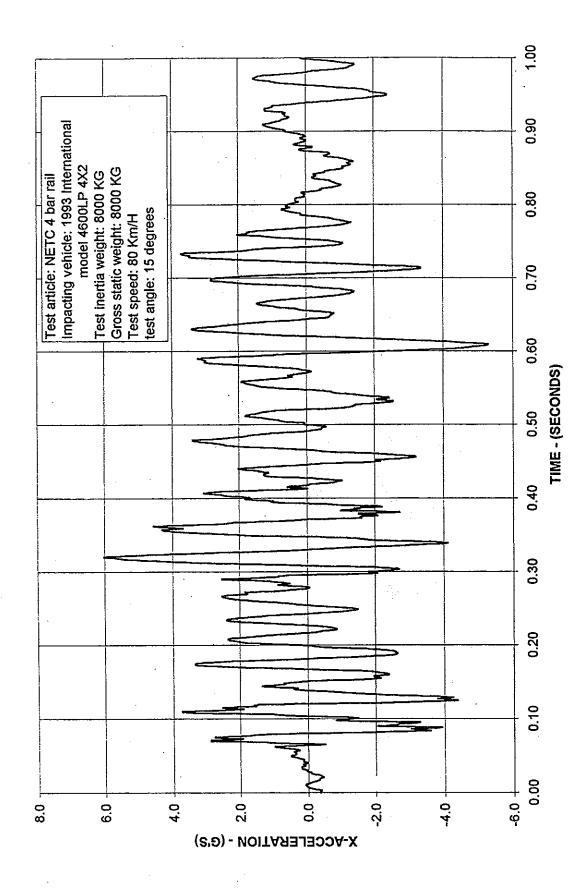
Rear axle longitudinal accelerometer plot - Test NETC-3.



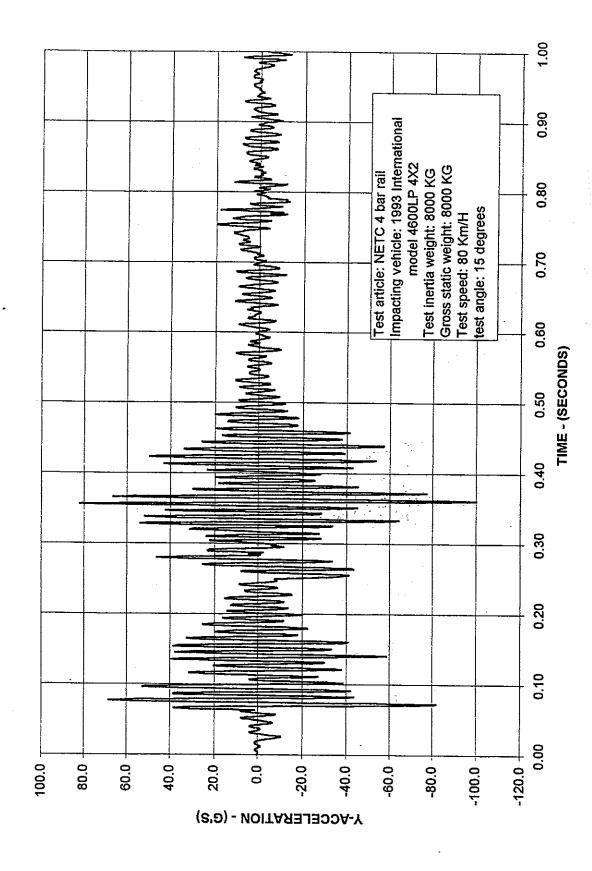
Rear axle lateral accelerometer plot - Test NETC-3.



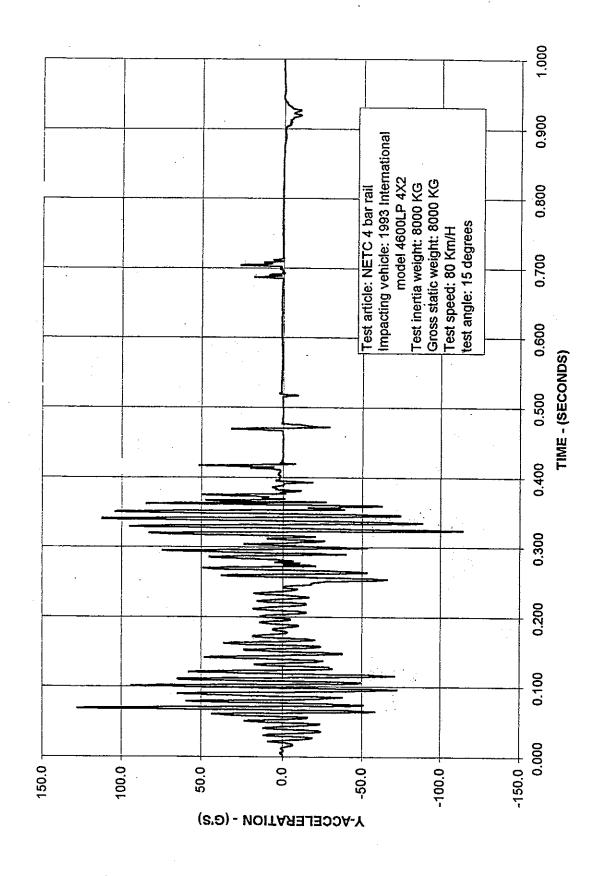
Rear axle vertical accelerometer plot - Test NETC-3.



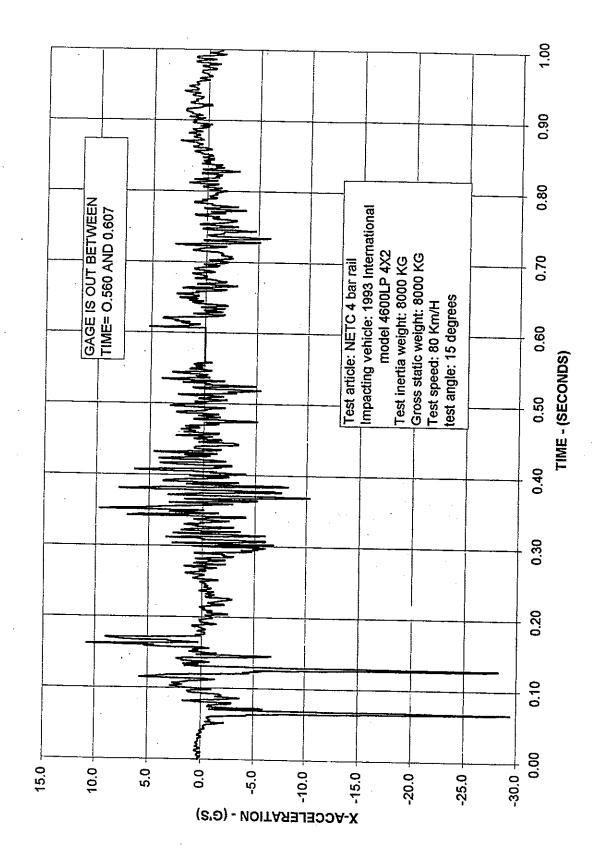
Top of engine longitudinal accelerometer plot - Test NETC-3.



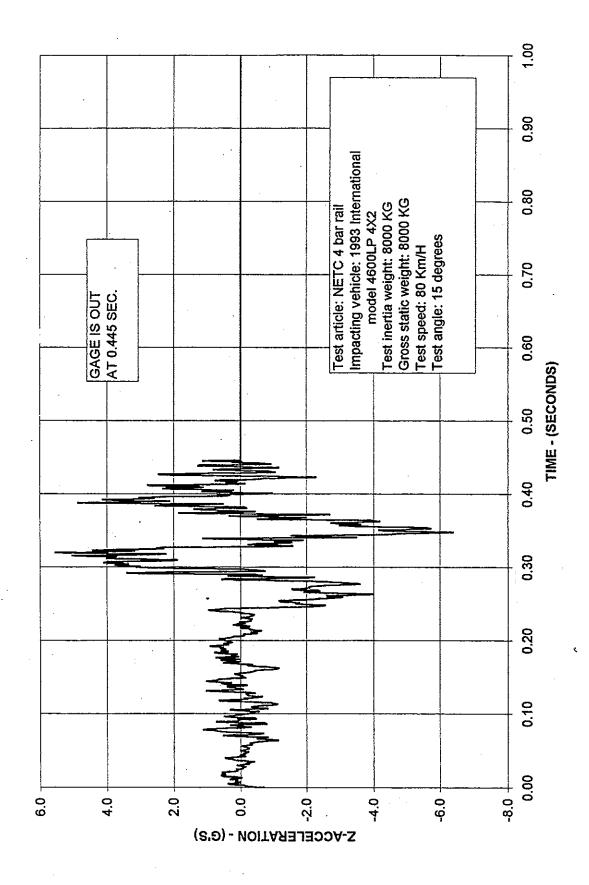
Right front disc brake longitudinal accelerometer plot - Test NETC-3.



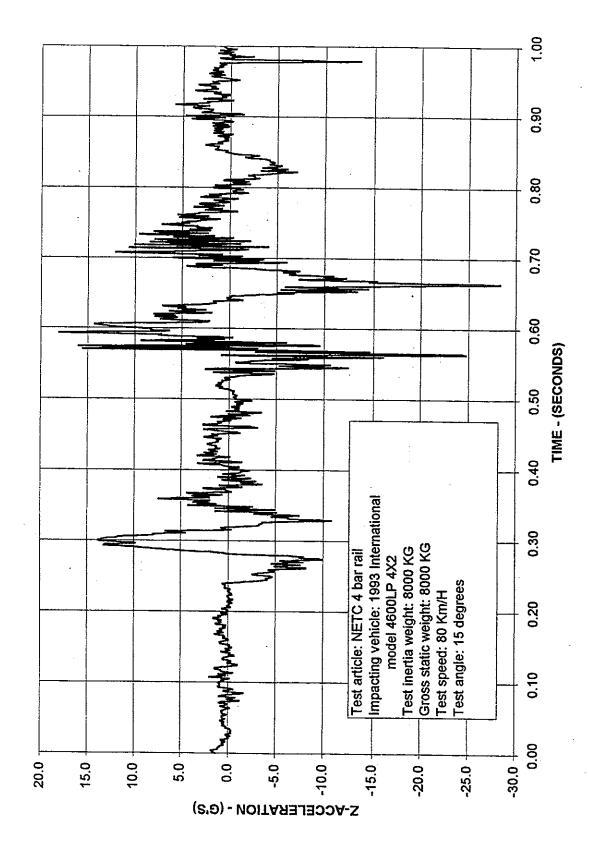
Left front disc brake longitudinal accelerometer plot - Test NETC-3.



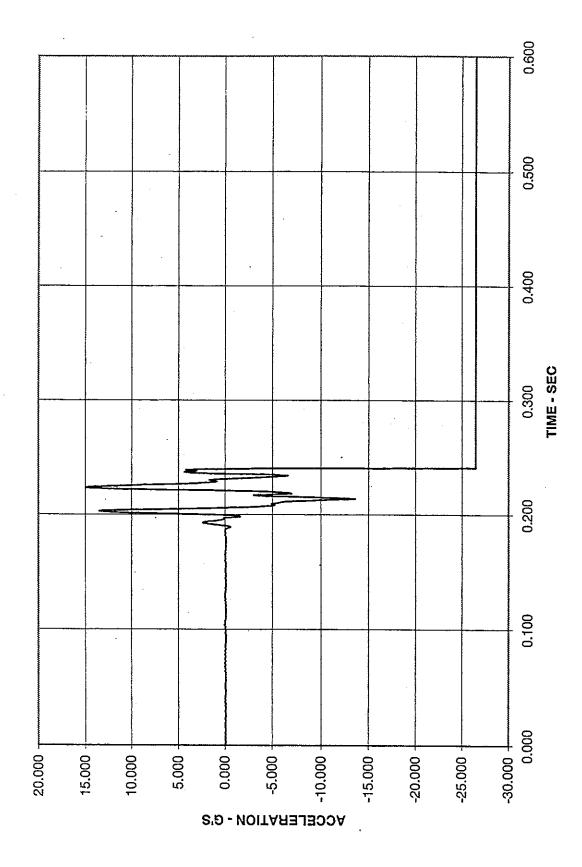
Instrument panel accelerometer plot - Test NETC-3.



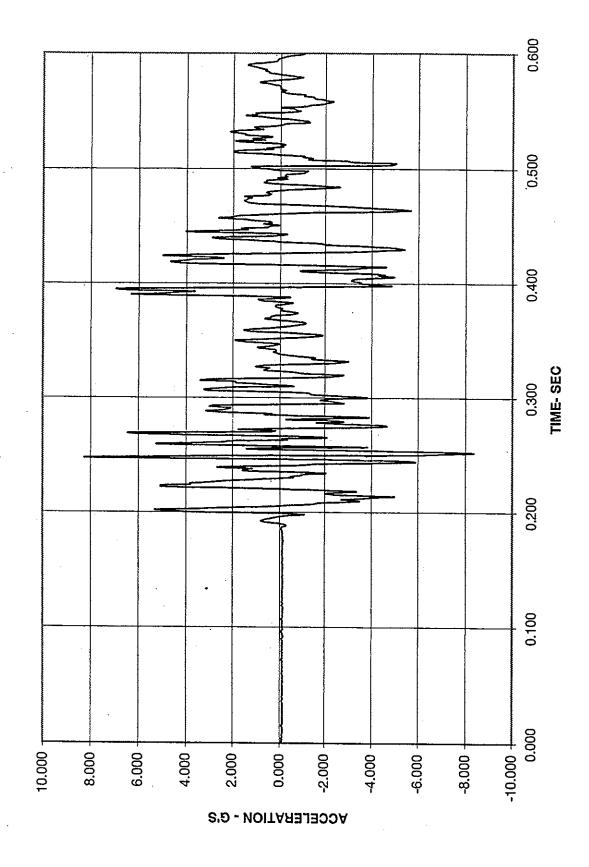
Right rear brake vertical accelerometer plot - Test NETC-3.



Left rear brake vertical accelerometer plot - Test NETC-3.



Top of post 7 lateral accelerometer plot - Test NETC-3.



Bottom of post 7 lateral accelerometer plot - Test NETC-3.

TRANSDUCER DATA WITH CALCULATED VEHICLE KINETICS AND OCCUPANT RISK SUMMARIES

TEST ID ----- NETC-3A
TEST DATE ---- 12-18-97
VEHICLE CLASS - OTHER
IMPACT SPEED -- 22.23 M/S

VEHICLE KINETICS SUMMARY NOTE: VALUES ARE INSTANTANEOUS AT TIME

TIME (S)	ACC			- HEAD. ANG(D)	VELO		(MPS) VERT.	D	ISP. Y	(M)
.000	.1	4	-1.2	15.0	22.2	. 0	.0	.0	. 0	.0
.010	-1.0	.9	1.0	15.0	22.2	. 1.	.0	.2	.1	
.020	.1	.7	.2	15.1	22.2	.1	.1	.4	.1	
.030	.0	.1	8	15.2	22.2	.1	.0	.6	.2	.0
.040	-1.5	-1.2	.5	15.2	22.1	.2	.0	.9	. 2	
.050	1	-1.7	5		22.0	.2	.1	1.1	.3	
.060	-1.1	4	.3		22.0	.2	.0	1.3	.3	
.070	3.6	7.7	-1.6	15.4	22.0	.2	.2	1.5	. 4	
.080	-4.1	4.3	-2.7		22.0	.2	.0	1.7	. 5	
.090	-1.1	1.5	7	15.4	22.1	.2	2	1.9	.5	.0
.100	-1.7	1.4	.6	15.3	22.0	. 2	.0	2.1	.6	
.110	-1.4	2.0	-3.9	15.3	21.9	.3	2	2.3	.6	
.120	4	.1	3		22.0	.3	5	2.6	.7	
.130	3	1.1	1.0		21.9	.3	3	2.8	.7	
.140	1.8	3.4	-2.4		22.0	.3	5	3.0	. 8	
.150	-1.1	2.7	2.5	15.6	22.0	.3	5	3.2	. 8	.0
.160	2.1	2.9	.6		21.8	.3	3	3.4	.9	
.170	2.1	1.9	-1.0		22.0	.3	5	3.6	1.0	
.180	2.6	1.9	3.7		21.9	.4	3	3.8	1.0	.0
.190	1.4	1.4	5		21.8	.4	2	4.0	1.1	.0
.200	9	1.4	1.7		21.9	.5	2	4.3	1.1	
.210	9				21.8	.5	.0	4.5	1.2	
.220	2.0	.7			21.8	.6	.0	4.7	1.2	
.230	-1.3	.1			21.9	.6	.0	4.9	1.3	
.240	-1.0	.7			21.7	.7	.3	5.1	1.3	
.250	.9	1.4	-1.0		21.8	.6	.1	5.3	1.4	
.260	-2.5	9	2.3		21.6	.7	.2	5.5	1.4	
.270	.4	-1.8	-7.3		21.3	.6	.3	5.7	1.5	.0
.280	-4.6	1.5	-2.9		21.4	.5	1	5.9	1.5	
.290	-7.3	-8.1	1.5		21.0	.3	.1	6.1	1.6	
.300	2.6	2.0	-5.8		21.0	.2	2	6.3	1.7	
.310	-13.6	-7.6	-4.1		21.0	.3	6	6.6	1.7	
.320		-10.1	.4		20.5	.4	3	6.8	1.8	
.330	11.8	-13.8	-7.9		20.3	.1	6	6.9	1.8	
.340		-10.5			20.5	2	9	7.1	1.9	
.350	-8.5	2	-1.4	15.8	19.9	7	5	7.3	1.9	1

(S) LONG. LAT. VERT. ANG (D) LONG. LAT. VERT. X Y Z
.360 1 -2.9 -15.4 15.5 20.0 -1.1 -1.1 7.5 2.0 -1 .370 -10.5 -5.3 10.0 15.2 19.7 -1.5 -1.2 7.7 2.1 -1 .380 -6 -14.3 -5.8 15.0 19.3 -1.7 -1.0 7.9 2.1 -1 .390 -5.8 -13.7 -3.1 14.6 19.7 -1.9 -1.6 8.1 2.2 -1 .400 -8.6 -6.6 3.5 14.2 19.2 -2.1 -1.2 8.3 2.3 -1 .410 -2.9 -9.2 -8.1 13.6 19.2 -2.5 -1.3 8.4 2.3 -1 .420 -2.8 -6.6 3.5 14.2 19.2 -2.5 -1.3 8.4 2.3 -1 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.
.370 -10.5 -5.3 10.0 15.2 19.7 -1.5 -1.2 7.7 2.1 -1 .380 6 -14.3 -5.8 15.0 19.3 -1.7 -1.0 7.9 2.1 -1 .390 -5.8 -13.7 -3.1 14.6 19.7 -1.9 -1.6 8.1 2.2 -1 .400 -8.6 -6.6 3.5 14.2 19.2 -2.1 -1.2 8.3 2.3 -1 .410 -2.9 -9.2 -8.1 13.6 19.2 -2.5 -1.3 8.4 2.3 -1 .420 -2.8 -6.7 2.4 13.1 19.3 -2.8 -1.6 8.6 2.4 -1 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .440 4.0 .2 -5.6 11.9 19.1 -3.5 -1.2 9.2 2.6 -2 .450 -5.7 8 7.5 11.4 19.1 -3.5 -1.2 </td
.380 6 -14.3 -5.8 15.0 19.3 -1.7 -1.0 7.9 2.1 -1 .390 -5.8 -13.7 -3.1 14.6 19.7 -1.9 -1.6 8.1 2.2 -1 .400 -8.6 -6.6 3.5 14.2 19.2 -2.1 -1.2 8.3 2.3 -1 .410 -2.9 -9.2 -8.1 13.6 19.2 -2.5 -1.3 8.4 2.3 -1 .420 -2.8 -6.7 2.4 13.1 19.3 -2.8 -1.6 8.6 2.4 -1 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.3 -1.3 9.0 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.6 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2
.390 -5.8 -13.7 -3.1 14.6 19.7 -1.9 -1.6 8.1 2.2 -1 -1 .400 -8.6 -6.6 3.5 14.2 19.2 -2.1 -1.2 8.3 2.31 .410 -2.9 -9.2 -8.1 13.6 19.2 -2.5 -1.3 8.4 2.31 .420 -2.8 -6.7 2.4 13.1 19.3 -2.8 -1.6 8.6 2.41 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.52 .440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.3 9.0 2.52 .450 -5.7 8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.62 .460 .5 -2.7 .0 11.0 18.8 -3.77 9.3 2.72 .470 .9 -10.14 10.4 19.0 -3.9 -1.1 9.5 2.82 .480 -3.1 -6.9 6.6 9.9 18.8 -4.27 9.7 2.82 .490 1.2 -6.0 -2.4 9.1 18.6 -4.55 9.9 2.92 .500 .45 7.8 18.8 18.5 -5.13 10.2 3.12 .510 -1.8 1.6 4.5 7.8 18.5 -5.32 10.4 3.12 .520 1.8 3.0 -1.3 7.1 18.5 -5.32 10.4 3.12 .530 8 2.9 1.9 6.3 18.6 -5.73 10.6 3.22 .540 -1.0 1.4 3.0 5.7 18.3 -6.2 .2 10.9 3.42 .550 2.2 3.75 4.9 18.3 -6.2 .2 10.9 3.42 .550 -1.9 3.7 2.5 4.9 18.3 -6.2 .2 10.9 3.42 .560 -1.9 3.7 2.5 3.8 2.6 17.4 -9.1 .1 11.6 3.72
.400
.410 -2.9 -9.2 -8.1 13.6 19.2 -2.5 -1.3 8.4 2.3 -1 .420 -2.8 -6.7 2.4 13.1 19.3 -2.8 -1.6 8.6 2.4 -1 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.3 9.0 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.6 -2 .460 .5 -2.7 .0 11.0 18.8 -3.7 7 9.3 2.7 2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5
.420 -2.8 -6.7 2.4 13.1 19.3 -2.8 -1.6 8.6 2.4 -1 .430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.3 9.0 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.3 -1.2 9.2 2.6 -2 .460 .5 -2.7 .0 11.0 18.8 -3.7 7 9.3 2.7 -2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 -2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 -2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 -5 9.9 2.9 -2 .500 .4 5 .7 8.4 18.8 -4.5 -5 9.9
.430 .1 1.0 3.7 12.6 19.0 -3.1 -1.1 8.8 2.5 -2 .440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.3 9.0 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.6 -2 .460 .5 -2.7 .0 11.0 18.8 -3.7 -7 7 9.3 2.7 -2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 -2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 -2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 -2 .500 .4 5 .7 8.4 18.8 -5.1 -3 10.1 3.0 -2 .510 -1.8 1.6 4.5 7.8 18.5 -5.3 -2
.440 4.0 .2 -5.6 11.9 19.1 -3.3 -1.3 9.0 2.5 -2 .450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.6 -2 .460 .5 -2.7 .0 11.0 18.8 -3.7 7 9.3 2.7 2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 1
.450 -5.7 .8 7.5 11.4 19.1 -3.5 -1.2 9.2 2.6 2 .460 .5 -2.7 .0 11.0 18.8 -3.7 7 9.3 2.7 2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1
.460 .5 -2.7 .0 11.0 18.8 -3.7 7 9.3 2.7 2 .470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 1
.470 .9 -10.1 4 10.4 19.0 -3.9 -1.1 9.5 2.8 2 .480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 <t< td=""></t<>
.480 -3.1 -6.9 6.6 9.9 18.8 -4.2 7 9.7 2.8 2 .490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -6.2 .2 10.9 3.4 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3<
.490 1.2 -6.0 -2.4 9.1 18.6 -4.5 5 9.9 2.9 2 .500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 </td
.500 .4 5 .7 8.4 18.8 -4.8 7 10.1 3.0 2 .510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 </td
.510 -1.8 1.6 4.5 7.8 18.5 -5.1 3 10.2 3.1 2 .520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11
.520 1.8 3.0 -1.3 7.1 18.5 -5.3 2 10.4 3.1 2 .530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 1
.530 8 2.9 1.9 6.3 18.6 -5.7 3 10.6 3.2 2 .540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12
.540 -1.0 1.4 3.0 5.7 18.3 -5.9 .1 10.8 3.3 2 .550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 <td< td=""></td<>
.550 2.2 3.7 5 4.9 18.3 -6.2 .2 10.9 3.4 2 .560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.0 2 .630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6 12.5 4.2
.560 -1.9 3.7 2.5 4.4 18.1 -6.6 .3 11.1 3.4 2 .570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.0 2 .630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6
.570 .8 8.5 8 3.6 17.9 -7.2 .4 11.3 3.5 2 .580 -4.4 -17.5 .7 3.1 17.6 -8.3 .1 11.5 3.6 2 .590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.7 2 .600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.0 2 .630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6 12.5 4.2 2 .650 3 -9.8 -1.7 1.4 17.1 -9.1 5 12.7 4.3 2 .660 -4.4 -9.9 2.5 1.3 17.2 -8.9 6 12.8 4.4<
.580
.590 7.2 -12.5 -3.8 2.6 17.4 -9.1 .1 11.6 3.72 .600 14.5 -5.3 6.4 2.3 17.6 -9.71 11.8 3.82 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.92 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.02 .630 -6.7 5.2 -5.8 1.6 17.4 -9.66 12.3 4.12 .640 -4.0 -7.6 3.8 1.5 17.1 -9.36 12.5 4.22 .6503 -9.8 -1.7 1.4 17.1 -9.15 12.7 4.32 .660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.0 2 .630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6 12.5 4.2 2 .650 3 -9.8 -1.7 1.4 17.1 -9.1 5 12.7 4.3 2 .660 -4.4 -9.9 2.5 1.3 17.2 -8.9 6 12.8 4.4 2 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.5 2
.600 14.5 -5.3 6.4 2.3 17.6 -9.7 1 11.8 3.8 2 .610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.9 2 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.0 2 .630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6 12.5 4.2 2 .650 3 -9.8 -1.7 1.4 17.1 -9.1 5 12.7 4.3 2 .660 -4.4 -9.9 2.5 1.3 17.2 -8.9 6 12.8 4.4 2 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.5 2
.610 5.1 4.1 6.6 1.9 17.2 -10.0 .3 12.0 3.92 .620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.02 .630 -6.7 5.2 -5.8 1.6 17.4 -9.66 12.3 4.12 .640 -4.0 -7.6 3.8 1.5 17.1 -9.36 12.5 4.22 .6503 -9.8 -1.7 1.4 17.1 -9.15 12.7 4.32 .660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.620 -1.2 -1.7 -11.9 1.7 17.3 -9.8 .2 12.2 4.02 .630 -6.7 5.2 -5.8 1.6 17.4 -9.66 12.3 4.12 .640 -4.0 -7.6 3.8 1.5 17.1 -9.36 12.5 4.22 .6503 -9.8 -1.7 1.4 17.1 -9.15 12.7 4.32 .660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.630 -6.7 5.2 -5.8 1.6 17.4 -9.6 6 12.3 4.1 2 .640 -4.0 -7.6 3.8 1.5 17.1 -9.3 6 12.5 4.2 2 .650 3 -9.8 -1.7 1.4 17.1 -9.1 5 12.7 4.3 2 .660 -4.4 -9.9 2.5 1.3 17.2 -8.9 6 12.8 4.4 2 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.5 2
.640 -4.0 -7.6 3.8 1.5 17.1 -9.36 12.5 4.22 .6503 -9.8 -1.7 1.4 17.1 -9.15 12.7 4.32 .660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.6503 -9.8 -1.7 1.4 17.1 -9.15 12.7 4.32 .660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.660 -4.4 -9.9 2.5 1.3 17.2 -8.96 12.8 4.42 .670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.670 2.1 -3.0 7.2 1.4 17.0 -9.0 .0 13.0 4.52
.690 -8.9 -1.0 4.8 1.1 17.0 -9.52 13.3 4.72
.700 -9.7 -4.2 -1.2 1.0 16.7 -9.6 .3 13.5 4.82
.710 24.3 -7.8 -7.6 .8 16.9 -9.6 .0 13.7 4.92
.720 -38.4 14.2 16.1 1.0 17.2 -9.6 .0 13.8 5.02
.730 -17.6 -4.1 5.3 .8 16.4 -9.4 .7 14.0 5.12
- 1/40 40.5 -5.5 .5 .6 .6 .6 .7.5 .5 .4.2 5.2 - 2
.750 7.95 4.7 .8 16.6 -9.5 .6 14.3 5.32
.760 1.1 -1.5 1.0 .7 16.5 -9.5 .9 14.5 5.42
.770 -1.8 9.4 .3 .6 16.5 -9.5 .6 14.7 5.52
.7804 5.2 3.2 .8 16.4 -9.5 .7 14.8 5.62
.790 1.7 2.3 -3.1 .6 16.3 -9.6 .8 15.0 5.72
.800 -4.1 -4.1 3.1 .6 16.4 -9.6 .9 15.1 5.82

TIME	ACC	EL. (6	3'S)	HEAD.	VELO	CITY	(MPS)	D	ISP.	(M)
(S)	LONG.			ANG (D)	LONG.	LAT.	VERT.	X	Y	Z
.810	-2.2	-2.7	1.0	.6	16.2	-9.6	1.2	15.3	5.9	2
.820	-3.1	-2.0	-3.4	.5	16.3	-9.7	1.0	15.5	6.0	2
.830	-3.5	6	2.8	.7	16.3	-9.7	1.0	15.6	6.1	2
.840	4	-2.8	-5.2	.7	16.1	-9.7	1.1	15.8	6.2	1
.850	2.4	.3	-1.2	1.0	16.3	-9.6	.8	16.0	6.3	-,1
.860	-2.2	1.4	4.1	1.1	16.1	-9.7	.8	16.1	6.4	1
.870	5.7	. 3	-1.8	1.2	16.1	-9.6	.9	16.3	6.5	1
.880	7	2.4	.1	1.3	16.3	-9.5	. 7	16.4	6.6	1
.890	.1	4.3	4.0	1.5	16.2	-9.4	1.0	16.6	6.7	1
.900	2.4	5.8	.5	1.8	16.2	-9.3	1.0	16.8	6.8	1
.910	.2	4.2	3.4	1.6	16.1	-9.3	1.0	16.9	6.8	1
.920	4.1	2.9	.0	2.1	16.1	-9.3	1.2	17.1	6.9	1
.930	~.5	-2.1	8	1.7	16.1	-9.5	1.1	17.2	7.0	1
.940	-1.9	-1.7	3.1	1.9	16.0	-9.5	1.3	17.4	7.1	.0
.950	2.1	.4	5	2.4	16.0	-9.5	1.4	17.5	7.2	.0
.960	.3	3.7	2.1	2.6	16.1	-9.4	1.4	17.7	7.3	.0
.970	-2.2	2.2	2.1	2.8	16.0	-9.3	1.6	17.9	7.4	.0
.980	1.3	1.5	8	2.8	16.0	-9.2	1.6	18.0	7.5	.0
.990	-1.4	2.9	2.2	2.8	16.0	-9.0		18.2	7.6	.0

HIGHEST 50.0-MS AVG. ACCEL.

		TIME	(SEC)
	G'S	START	END
LONG.	-2.72	.308	.358
LAT.	-5.79	.557	.607

TEST ID ----- NETC-3A
TEST DATE ---- 12-18-97
VEHICLE CLASS - OTHER
IMPACT SPEED -- 22.23 M/S

OCCUPANT RISK SUMMARY

NOTE: INSTANTANEOUS 10-MS AVERAGE ACCELERATIONS

	(VEHICLE	3)	(occi	JPANT	}
TIME	ACCEL.	(G'S)	ANG.VEL	VEL.		DISP.	(M)
(S)	LONG.		(RAD/S)	LONG.	LAT.	LONG.	LAT.
.000	.11	41	.17	.00	.00	.00	.00
.010	55	.38	.09	.14	.66	.00	.02
.020	30	.28	06	.44	1.78	.01	.04
.030	03	.08	26	.78	3.30	.01	.06
.040	-1.03	.03	11	.59	2.27	.02	.08
.050	23	17	14	.71	2.54	.03	.09
.060	.15	.08	20	.81	3.02	.03	.11
.070	63	.78	40	1.20	4.51	.04	.14
.080	.71	82	36	1.11	4.20	.04	.14
.090	.30	-:01	63	1.48	6.14	.05	.16
.100	-2.04	.51	.24	.09	18	.05	.16
.110	1.17	07	17	.86	2.79	.06	.17
.120	~.48	02	21	.84.	3.27	.07	.21
.130	34	.55	.31	.05	53	.07	.22
.140	1.11	13	21	.88	3.25	.08	.22
.150	-1.20	02	46	1.28	5.06	.08	.24
.160	13	01	.02	.63	1.59	.09	.25
.170	.75	.48	. 07	.37	1.19	.09	.26
.180	-1.67	.52	13	.85	2.73	.10	.27
.190	1.07	.65	.07	.54	1.27	.11	.28
.200	38	.70	.22	.20	.20	.11	.28
.210	-1.00	.54	04	.78	2.19	.12	.29
220	1.51	.43		.47	1.18*	.12	.30*
.230	-1.22	03	30	1.11	4.22	.13	.31
.240	45	.06	01	.78	2.16	.14	.33
.250	.43	12	51	1.53	5.76	. 1.5	.34
.260	-4.58	40	45	1.66	5.39	.16	.37
.270	-1.61	-1.36	24	1.62	3.88	.17	.39
.280	12	-2.49	67	2.19	6.98	.19	.44
.290	-2.01	-1.08	12	1.66	2.75	.20	.45
.300	.95	42	.97	18	-5.27	.21	.43
.310	86	.14	-1.26	3.60	11.05	.23	.45
.320	-5.96	91	04	2.03	2.27	.25	.48
.330	.27	-2.77	.03	2.10	1.54	.27	.48
.340	-2.89	-4.74	. 63	.95	-3.17	.29	.50
.350	-1.98	-4.07	.38	1.96	-1.96	.31	.49

		(VEHICLE	§)	(occ	UPANT)
TI	EME	ACCEL.		ANG. VEL	VEL.		DISP.	(M)
((S)	LONG.	LAT.	(RAD/S)			LONG.	LAT.
	360	.54	-3.66	.50	1.69		.33	.47
	.370	-7.78	-1.73	.58		-4.49	.35	.46
	.380	3.19	82	.71	2.05	-5.69	.37	.46
	.390	35	56	.83	1.41	-6.83	.39	.44
	400	-4.15	-2.19	.96	1.67	-8.17	.42	.41
	410	2.93	-2.09	1.74	.46	-14.39	.44	.37
	420	-1.95	-1.61		1.57		.46	.33
	430		29	1.54		-13.94	.48	.30
	440	2.59	.12	1.19	1.40	-11.99	.50	.24
	450	-3.00	.01	.61	2.41	-8.17	.52	.20
	460	.29	-1.00	1.24	1.69	-12.99	.55	.18
	470	1.41	86	.69		-9.52	.57	.13
	480	-2.91	-1.02	2.00	.36+		.59+	.09
	490	1.24	57	1.41	1.52	-15.85	.60	.02
	500	.03	91	1.12	1.86	-14.39	.62	05
	510	-1.15	47	.86	2.50	-12.96	.64	09
	520	1.80	33	1.43	1.54	-17.65	.66	15
	530	46	36	1.16		-16.30	.67	23
	540	-1.38	32	1.18		-16.93	.69	28
	550	.48	-1.47	1.54	1.55	-20.09	.70	~.35
	560	-1.54	-2.65	. 63	3.14	-14.11	.73	39
	570	-1.46	-5.47	1.43	2.06	-20.87	.74	47
	580	-1.17	-8.87*		4.34	-13.15	.76	50
	590	.81	-7.54	.86	3.38	-19.05	.79	51
	600	-1.72	-3.26	1.85	1.55	-26.92	.83	50
	610	-2.00 2.51	.28	.14	4.76	-14.89	.86	49
	.620 .630	1.23	3.58 2.11	.70	3.69	-18.91	.90	46
	640	-4.45	3.54	34	5.34	-11.14	.95	41
		1.80		26 .50	5.52		.99	38
	.650 .660	68	.98 .92	29	4.27	-16.77	1.04	34
	670	-1.82	-1.93	02	5.45 5.16	-10.98 -12.93	1.09	30
	680	1.49	-2.39	.62	4.13	-17.98	1.14	24
	690	-1.79	~1.30	.30	4.64	-15.90	1.19	21
	700	.48	86	.30	4.96	-16.10	1.23 1.28	18 15
	710	-3.01	~1.43	33	5.78	-11.62	1.33	12
	720	2.17+	3.78	32	5.41	-11.61	1.39	05
	730	.87	.77	.19	5.36	-15.19	1.44	02
	740	75	16	.22	5.11	-15.25	1.49	.03
	750	-3.92	.26	1.33	3.27	-23.50	1.55	.03
	760	1.51	22	91	7.11	-7.34	1.60	.11
	770	1.21	39	54	6.47	-10.04	1.65	.15
	780	-2.81	06	28	6.20	-11.80	1.71	.23
	790	.26	56	.21	5.48	-15.51	1.77	.25
	800	57	.04	.08	5.59	-14.59	1.82	.31
							02	

TIME ACCEL. (G'S) ANG.VEL VEL. (M/S) DISP. (M) (S) LONG. LAT. (RAD/S) LONG. LAT. LONG. LAT. .8107137 .02 5.85 -14.19 1.88 .35 .820 1.4629 .14 5.56 -15.19 1.94 .39 .830 -2.2699 .12 5.64 -14.98 2.00 .47 .8402856 .13 5.81 -15.10 2.06 .53 .850 .97 .02 .03 5.78 -14.11 2.13 .64 .860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC. (GS)		(VEHICLE	} (occt	JPANT)
.8107137 .02 5.85 -14.19 1.88 .35 .820 1.4629 .14 5.56 -15.19 1.94 .39 .830 -2.2699 .12 5.64 -14.98 2.00 .47 .8402856 .13 5.81 -15.10 2.06 .53 .850 .97 .02 .03 5.78 -14.11 2.13 .64 .860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
.820	(S)	LONG.	LAT.	(RAD/S)	LONG.	LAT.	LONG.	LAT.
.820								
.830 -2.2699 .12 5.64 -14.98 2.00 .47 .8402856 .13 5.81 -15.10 2.06 .53 .850 .97 .02 .03 5.78 -14.11 2.13 .64 .860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
.8402856 .13 5.81 -15.10 2.06 .53 .850 .97 .02 .03 5.78 -14.11 2.13 .64 .860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
.850 .97 .02 .03 5.78 -14.11 2.13 .64 .860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
.860 -1.914450 6.82 -10.30 2.19 .70 .870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)		•		•				
.870 .64 .6719 6.34 -12.43 2.25 .78 .880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
.880 .57 .88 .04 5.76 -14.00 2.31 .84 .890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 .222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)							— —	
.890 -1.12 .96 -1.39 8.31 -3.41 2.37 .93 OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
OCCUP. RISK FACTORS TIME VELOCITY (S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)								
(S) (M/S) >LONG. VEL. AFTER 0.6 M DISP488 1.65 >LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)	.890	-1.12	.96	-1.39	8.31	-3.41	2.37	.93
>LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)	OCCUP.	RISK FA	ACTORS					
>LAT. VEL. AFTER 0.3 M DISP222 -2.89 MAX. ACCEL. AFTER OCCUPANT IMPACT TIME(S) ACC.(GS)	>LON	G. VEL.	AFTER 0	.6 M DISP		.488	1.65	
	MAX. A	CCEL. A	FTER OCC	UPANT IMPA	ACT	TIME(S)	ACC. (GS)	
>LONG. ACCELERATION725 -8.95	>LON	G. ACCEI	LERATION			725	-8 95	
>LAT. ACCELERATION582 14.30								

TEST ID ----- NETC-3B
TEST DATE ---- 12-18-97
VEHICLE CLASS - OTHER
IMPACT SPEED -- 22.23 M/S

TIME (SEC)	(VEL. X	CG ACC	CEL(G' Z	S)) R	(VEL. X	REAR Y	ACCEL	(G'S)) R
.000	.1	2	7	.7	3 .2	1 2	.1	.4 .5
.010	6	.5	.7	1.0 .5	.6	3	4 6	.s .9
.020	.1 .0	.4	.1 5	.5	-1.1	1	1.0	1.4
.030	.0 9	6	5	1.1	.2	.1	-1.3	1.4
.050	1	8	3	.9	9.	.2	1.2	1.5
.060	6	3 2	2	.7	.3	.2	7	.8
.070	1.8	3.8	5	4.2	.4	.2	1.5	1.6
.080	-2.5	2.5	-1.8	4.0	6	.2	2.8	2.8
.090	3	.8	2	.8	.1	-1.3	-1.7	2.1
.100	9	.6	.3	1.1	~.7	8	5	1.2
.110	8	.9	-2.5	2.8	7	1	.0	.7
.120	2	.1	1	.3	5	8	-2.9	3.0
.130	1	.6	. 6	.9	1.0	~.5	.0	1.1
.140	1.0	1.8	-1.6	2.6	6	3	.7	1.0
.150	8	1.3	1.6	2.2	1.1	4		1.5
.160	1.1	1.5	.3	1.9	.6	1		.9
.170	1.2	1.0	6	1.7	9	4		1.2
.180	-1.7	.9	2.2	2.9	4	3		.5
.190	.9	. 8	4	1.3	.6	4		.9
.200	6	.8	1.0	1.4	-1.5	4		2.4
.210	6	.3	1.2	1.4	.8	1		.9
.220	1.3	.4	-1.1	1.8	.7	2	4	. 9
.230	8	.0	1.6	1.8	2 1	.0	1.0 -1.1	1.0 1.2
.240	6 .7	.4 .8	:4 6	.8 1.2	1 4	.0	-1.1	.6
.250 .260	-1.8	.o 5	1.5	2.4	-1.4	1.5	.9	2.2
.270	.5	-1.0	-3.8	4.0	.0	1.9	.2	1.9
.280	-2.3	.9	-1.7	3.0	1.8	1.5		7.3
.290	-4.3	-4.1	.8	6.0	-2.0	1.0	1.7	2.9
.300	1.7	1.3	-3.8	4.3	2.7	4.7	-3.0	6.2
.310	-7.9	-4.0	-1.1	8.9	-1.8	-1.6	8.4	8.8
.320	.0	-5.1	.2	5.1	-1.5	.6	-2.4	2.9
.330	6.9	-7.6	-4.5	11.2	.7	3.0	-3.0	4.3
.340	-1.4	-5.9	4.4	7.5	-3.2	5.0	2.7	6.5
.350	-5.1	9	4	5.2	2.2	3.8	-1.3	4.5
.360	.6	-1.8	-8.0	8.2	-1.3	4.2	. 5	4.4
.370	-6.6	-2.6	4.6	8.4	-2.5	.7	-1.4	3.0
.380	.5	-7.8	-3.5	8.5	7.5	1		7.5
.390	-3.0	-7.4	-2.3	8.3	-4.4	-2.7		12.5
.400	-5.6	-3.8	2.5	7.3	.8	-1.2	-3.8	4.0

TIME (SEC)	(VEL. X	CG AC	CEL(G' Z	S)) R	(VEL. X	REAR Y	ACCEL	(G'S)) R
.410	9	-4.7	~4.2	6.4	-3.0	7	.4	3.1
.420	-1.5	-3.5	1.5	4.1	4.4	.3	1.6	4.7
.430	2	.4	2.0	2.1	7	3	3.0	3.1
.440	2.9	2	-3.1	4.2	1	1	-3.1	3.1
.450	-3.7	.4	4.4	5.7	1.0	7	5.6	5.7
.460 .470	.3 .7	-1.3 -5.3	.1 8	1.3 5.4	1.8 -3.3	-1.2 8	-1.8	2.8
480	-1.8	-3.6	4.1	5.8	1.8	~.8 ~.5	4.8 -2.0	5.9 2.7
.490	.9	-3.2	-1.3	3.6	-4.0	.4	5.1	6.5
.500	. 2	4	.5	.7	3.5	1	-2.5	4.2
.510	-1.1	.8	2.8	3.2	3	2	4.8	4.8
.520	1.2	1.5	9	2.1	4	7	-3.5	3.6
.530	5	1.4	1.4	2.1	.5	8	2.6	2.7
.540	6	.5	1.9	2.1	9	3	-1.2	1.5
.550	1.1	1.6	4	2.0	1.0	.3	-1.1	1.5
.560 .570	-1.3	1.5	1.0	2.2	1.2	1.3	3.0	3.5
.580	1.0 -2.9	4.5 -11.3	.5 .7	4.6 11.7	-4.6	-3.5	-6.8	9.0
.590		-7.3	-1.5	8.6	-10.7 10.2	14.6 10.6	3.7 -1.4	18.5
.600	8.0	-2.8	. 3.8	9.3		6.2	-1.4 -11.7	14.8 16.3
.610	2.8	2.5	4.0	5.5	-5.4	1.6	5.3	7.7
.620	6	5	-7.1	7.1	1.2	-2.0	-2.1	3.2
.630	-4.2	2.8	-3.3	6.0	4.9	-5.6	1	7.4
.640	-2.7	-3.9	2.1	5.1	-4.1	-2.6	-3.6	6.1
.650	.6	-4.7	-1.2	4.9	1.4	-2.0	-3.5	4.3
.660	-2.4	-4.9		5.7	1	-2.8	3.8	4.8
.670	.8	-1.8	4.0	4.5	4.7	.1 1.6	1.4	4.9
.680 .690	1.1 -5.1	-1.7	-2.4	3.1	3.2	1.6	-3.6	5.1
.700	-5.1 -5.4	-1.0 -1.7	2.8	5.9 5.7	1.7 -2.2	.8	1.7	2.6
.710	12.7	-4.1	-5.0	14.3	1.1	.8 4.6	-1.5 -8.3	2.8 9.6
.720	-22.5	8.6	7.5	25.2	9.7	-1.0	11.8	15.3
.730	-10.3	-3.2	2.9	11.2	-4.6	1	-11.6	12.4
.740	5.7	-3.0	8	6.5	-12.6	3.2	3.7	13.5
.750		9	2.7	5.1	1.9	1.3	-7.8	8.1
.760	.0	-1.8	∴2	1.9	2.1	1.4	9.1	9.4
.770	-1.0	5.0	.0	5.1	-2.4	4.2	-7.2	8.7
.780	6	2.7	1.8	3.3	9	1.6	-2.8	3.3
.790	1.3 -2.4	1.0	-1.3	2.1	2.4	.6	1.6	2.9
.800 .810	-2.4 -1.2	-2.2 -1.4	1.9 .5	3.8	1.7	2.5	4.2	5.2
.820	-1.3	-1.4 9	.5 -2.0	1.9 2.5	2.3 .0	.8 1	6	2.5
.830	-2.2	2	1.7	2.5	-1.3	.0	2.6 -1.1	2.6
.840	1	-1.5	-2.8	3.2	1.1	1	-2.9	1.7 3.1

TIME (SEC)	(VEL. X	CG AC	CEL(G' Z	S)) R	(VEL. X	REAR Y	ACCEL	(G'S) R	.)
.850	1.3	.0	-1.0	1.6	.7	1	2.2	2.3	
.860	-1.6		2.3	3.0	-1.0	8	-4.3		
		.8							
.870	3.3	.2	-1.3	3.6	-3.5	-2.1	1.2	4.2	
.880	4	1.3	.2	1.3	.7	.1	.1	.7	
.890	1	2.3	2.2	3.2	1.1	-1.6	.7	2.1	
.900	1.4	3.0	.0	3.3	9	-1.0	1.9	2.4	
.910	2	2.0	1.8	2.7	-1.5	1	-1.5	2.2	
.920	2.3	1.3	.1	2.7	1.2	1.8	.6	2.2	•
.930	3	-1.3	4	1.4	7	.1	3.1	3.2	
.940	-1.2	-1.0	2.0	2.5	7	.0	-2.0	2.1	
.950	1.1	.1	4	1.2	.2	.1	. 9	.9	
.960	.1	2.1	1.2	2.4	6	9	1.6	1.9	
.970	-1.4	1.2	1.3	2.2	1.1	-1.0	-1.6	2.2	
.980	.8	.9	- 7	1.4		3			
.990	- 9	1.5	1.5	2.3	1.4	5			
	NUM VALUES						3.5	J.,	
		Х-	SEC	· Y	SEC	Z	SEC	R	-SEC
- VEL. CG ACCI	BL (G'S)	26.8	.721	-22.9	.579	11.5	.714	29.5	.721
VEL. REAR ACC					.586	26.6	.737	26.7	.737
7221 1024 1100	(0 0)	-0.0						20.,	

TEST ID ----- NETC-3C TEST DATE ---- 12-18-97 VEHICLE CLASS - OTHER IMPACT SPEED -- 22.23 M/S

		AC(CELERATIO	N-(G'S)	
			DISK	BRAKE	
TIME		BLOCK	CALI	PERS	INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
.000	4	-27.8	.5	3	.3
.010	.1	-28.3	3	1	.0
.020	4	-28.0	5	-1.8	.3
.030	.0	-29.2	1.2	5.0	.1
.040	.0	-29.5	3.7	5.5	.1
.050	.5	-30.3	3.5	14.7	-1.6
.060	.6	-27.1	3.3	37.7	-1.0
.070	2.9	32.6	-52.9	123.2	9
.080	.3	35.2	-2.2	50.4	-1.4
.090	-2.0	35.3	-31.7	65.0	-1.9
.100	-1.3	35.3	-6.1	67.8	1.0
.110	3.7	35.3	-23.0	63.6	1.2
.120	. 4	-24.7	-26.5	33.6	-1.9
.130	-3.8	-27.8	-29.0	4.8	-4.2
.140	. 4	-28.5	-58.7	12.6	1.8
.150	.2	-28.5	-33.3	-6.8	.0
.160	-2.4	-30.0	-40.9	10.3	4.4
.170	2.0	-29.7	-17.8	5.5	8.8
.180	.8	-29.0	-22.0	1.8	.4
.190	-2.6	-27.8	-11.5	4.4	-1.4
.200	.2	-28.6	-13.9	11.6	9
.210	2.0	-26.4	5	10.2	2
.220	6	37.3	3.9	-6.4	6
.230	1.3	35.3	-2.2	-8.6	-1.0
.240	1.2	35.3	3.8	-9.1	8
.250	-1.3	35.3	-13.0	-23.3	.2
.260	1.5	35.3	7.8	32.0	.1
.270	1.8	35.3	25.4	48.9	5
.280	.2	35.3	46.3	-6.4	-2.1
.290	2.5	35.3	23.3	-39.7	.8
.300	-1.8	-12.9	-2.3	-35.0	1.0
.310	1.4	-34.1	23.7	-11.1	2
.320	6.0	-9.3	31.4	82.8	-3.5
.330	1	-24.5	21.7	87.7	1.7
.340	-3.8	23.5	3.8	112.7	-4.0
.350	2.0	-13.4	-37.8	103.9	1

		AC	CELERATIO		
			DISK		
TIME	ENGIN	BLOCK	CALI	PERS	INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
.360	3.9	-24.7	-88.7	-59.5	. 4
.370	.3	-28.8	-27.7	12.7	-6.9
.380	-2:2	-27.8	-35.9	-10.1	5.7
					1.0
.390	-1.4	35.2	-25.2	8	
.400	1.8	35.1	-18.7	1.8	-2.3
.410	2.0	-28.9	-7.2	1.9	-1.7
.420	4	-29.4	-11.6	7	9
.430	1.2	-30.8	-18.1	.0	8
.440	2.0	-28.4	-41.7	.2	.2
.450	-2.2	-29.2	-20.0	.1	.1
.460	-2.3	-29.7	-11.1	.1	1.9
.470	1.8	-29.5	-6.5	19.2	2
.480	3.1	-29.5	-7.4	.3	4
.490	.3	-29.8	-3.6	.2	.4
.500	.1	-29.4	-5.6	.3	1
.510	1.5	-28.5	-3.2	.3	-1.8
.520	.5	-29.7	2.9	2.5	-2.9
					2.0
.530	-2.3	-27.8	8.1	1.2	
.540	-1.6	-28.4	2.1	1.2	.3
.550	1.0	-30.1	4.2	.9	1.3
.560	1.7	-2.3	4.6	.7	-3.5
.570	.1	35.3	10.5	.6	-151.7
.580	1.5	35.3	1.8	.6	-151.7
.590	3.2	35.3	9	.9	-151.7
.600	-2.3	-28.0	.5	1.0	-151.7
.610	-5.2	-28.1	8.1	1.1	1.4
.620	~.3	-30.4	5.3	1.1	3.9
.630	3.4	-30.4	.7	1.0	-1.4
.640	1.2	-30.6	-6.3	1.1	8
.650	8	-28.9	-4.9	1.2	2.4
.660	.9	-28.4	-6.0	1.0	-1.5
.670	.8	-28.3	-6.1	. 9	.0
.680	-1.3	-28.8	-2.1	.8	1
.690	.6	-28.3	-6. 4	9.0	1.1
.700	2.6	35.3	9	2.4	-2.1
.710	-2.5	35.3	-1.1	.5	-1.4
.720	8	35.3	4.1	.7	
					.1
.730	3.4	35.3	5.6		.0
.740	1.2	35.3	10.2	.7	-1.5
.750	8	35.3	1.9	. 8	-2.9
.760	1.9	-1.9	2	.8	-1.9
.770	4	-27.7	-4.8	.8	-1.1
.780	- 9	-28.3	-5.9	. 8	6
.790	.4	-27.4	-7.3	.8	9
.800	.5	-28.8	5	.8	-1.9

----- ACCELERATION-(G'S) ------DISK BRAKE

			DISK	BRAKE	
TIME	ENGIN	BLOCK	CALI	PERS	INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
		~			
.810	.1	-29.5	-10.9	.7	-1.0
.820	5	-28.8	-1.1	.5	8
.830	9	-29.0	5	.3	. 2
.840	3	-28.7	.7	.5	.3
.850	-1.1	-28.7	-3.2	.5	5
.860	-1.4	-28.9	-5.0	.2	2
.870	7	-29.6	-3.5	.2	2.0
.880	. 0	-28.4	-3.3	3	.9
.890	.2	5.5	-1.3	-1.0	.1
.900	.6	35.3	-6.6	6	1.5
.910	1.2	35.3	-7.2	-4.3	1.6
.920	.6	35.3	1.6	-9.3	.6
.930	1.2	35.3	5.5	-4.4	1.0
.940	4	35.3	.1	5	1.9
.950	-2.4	35.3	2.5	.1	1.1
.960	9	35.3	5	2	.7
.970	1.4	35.3	1.9	.1	.6
.980	.1	35.3	-5.5	. 2	6
.990	-1.4	35.3	5	. 3	1.1

TEST ID ----- NETC-3D TEST DATE ---- 12-18-97 VEHICLE CLASS - OTHER IMPACT SPEED -- 22.23 M/S

		AC	CELERATIO		
			DISK		
TIME		BLOCK	CALIPER		INSTRUMENT
(S)	TOP	BOTTOM	RIGHT	LEFT	PANEL
.000	4	-27.8	7	1.3	.3
.010	.1	-28.3	.1	. 9	.0
.020	4	-28.0	.6	. 3	.3
.030	.0	-29.2	.1	2	.1
.040	.0	-29.5	.5	. 5	.1
.050	.5	-30.3	.0	.6	-1.6
.060	.6	-27.1	3	.6	-1.0
.070	2.9	32.6	.5	.3	9
.080	.3	35.2	.4	.9 . 9	-1.4
.090	-2.0	35.3	.1	6	-1.9
.100	-1.3	35.3	2	. 9	1.0
.110	3.7	35.3	4	.8	1.2
.120	. 4	-24.7	2	1.4	-1.9
.130	-3.8	27.8	.7	3	-4.2
.140	. 4	-28.5	.5	3 '	1.8
.150	2	-28.5	1	1	.0
.160	-2.4	-30.0	7	1	4.4
.170	2.0	-29.7	.2	.5	8.8
.180	.8	-29.0	· .2	.2	.4
.190	-2.6	-27.8	.5	1.6	-1.4
.200	.2	-28.6	.5	.0	9
.210	2.0	-26.4	5	1	2
.220	6	37.3	2	.0	6
.230	1.3	35.3	2	.0	-1.0
.240	1.2	35.3	.8	.2	8
.250	-1.3	35.3	-1.7	-4.4	.2
.260	1.5	35.3	-2.6	-5.4	.1
.270	1.8	35.3	-1.6	-7.8	5
.280	.2	35.3	-2.6	-3.6	-2.1
.290	2.5	35.3	4	9.5	. 8
.300	-1.8	-12.9	3.1	13.8	1.0
.310	1.4	-34.1	1.9	6.7	2
.320	6.0	-9.3	5.6	-1.1	-3.5
.330	1	-24.5	-1.1	-9.7	1.7
.340	-3.8	23.5	-1.1	-5.1	-4.0
.350	2.0	-13.4	-4.3	4.3	1

ACCELERATION-(G'S) DISK BRAKE TIME ENGIN BLOCK CALIPERS-REAR (S) BOTTOM RIGHT 3.9 -2.7 .360 -24.7 5.4 . 4 .3 .370 -28.8 .3 .1 -6.9 .380 -2.2 -27.8.8 -3.5 5.7 -1.4 35.2 2.1 1.1 .390 1.8 35.1 -.3 -1.5.400 2.0 -28.9 1.3 1.0 .410 3.3 -29.4 .420 - .4 - . 4 1.0 .430 1.2 -30.8 -1.1 .440 2.0 -28.4 -.1 1.1 -2.2 -29.2113.3 .450 1.8 .1 -29.7 .460 -2.332.5 -3.0 1.9 .470 1.8 -29.5 113.3 -.2 3.1 .480 -29.5113.3 -1.8-.4 .3 .490 -29.8113.3 - . 6 .1 .500 -29.4113.3 -.6 1.5 -28.5 .510 113.3 -.5 -1.8 .5 -29.7 .520 113.3 1.2 -2.9-2.3 -27.8 .530 113.3 .5 .540 -1.6 -28.4113.3 -4.8 .3 .550 1.0 -30.1 113.3 -6.0 .560 1.7 -2.3 113.3 -16.0-3.5.1 .570 35.3 113.3 15.6 -151.7 .580 1.5 35.3 -6.0 113.3 -151.7 .590 3.2 35.3 113.3 7.4 -151.79.6 .600 -2.3-28.0 113.3 -151.7 -5.2 .610 -28.1 113.3 2.2 .620 -.3 -30.4113.3 7.9 3.9 3.4 .630 -30.4 4.7 113.3 .640 1.2 -30.6113.3 -1.4-.8 .650 -.8 -28.9113.3 -6.8 2.4 .9 .660 -28.4113.3 -11.2 .8 .670 -28.3-7.3 113.3 .0 .680 -1.3-28.8-5.7 113.3 -.1 .690 .6 -28.3 113.3 .8 1.1

.700 2.6 35.3 113.3 5.9 -2.1 .710 -2.535.3 113.3 3.6 35.3 .720 -.8 113.3 -1.1.1 .730 3.4 35.3 113.3 4.5 .0 .740 1.2 35.3 113.3 4.3 -1.5 .750 -.8 35.3 113.3 5.1 -2.91.9 .760 4.3 -1.9 113.3 -1.9.770 . -.4 -27.7113.3 . 9 -1.1 -.9 .780 -28.3113.3 .3 -.6 .790 . 4 -27.4 113.3 2.2 -.9 .800 .5 -28.8 113.3 1.8 -1.9

	_~	AC	CELERATION	1- (G'S)	
			DISK F	BRAKE	
TIME	ENGIN	BLOCK	CALIPERS	S-REAR	INSTRUMENT
(S)		BOTTOM	RIGHT	LEFT	. PANEL
.810	.1	-29.5	113.3	.7	
.820	5	-28.8	113.3		8
.830	9	-29.0	113.3	-5.2	. 2
.840	3	-28.7	113.3	-3.7	.3
.850	-1.1	-28.7	113.3	.5	5
.860	-1.4	-28.9	113.3	2.6	2
.870	7	-29.6	113.3	.2	2.0
.880	.0	-28.4	113.3	1.8	. 9
.890	.2	5.5	113.3	1.0	.1
.900	.6	35.3	113.3	1.4	1.5
.910	1.2	35.3	113.3	1.9	1.6
.920	.6	35.3	113.3	2.3	.6
.930	1.2	35.3	113.3	.1	1.0
.940	4	35.3	113.3	1.6	1.9
.950	-2.4	35.3	113.3	1.4	1.1
.960	9	35.3	113.3	1.1	. 7
.970	1.4	35.3	113.3	1.1	.6
.980	.1	35.3	113.3	-8.5	6
.990	-1.4	35.3	113.3	1.4	1.1

BLANK PAGE

POST NO. 7 ACCELEROMETER DATA

ACCELERO	OMETER D	ATA - TEST	NETC-3
	POST 7	POST 7	
		BOTTOM	
TIME	ACCEL	ACCEL	
(SEC)	(G'S)	(G'S)	
0.000	0.000	0.013	
0.001	-0.052		
0.002	-0.091		
0.003			
0.004		-0.065	
0.005			
. 0.006		-0.104	
0.007		-0.091	
0.008	-0.052		
0.009			
0.010	-0.065		·
0.011	-0.065	-0.117	
0.012	-0.091	-0.117:	
0.013	-0.078	-0.117	
0.014	-0.091	-0.117	
0.015	-0.078	-0.065	
0.016	-0.052	-0.117	
0.017		-0.117	
0.018			
0.019		-0.104	
0.020			
0.021			
0.022			
0.023			·
0.024			
0.025			
0.026			
0.027			
0.028			
0.029			
0.030			
0.031		-0.130	······································
0.032			
0.033		-0.104	······································
0.034		·	
0.035			
0.036	<u> </u>		
0.037	<u> </u>	-0.117	···
0.037			
0.039			
0.040			
0.041	<u></u>	·	
0.042	-0.052	-0.130	<u> </u>

0.043	-0.091	-0.104
0.044	-0.078	-0.130
0.045	-0.091	-0.117
0.046	-0.078	-0.117
0.047	-0.104	-0.117
0.048	-0.078	-0.117
0.049	-0.065	-0.117
0.050	-0.078	-0.104
0.051	-0.065	-0.091
0.052	-0.078	-0.104
0.053	-0.065	-0.130
0.054	-0.078	-0.117
0.055	-0.078	-0.130
0.056	-0.078	
		-0.104
0.057:	-0.091	-0.117
0.058	-0.130	-0.130
0.059	-0.091	-0.104
0.060	-0.091	-0.078
0.061	-0.091	-0.091
0.062	-0.078	-0.130
0.063:		-0.091
0.064	-0.026	-0.091
0.065	-0.078	-0.130
0.066	-0.065	-0.104
0.067	-0.065	-0.091
0.068	0.000	-0.104
0.069	-0.078	-0.091
0.070	-0.013	-0.104
0.071	-0.013	-0.117
0.072	-0.039	-0.065
0.073	-0.078	-0.117
0.074	-0.013.	-0.091
0.075	-0.065	-0.031
		· · · · · · · · · · · · · · · · · · ·
0.076	-0.065	
0.077	-0.091·	-0.091
0.078	-0.026	-0.130
0.079	-0.065	-0.078
0.080	-0.091	-0.104
0.081	0.000	-0.104
0.082	-0.052	-0.091
0.083:	-0.091	-0.104
0.084	-0.065	-0.078
0.085	-0.065	-0.117
0.086	-0.065	-0.104
0.087	-0.052	-0.104
0.088	-0.078	-0.130
0.089	-0.104	-0.091
0.090	-0.104	-0.065
0.090	-0.117	
		-0.130
0.092	-0.117	-0.143
0.093	-0.104	-0.130

0.094			
0.096	0.094	-0.104	-0.117
0.097	0.095	-0.117	-0.091
0.098	0.096	-0.091	-0.078
0.099 -0.078 -0.117 0.100 -0.052 -0.104 0.101 0.005 -0.091 0.103 -0.013 -0.091 0.104 0.013 -0.091 0.105 -0.026 -0.104 0.106 -0.026 -0.104 0.107 -0.013 -0.065 0.108 -0.039 -0.104 0.109 -0.078 -0.117 0.110 -0.078 -0.117 0.111 -0.104 -0.104 0.112 -0.104 -0.117 0.113 -0.091 -0.130 0.114 -0.117 -0.113 0.015 -0.117 -0.143 0.116 -0.130 -0.130 0.117 -0.117 -0.143 0.118 -0.104 -0.117 0.119 -0.091 -0.078 0.120 -0.130 -0.117 0.121 -0.104 -0.117 0.122 -0.091 <t< td=""><td>0.097</td><td>-0.065</td><td>-0.065</td></t<>	0.097	-0.065	-0.065
0.100 -0.052 -0.104 0.101 0.000 -0.104 0.102 -0.065 -0.091 0.103 -0.013 -0.091 0.104 0.013 -0.091 0.105 -0.026 -0.104 0.106 -0.026 -0.104 0.107 -0.013 -0.065 0.108 -0.039 -0.104 0.109 -0.078 -0.117 0.110 -0.078 -0.117 0.111 -0.104 -0.104 0.112 -0.104 -0.117 0.113 -0.091 -0.130 0.114 -0.117 -0.113 0.115 -0.117 -0.143 0.116 -0.130 -0.130 0.117 -0.117 -0.143 0.118 -0.104 -0.117 0.119 -0.091 -0.078 0.120 -0.130 -0.17 0.121 -0.104 -0.117 0.122 -0.091 -0.078 0.123 -0.039 -0.117 0.124 -0.078 -0.117 0.125 -0.013 -0.010 0.127 -0.039 -0.117 0.128 -0.039 -0.117 0.129 -0.091 -0.078 0.120 -0.309 -0.117 0.121 -0.040 -0.130 0.1123 -0.039 -0.117 0.124 -0.078 -0.117 0.125 -0.013 -0.104 0.126 -0.039 -0.104 0.127 -0.039 -0.091 0.128 -0.013 -0.104 0.129 -0.026 -0.091 0.130 -0.026 -0.091 0.131 -0.026 -0.091 0.131 -0.026 -0.091 0.133 -0.026 -0.104 0.135 -0.078 -0.117 0.138 -0.078 -0.117 0.138 -0.078 -0.117 0.138 -0.078 -0.117 0.138 -0.078 -0.117 0.138 -0.078 -0.117 0.138 -0.078 -0.117 0.139 -0.104 -0.130 0.141 -0.078 -0.117 0.139 -0.104 -0.130 0.141 -0.078 -0.117 0.138 -0.078 -0.117 0.139 -0.104 -0.130 0.141 -0.078 -0.117 0.142 -0.078 -0.117 0.139 -0.104 -0.130 0.141 -0.078 -0.117	0.098	-0.091	-0.130
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0.149	-0.078	-0.104
0.150	-0.052	-0.104
0.151	-0.052	-0.130
0.152	-0.065	-0.130
0.153	-0.065	-0.104
0.154	-0.091 _i	-0.117
0.155	-0.104	-0.130
0.156	-0.091	-0.078
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0.162	-0.052	-0.104
0.163	-0.026	-0.091
0.164:	-0.039	-0.104
0.165	-0.026	-0.091
0.166	-0.039	-0.091
0.167	-0.039	-0.104
0.168	-0.026	-0.117
0.169.	-0.078	-0.117:
0.170:	-0.078	-0.104
0.171	-0.091	-0.117
0.172:	-0.104	-0.130
0.173	-0.130	-0.130
0.174	-0.091	-0.130
0.175	-0.117	-0.156
0.176	-0.143	-0.104
0.177	-0.130	-0.130
0.178	-0.104	
0.179	-0.104	-0.130
0.180	-0.104	-0.091
0.181	-0.078	-0.117
0.182	-0.013	-0.117
0.183	-0.039	-0.091
0.184	-0.052	-0.091
0.185	-0.013	-0.052
0.186	-0.013	-0.065
0.187	-0.013	-0.091
0.187	-0.259	-0.259
0.189	-0.583	
		-0.233
0.190	-0.130	0.052
0.191	0.868	0.492
0.192	1.983	0.790
0.193	2.397	0.726
0.194	1.749	0.544
0.195	0.700	0.324

	0.404	0.000	_
0.196	0.104	0.039	_
0.197	0.091	-0.441	_
0.198	-1.646	-1.089	
0.199	-1.361	0.168	-
0.200	1.866	3.628	
0.201	8.073	4.574	_
0.202	11.844	5.287	-
0.203	13.412	3.214	
0.204	9.447	1.736	
0.205	3.745	0.376	_]
0.206	-1.011 ¹	-0.531	}
0.207	-3.551	-1.490	
0.208	-5.209	-1.762	
0.209	-4.898	-3.084·	
0.210	-5.572	-3.499	
0.211	-6.155	-2.708	
0.212	-7.931	-3.473	
0.213	-11.274	-4.147	
0.214	-13.554	-4.950	
0.215	-9.654	-2.864	
0.216	-4.315	-2.047	
0.217	-3.097	-2.242	_
0.218	-6.881	-3.356	_
0.219	-6.687	-2.410	
0.220	-4.224	-0.220	
0.221	2.320	2.773	_
0.222	10.056		
0.223	14.941	5.067	
0.224	14.552	3.797	٠.
0.225	10.561	3.823	
0.226	8.371	3.058	-
0.227	3.564	2.397	-
0.228	1.464	1.244	•
0.229	0.881		
0.230	1.736		
0.231	0.324	-0.479	
0.232	-2.916	-0.933	
0.233	-5.455	-1.166	٠
0.234	-6.518	-2.034	-
0.235	-3.706	-0.311	
0.236	2.682	1.568	
0.237	4.341	1.555	
0.237	3.058	1.218	
0.239	4.108	2.656	-
0.239	-4.743	0.402	-
			
0.241.	-26.539	-0.985	•
0,242	-26.539	-1.814	
0.243.	-26.539		-
0.244:	-26.539	-5.870	
0.245	-26.539	<u>-4.885</u>	
0.246	-26.539	-1.451	

	0.296	-26.539	-2.540	****************
l .	0.295	-26.539	-2.799	
	0.294	-26.539	0.272	
	0.293	-26.539	2.877	
	0.292	-26.539	2.993	
	0.291	-26.539	2.086	
	0.290	-26.539	2.177	
<u> </u>	0.289	-26.539	2.488	
!	0.288	-26.539	3.136	
	0.287	-26.539	2.384	
	0.286	-26.539	0.376	
	0.285	-26.539	0.635	
<u> </u>	0.284	-26.539	-1.646	
	0.283	-26.539:	-3.888	
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		-26.539	0.194	
		-26.539	0.389	
		-26.539	6.376	
		-26.539		
		-26.539	2.475	
		-26.539	-1.192	
		-26.539	-2.073	
:		-26.539	-0.091	
		-26.539	-0.324	
		-26.539	2.203	
		-26.539	2.307	
	0.260		4.095	
		-26.539	5.157	
		-26.539	1.490.	
		-26.539	-3.810	
	0.256		0.130	
		-26.539;	1.361	
	0.254	-26.539	-2.294	
	0.253	-26.539	-6.648	<u>-</u>
	0.252	-26.539	-8.358	
	0.251	-26.539	-7.049	
	0.250	-26.539	-5.443	
		-26.539	1.853	
	0.248	-26.539	6.000	
	0.247	-26.539	8.008	

0.298			
0.299		-2.358	
0.300	-26.539	-3.784	
0.301	-26.539	-3.214	
0.302	-26.539	-1.996	
0.303	3 -26.539	-1.374	
0.304	-26.539	-1.296	****
0.305	-26.539		
0.306	-26.539	3.123	
0.307		3.227	
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0.328	•		
0.329			
0.330		-1.983	
0.331	-26.539	-2.799	*
0.332	-26.539	-2.967	
0.333	3: -26.539	-1.762	
0.334	-26.539	-1.412	
0.335	-26.539	-1.568	The state of the s
0.336		-1.050	
0.337		-0.415	***** ** * * * ****** ****************
0.338		0.000	
0.339		0.130	
0.340		0.298	
0.34		0.181	
0.342		0.220	
0.343	<u> </u>	0.687	
0.344		0.007	
0.345			
		0.441	
0.346		0.246	
0.347		0.052	
0.348	326.539	0.544.	

0.349	-26.539	1.542	
0.350	<u>-26.539</u> .	1.879	
0.351	-26.539	0.985	
0.352	-26.539	-0.130	
0.353	-26.539	-1.063	
0.354	-26.539	-1.827	
0.355	-26.539	-1.879	
0.356	-26.539	-1.140°	
0.357	-26.539	-0.078	
0.358	-26.539	1.231	
0.359	-26.539	1.542	
0.360	-26.539	1.179	
0.361:	-26.539	0.363	
0.362	-26.539	-0.156	
0.363	-26.539	-0.557	
0.364	-26.539	-0.933	— —
0.365	-26.539	-1.140	
0.366	-26.539	-1.063	· · · · · · · · · · · · · · · · · · ·
0.367	-26.539	-0.622	:
0.368	-26.539	0.104	
0.369	-26.539	0.635	
0.370	-26.539	0.428	
0.371	-26.539	0.402	
0.372	-26.539	0.233	
0.373	-26.539	-0.531	
0.374		-0.790	
0.375	-26.539	-0.583	· ·
0.376	-26.539	-0.130	
0.377	-26.539	-0.13	
0.378	-26.539		
0.379		0.091	
0.379	-26.539	0.207	·
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0.386:	-26.539	0.920	
0.387	-26.539	0.143	
0.388	-26.539	-0.389:	
0.389	-26.539	1.711:	
0.390	-26.539	6.194	
0.391	-26.539	5.222:	
0.392	<i>-</i> 26.539	4.406	
0.393	-26.539	3.719	
0.394.	-26.539	6.414	
0.395	-26.539	6.868	
0.396	-26.539	3.136	
0.397	-26.539	-1.387	
0.398	-26.539	-4.782	
0.399	-26.539	-4.367	
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0.400	-26.539	-3.473
0.401	-26.539	-3.551
0.402	-26.539	-3.201
0.403	-26.539	-3.136
0.404	-26.539	-3.304
0.405	-26.539	-4.250
0.406	-26.539	-4.963
0.407	-26.539	-4.315
0.408	-26.539	-4.561
0.409	-26.539	-3.732
0.410	-26.539	-1,801
0.411	-26.539	-0.894
0.412	-26.539	-2.320
	-26.539	-3.201
0.414	-26.539	-3.667
0.414	-26.539	-4.535 ⁴
0.415	-26.539	-1.425
0.417		3.214
	-26.539	4.315
0.419		4.678
0.420	-26.539	4.082
0.420	-26.539	3.615
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0.422	-26.539	2.410 3.097
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0.436		
0.437	-26.539	0.363
0.438	-26.539	1.542
0.439	-26.539	2.501
0.440	-26.539	2.864
0.441	-26.539	0.687
0.442	-26.539	0.130
0.443	-26.539	-0.285
0.444	-26.539	0.700
0.445	-26.539	3.952
0.446	-26.539°	2,929
0.447	-26.539	1.400
0.448	-26.539	1.646
0.449	-26.539	0.544
	-26.53 9	0.492
0.450	- 20.55 9	U.43 <u>C</u>

0.451	-26.539	0.052
0.452	-26.539	0.726
0.453	-26.539	0.389
0.454	-26.539	0.467
0.455	-26.539	1.244
0.456	-26.539	1.464
0.457	-26.539	2.618
0.458	-26.539	2.022
0.459	-26.539	1.762
0.460	-26.539	0.739
0.461	-26.539	
0.462		-1.723
0.463	-26.539	-4.121
0.464	-26.539	-5.624
0.465	-26.539	-5.248
0.466	-26.539	-4.173
0.467	-26.539	-3.084
0.468	-26.539	-2.022
0.469	-26.539	-0.013
0.470	-26.539	1.179
0.471	-26.539	1.400
0.472	-26.539	1.529
0.473	-26.539	1.451
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0.475	-26.539	1.205
0.476:	-26.539	
	-26.539	0.596
0.478	-26.539	0.428
0.479	-26.539	0.596
0.480	-26.539	
0.481	-26.539	0.065
0.482	-26.539	-0.454
0.483	-26.539	-1.711
0.484	-26.539	-2.631
0.485	-26.539	
0.486	-26.539	
0.487	-26.539	0.156
0.488	-26.539	0.687
0.489	-26.539	0.609
0.490	-26.539	0.596
0.491	-26.539	-0.285
0.492	-26.539	0.143
0.493	-26.539	-0.298:
0.494	-26.539	-0.194
0.495:	-26.539	-0.246:
0.496	-26.539	-1.037
0.497	-26.539	-1.089
0.498	-26.539	-1.192
0.499	-26.539:	0.246
0.500	-26.539	0.479
0.501	-26.539	1.179

	0.502	-26.539	1.244	
	0.503	-26.539	-4.276	
	0.504	-26.539	-4.924	
	0.505	-26.539	-5.002	
	0.506	-26.539	-3.278	
	0.507	-26.539	-2.825	
	0.508	-26.539	-1.270	
	0.509	-26.539	-1.464	
	0.510	-26.539	-0.998	
	0.51.1	-26.539	-1.076:	
	0.512	-26.539	0.052	
	0.513	-26.539	0.492	
	0.514	-26.539	1.931	
	0.515	-26.539	1.957	
<u></u>	0.516	-26.539	1.646	
		-26.539	0.363	***
		-26.539	0.609	
		-26.539	-0.091	
		-26.539	0.013	
		-26.539	-0.194	
		-26.539	0.207	
-		-26.539	1.335	
		-26.539	1.879	
	0.525		0.687	
	0.526		1.192:	
	0.527		0.518	
	0.528	-26.539	0.402	
	0.529	-26.539	1.516	
	0.530	-26.539	1.490	
	0.531	-26.539	1.827	
	0.532	-26.539	2.125	
	0.533	-26.539	1.736	
	0.534		0.778	·
ļ	0.535	-26.539	0.998	
	0.536	-26.539	1.101	
	0.537	-26.539	0.311	
	0.538	-26.539	-0.078	
	0.539	-26.539	-0.285	····································
	0.540	-26.539	-1.283	
	0.541	-26.539	-1.231	
 	0.542	-26.539	-0.868	
	0.543	-26.539	-0.324.	· · · · · · · · · · · · · · · · · · ·
	0.544	-26.539	0.376	
	0.545	-26.539	0.790	
	0.546	-26.539 -26.539	1.490	
				
<u> </u>	0.547	-26.539	1.011	
	0.548	-26.539 26.530	1.063	*
	0.549:	-26.539	-0.428	
	0.550	-26.539	-0.881	
<u> </u>	0.551	-26.539	-0.674	******************************
	0.552	-26,539	-0.583	

2.550	00.000		
	-26.539	-0.026	
0.554		-1.153	
0.555		-1.322	
0.556			
0.557		-2.060	
	-26.539		
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0.560			
	-26.539		:
0.562	-26.539	-1.490	
***************************************	-26.539		:
0.564	-26.539	-1.089	:
0.565	-26.539	-0.311	· · ·
0.566	-26.539	-0.181	
0.567	-26.539	-0.013	
0.568	-26.539	-0.220	
0.569	-26.539	0.000	:
0.570	-26.539	0.000	•
0.571	-26.539	0.026	· · · · · · · · · · · · · · · · · · ·
0.572	-26.539	0.078	
0.573	-26.539	0.363	· · · · · · · · · · · · · · · · · · ·
0.574	-26.539	0.596	
0.575	-26.539	0.894	
0.576		0.531	
0.577	-26.539	-0.143	:
0.578	-26.539	-0.622	:
0.579	-26.539 ¹	-0.985	
0.580	-26.539	-0.661	
0.581	-26.539	-0.181	
0.582	-26.539	0.220	:
0.583	-26.539	0.505	
0.584	-26,539	0.531	
0.585	-26.539	0.674	
0.586	-26.539	0.635	:
0.587	-26.539	0.855	
0.588	-26.539	1.063	
0.589	-26.539	1.283	
0.590	-26.539	1.412	— —
0.591	-26.539	1.127	
0.592	-26.539	0.648	. ,
0.593	-26.539	0.207:	
0.594	-26.539	0.156	
0.595	-26.539	0.117	
0.596	-26.539	-0.052	
0.597	-26.539	-0.194	·
0.598	-26.539	-0.531	
0.599	-26.539	-0.946	
. 0.600	-26.539	-1.089	
		1,000	



APPENDIX E - FEDERAL HIGHWAY ADMINISTRATION ACCEPTANCE LETTER

U.S.Department of Transportation

Federal Highway Administration March 11, 1999

400 Seventh St., S.W. Washington, D.C. 20590

Refer to: HMHS-1

Mr. James M. Sime Assistant Manager for Research Connecticut Department of Transportation 280 West Street Rocky Hill, CT 06067

Dear Mr. Sime:

In your January 25, 1998, letter to the Federal Highway Administration's (FHWA) Director, Office of Engineering, you requested acceptance of two bridge rail designs that were developed and tested for use on the National Highway System by the New England Transportation Consortium (NETC).

The first design is the NETC 2-Bar Curb-Mounted Bridge Railing shown as Enclosure 1. This design was tested to Performance Level 2 (PL-2) in accordance with the American Association of State Highway and Transportation Officials Guide Specifications for Bridge Railings and was effectively accepted as an NCHRP Report 350 Test Level 4 (TL-4) railing by its inclusion in the summary listings attached to my May 30, 1997, memorandum on crash testing of bridge railings.

The second design is the NETC 4-Bar Sidewalk-Mounted Bridge Railing shown as Enclosure 2, and documented in publication Nos. FHWA-RD-99-027, FHWA-RD-99-028, FHWA-RD-99-029, and FHWA-RD-99-030, entitled "Full-Scale Crash Evaluation of Sidewalk-Mounted Steel Bridge Railing." Review of each crash test report showed that the 4-Bar Bridge Railing met all appropriate evaluation criteria for an NCHRP Report 350 traffic barrier at TL-4. Summary sheets on each of the three tests that were conducted are enclosed (Enclosure 3).

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Based on the information you provided for our review, we conclude that both the NETC 2-Bar Curb-Mounted Bridge Rail and the 4-Bar Sidewalk-Mounted Bridge Rail are acceptable as TL-4 designs and may be used on the National Highway Safety when selected by a transportation agency. We understand that neither design is proprietary and that anyone wishing to obtain detailed plans and specifications may contact you by telephone at (860) 258-0309 or via e-mail at james.simes@po.state.ct.us. We further understand that the NETC is currently developing transitions to be tested in the near future for use with these two bridge railings.

Sincerely yours,

Dwight 4. Horne

Dwight A. Horne
Director, Office of Highway Safety
Infrastructure

3 Enclosures

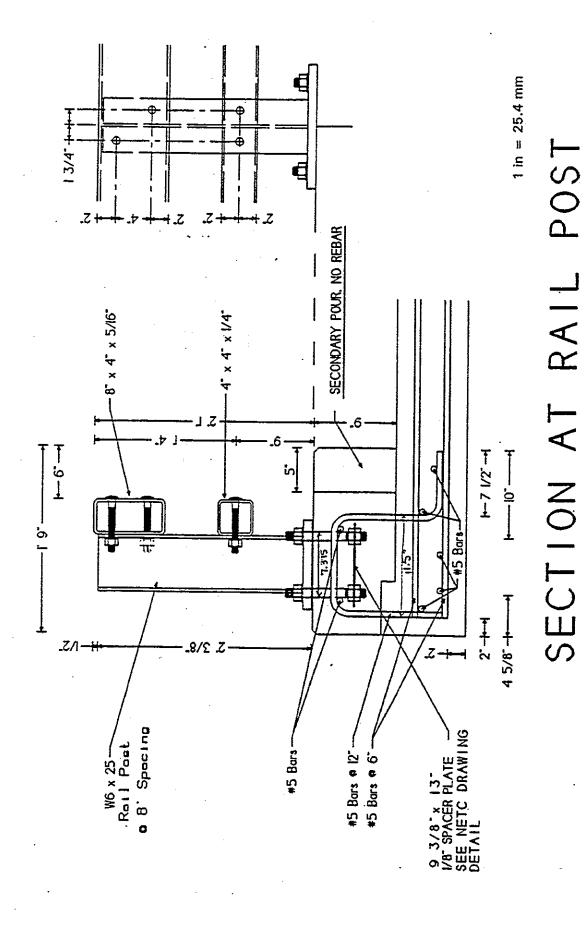
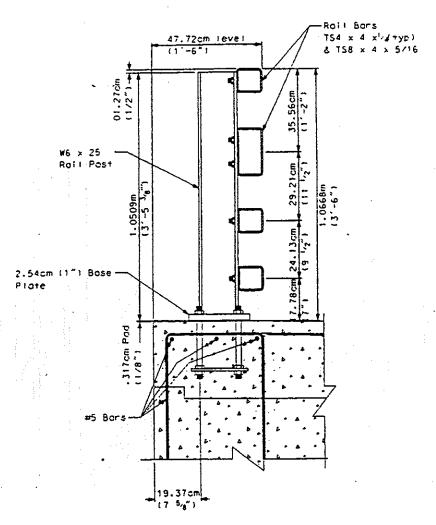
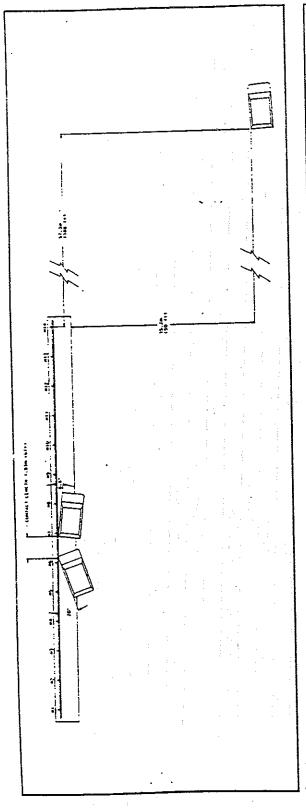


Figure 1. Schematic of the test installation for test 471470-18.



TYPICAL SECTION

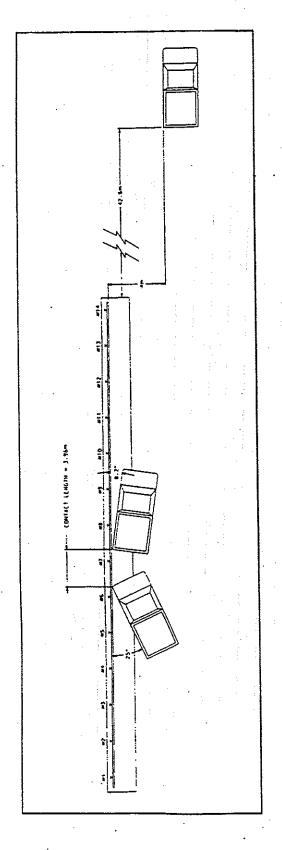


		7 True Vokicle (Continued)		10. Ridedows Acceleration (g's)	
4. General Information		,			
Test Award	Southwest Research Institute	Mass (kg) Dummy(s)	75	y-direction	•
(1118)	- OLLI	Mass (kg) Gross Static	903	11. Test Article Deflection (m)	
Ten Number	Nei C-1				0
Test Date	16/11/11	2. Impact Canditions		Lypamic	
		Speed (km/h)	0'001	Permanent	0
S. IOKARIWE		A	20.0	12. Vehicle Damage	
Type	Bridge Kaul	Augus (ask)		1	
Installation eneth (m)	32.9	9. Exit Conditions		Ехієпог	
()	- Contract De 2) -	Speed (km/h)	18.3	VDS	11-FL-2
Bunser	4 Stock State			Off.	11F1.EE2
6. Soll Type and Condition	N/A	Angle (deg)	6.6		
4 4 5 5 5 5 5 5		10. Occupant Risk Values		Interior	
/ ICH YCHKK				Jugor I	LF0000000
Type	Production	Impact Velocity (m/s)			
	2000	x-direction	•	13. Post-Impact Vehicular Behavior	
		distant		Maximum Roll Angle (deg)	10 Approximate
Model	1991 Ford Festiva	yarcenon		1.00	Annountee
Mass (kg) Curb	127	Ridedown Acceleration (g's)		Maximum Fitth Angre (ucg)	
	2.7	X-direction	•	Maximum Yaw Angle (deg.)	34 Approximate
Wass (8) test metals					

*No occupant risk data - lateral accelerometer malfunctioned during test.

Figure 8. Impact sequence and summary of test conditions and results - Test NETC-1.

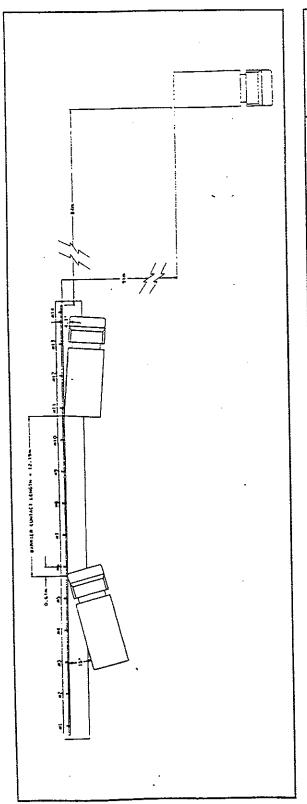
E-5



4 Ceneral Information		7. Test Vehicle (Centinued)		10. Ridedown Acceleration (g's)	-
Test America	Southwest Research Institute	Mass (kg) Dummy(s)	75	'y-direction	•
Total Number	NETC.2	Mass (kg) Gross Static	2,109	11. Test Article Deflection (mm)	
Total Name of Tables	11/20097	8. Impact Conditions		Dynamic	25 (cst.)
Jest Die		Speed (lun/b)	100.0	Permanent	េ
S. 1est Atticle		4 1- (4)	25.0	12. Vohicle Damage	
Туре	Brage Kali	(Par) 1000			
Installation Length (m)	34.1	9. Exit Conditions		Exteror	
Remise	4 Bar, Sidewalk-Mounted	Speed (km/h)	17	VDS	11-FL-3
C. C. Il Tone and Candidan	NA	Angle (deg)	8.2	cpc	IIFLEES
		10 Overnoor Bick Values		Interior	
7. Test Vehicle					1 5000000
Type	Production	Impact Velocity (m/s)		OCDI	LFWWWW
Theirmition	2000P	x-direction	3.99	13. Post-Impact Vehicular Behavior	•
9:00	056 7171001	valirection		Maximum Roll Angle (deg.)	20 Approximate
Model	1991F0fd F-250	Jamanan			15 Approximate
Mass (kg) Curb	2,034	Ridedown Acceleration (g's)		Maximum Filch Angle (Oct.)	a wanday of
Mace (ba) Toot Insertial	2.014	X-direction	-2.55	Maximum Yaw Angle (deg)	V/V
Mass (Ag) 10st mention					

*No data - vehicle lateral accelerometer malfunctioned during test.

Figure 11. Impact sequence and summary of test conditions and results - Test NETC-2.



1

A Course Information		7. Test Vehicle (Contlaued)		10, Ridedown Acceleration (g's)	
4. Central material	Compluser Decearch Institute	Mass (ke) Dummy(s)	NA	y-direction	14,30
1cst Agency				as many and the Badface (man)	
Test Number	NETC-3	Mass (kg) Gross Static	8,108	1), 1ct Afuct Denembra	
Tare Date	12/18/97	8. Impact Conditions		Dynamic (25
10t Date		Speed (km/h)	80	Permanent	13
S. Ich Ankle	: 4 : 4	Amole (dea)	15.0	12. Vehicle Damage	
Type	Bridge Kaul	المالات المدور			
Installation Length (m)	34.1	9. Enit Canditions		Exterior	
Barrier	4 Rails, Sidewalk-Mounted	Speed (km/h)	57.6	VDS	N/A
6 Call Tuna and Condition	N/A	Angle (deg)	17	. DCD	N/A
o, son type and construct		10 Occupant Rick Values		Interior	
7. Test Vehicle					411
Type	Production	Impact Velocity (12/8)		OCDI	NA
Designation	\$000\$	x-direction	1,65	13. Post-Impact Vehicular Behavior	
Model	1993 International 4600 LP	y-direction	-2.89	Maximum Roll Angle (deg)	20 Approximate
T. O. L. D. L. M.	81.8	Ridedown Acceleration (R's)		Maximum Pitch Angle (deg.)	5 Approximate
Mass (4g) Cuto		V disenton	-8.95	Maximum Yaw Angle (deg)	N/A
Mass (kg) Test Incrtial	8,108	A-duccion			

Figure 14. Impact sequence and summary of test conditions and results - Test NETC-3.